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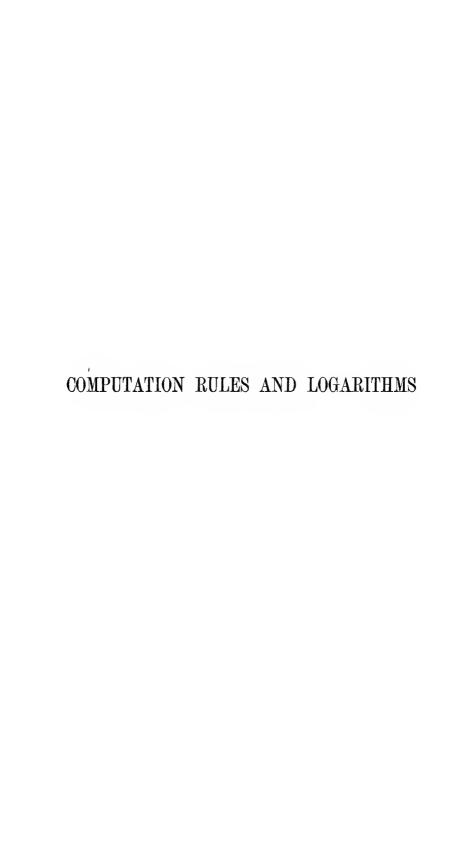
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COMPUTATION RULES

AND

LOGARITHMS

WITH TABLES OF OTHER USEFUL FUNCTIONS

 \mathbf{BY}

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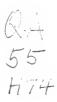
New York

MACMILLAN AND CO.

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1896

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PREFACE.

IT would probably be within safe limits to assert that one-half of the time expended in computations is wasted through the use of an excessive number of places of figures, and through failure to employ logarithms. This waste might be almost wholly avoided by following a few simple computation rules and practising slightly with logarithm tables.

The loss from the use of superfluous figures will be appreciated when it is considered that in direct or logarithmic multiplication and division with four, five, and six places of figures the work is respectively in the ratio of 1:2:3, or perhaps more nearly 2:3:4. Thus contrary to the fallacious excuse so commonly given that it is just about as easy to use six- or seven-place tables as smaller ones; the work is doubled or trebled by the use of six places instead of four. Even the employment of six- or seven-place tables, and dropping superfluous places when four or five are desired, causes much loss of time.

The proper employment of logarithms for work of four or more places effects a saving of one-quarter and upward of the time required for direct multiplication or division, with a lessening of fatigue and a gain of accuracy.

The following pages contain simple rules to enable one to answer for himself the question, how many places of figures ought I to use in this computation?—also, an explanation of the use of the notation by powers of ten; certain instructions, more or less novel in form, as to the use of the logarithm and other tables; and a collection of useful tables. This collection is designed to contain all the mathematical tables ordinarily required, and nothing more, in practical work in all branches of the engineering professions, and by students of physics, chemistry, and engineering, for work of any grade not exceeding about one-twentieth of one per cent in accuracy. For

viii PREFACE.

many persons the present volume should, therefore, provide all the logarithmic and trigonometric tables needed for the entire range of their practice. For work of greater precision than the above limit, the more bulky Vega, or some similar reliable seven-place table would be required. It is exceedingly rare that more than six or seven places are necessary, while for most work five are sufficient, although a striking chapter of absurd illustrations might be gleaned from various text-books and tables where ten- and even twenty-place logarithms are given, often for quantities uncertain in their fourth or fifth place. Persons doing much work with squares, cubes, square roots, cube roots, or reciprocals of more than four places would naturally make use of the Barlow Tables.

The rules for significant figures (pages xi to xv) are intended to be terse, direct, and simple, so that they may be easily acquired and retained. The strong type emphasizes the leading portions. The ordinary and finer types give details and explanations. For the sake of affording still greater prominence to the main working portions, some explanatory matter which will be unnecessary to many persons has been transferred from its more logical position of precedence to the latter part of the text. These rules in various forms have been in successful use by large classes of students, in connection with the author's "Physical Laboratory Notes" (printed, but not published, by the Massachusetts Institute of Technology), and his "Precision of Measurements." The recognition of the need of such rules amongst engineers and others whose practical work demands rapid and reliable computations was the cause of their general introduction into this laboratory instruction. It is therefore hoped that they may render effective service to others besides the students for whom they have been more directly designed.

In the arrangement of the tables, the effort has been exerted to make them correct, legible, systematic, and convenient in use. A new set of tables is, of course, liable to contain mistakes; notices of errata will therefore be thankfully received.

The special indexing of the corners of pages, the use of heavy type at points to be made conspicuous, the employment of spaces rather than rules for the partition of lines and columns, and the style of type and kind of paper used, are believed to conduce to legibility. As to system of arrangement, there are few novelties other than the insertion of the logs, cologs, and reciprocals of 1.000 to 1.100 at the top of the respective four-place tables, and the division

of most of the four-place tables so that the second page begins with 5.0 instead of the customary 4.5. The frequent occurrence of cor rection and reduction factors, ranging from 1.0 to 1.1, renders this by far the most frequently used part of the table; while at the same time, on account of the large tabular differences, interpolation is here the most laborious. The insertion of logs, cologs, and reciprocals from 1.0 to 1.1 with increments of 0.001 and 0.0001, respectively, in the four- and five-place tables, obviates this interpolation. In tables of antilogs and square roots the addition would be of little service. In the tables of logarithms and of square roots, heavier type has been used at apparently scattered points throughout the body of the tables. These points, in the five-place logarithm tables, for instance, are where the first two figures in the mantissa change by one unit in the second place, e.g. oo, o1, o2, etc. The obvious service of this is to aid the eye in finding any desired mantissa in working the table backward to obtain the antilog or number corresponding. The object is, of course, the same in the other tables.

As to the wisdom of departing from the usual custom of omitting decimal points entirely from logarithm tables, the author believes that the retention of the point promotes clearness of comprehension of the tables by beginners, and lessens mental effort in more experienced computers, especially when associated with the notation by powers of 10, as in the explanations here given. It seems unfortunate that this simple notation, so useful in computation and so great an aid in the explanation of numerical relations, is not universally incorporated into arithmetical instruction.

The rules for the employment of logarithms and of the tables have not been prepared especially to meet the need of those entirely unfamiliar with the principles of logarithms, although they would probably be intelligible to any mature beginner. It is thought, however, that the explanations and instructions given may prove an aid even to those who are already somewhat familiar with the subject.

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Boston, August, 1895.

COMPUTATION RULES.

PROPER NUMBER OF PLACES OF SIGNIFICANT FIGURES.

The following three pages contain the rules and their underlying principles in a condensed form for ready reference. For readers to whom some of the terms employed are unfamiliar, or who desire fuller proofs and explanations, some additional pages of "Definitions and Explanations" have been appended.

These rules should enable a computer to decide at the outset of his work, or at the successive stages of it, what number of places of significant figures he should retain in order to avoid waste of labor on the one hand or sacrifice of accuracy on the other. They provide for a sufficient number of places to assure that (barring mistakes) the accumulated error arising from the rejection of further places shall be always smaller, usually much smaller, than the supposed uncertainty of the data or result, in computations involving not more than about 20 rejections. The retention of more places is worse than useless. It adds nothing to the accuracy of the result, although increasing materially the labor of computing, and the liability to mistake. The aggregate value of the time thus wasted, - obvious enough to any one who has had occasion to perform extended computations, — may be appreciated from the fact that the use of five places where four would suffice, nearly doubles the labor; using six places instead of four, nearly trebles it; thus wasting 100 and 200 per cent respectively of the necessary amount of work, and probably a greater proportion of time. Moreover, incongruities in the use of places of figures arouse skepticism as to the competence of the worker in other directions.

FUNDAMENTAL PRINCIPLES.

Retain everywhere enough places to correspond to two unreliable places in the final result; the direct object of this is to keep the first place of unreliable figures in the final result substantially free from the accumulated rejection errors.

EXCEPTIONS.—A final result is seldom stated to more than one uncertain place unless the uncertainty of that place is small (say plus or minus four or less).

Example: 1, page xvi.

Single direct measurements generally yield numbers extending to only one uncertain place. This should not, however, be taken as a reason for relaxing the application of the above rule to subsequent steps of the computation, especially in deducing the mean or average of several single observations.

Final zeros occurring in decimal fractions should be retained when any other digit in the same place would be retained. This is of course essential to show that this place is known.

The foregoing principles consistently carried out constitute entirely sufficient rules. But more detailed instructions are usually required at the outset. These are readily understood in view of the two following propositions, which one can easily verify by algebra or by numerical examples.

Proposition I.—In multiplication or division, the percentage accuracy of the product or quotient cannot exceed that of the factor whose percentage accuracy is least.

Proposition II.—In addition or subtraction, the result cannot be accurate beyond the first decimal place which is inaccurate in any component.

A more general form of statement from which these follow is: If several numbers are multiplied or divided, a given percentage error in any one of them will produce the same percentage error in the result. If several numbers are added or subtracted, a given error or change in the digit in any decimal or other place will produce an equal error or change in the digit in the same decimal place in the result.

RULES IN DETAIL.

REJECTION. — In casting off places of figures, increase by I the last figure retained when the first left-hand rejected figure is 5 or greater; otherwise leave it unchanged.

Example. — If the last two figures are rejected

756 827.9 becomes 756 830. and 0.00 263 439 becomes 0.00 263 4.

A MEAN OR AVERAGE should always be carried to two unreliable figures.

A mean is more reliable than the single observation from which it is computed (in proportion to \sqrt{n} , the square root of the number of observations). Thus, as the data frequently extend to only one unreliable figure, the mean will often have to be carried two places further than the single observation.

MULTIPLICATION OR DIVISION. — Ascertain from the object of the work the percentage accuracy desired in the final result; or, by inspection of the data, find the percentage accuracy of that factor for which this is least, *i.e.* for which the deviation-measure or the estimated error, expressed as a per cent, is largest. See Example 1, page xvii.

In direct multiplication or division retain in every factor, product, and quotient throughout the entire process, and in final results, for an accuracy of about

One per cent, or worse, four (4) places of significant figures; One-tenth per cent, or worse, five (5) places of significant figures; and so on.

In the ordinary and the shortened processes of "long multiplication," it is best to carry out the partial products one place beyond that yielding the last place required in the result under the above rule.

Examples: 2-5, page xvii.

LOGARITHMS. — If the multiplication or division is performed by means of logarithms, the mantissa should contain as many places as are required by the foregoing rules for the direct process; i.e. for about

One per cent, or worse, use four (4) place tables;

One-tenth per cent, or worse, use five (5) place tables.

Examples: 2-5, page xvii.

Addition or Subtraction. — Ascertain from the stated object of the work the percentage accuracy desired. If this is about

One per cent, or worse, carry the result to four (4) places of significant figures;

One-tenth per cent, or worse, carry the result to five (5) places of significant figures; and so on, and carry each component quantity to that place of decimals which would correspond to this required place in the result, that is, stand in the same column with that place.

Examples: 6-8, page xix.

WHEN THE DESIRED ACCURACY IS NOT STATED, inspect the data to find the component whose first uncertain place is furthest to the left, i.e. whose deviation measure (page xlii), in units, not percentage or fractional, is greatest. Retain this component to two uncertain places, and all other components to the place which would stand in the same column with this second place.

Examples: 6-8, page xix.

N. B. — If the number of components approaches 20, care may well be taken in refined work that an unusually large rejection error does not enter through a special combination of rejected figures. The rules are, however, sufficient for the worst possible case.

The computer should notice that the *percentage* precision of a result which is the difference of two or more quantities will usually be smaller, and may be much smaller, than that of any of the component quantities.

Numerical Substitution in Formulæ. — A large number of formulæ may be represented by the type

$$x = \frac{a \cdot b \pm c \cdot d \pm \cdots}{p \cdot q \pm r \cdot s \pm \cdots},$$

where a, b, c, d, etc., represent numbers to be multiplied, divided, added, or subtracted, etc., as indicated. Any one or more of the factors and terms may be wanting; or, there may be several in place of two; and so on.

Obviously, in order that the result x shall be accurate to a specified per cent, both numerator and denominator must be at least of that accuracy, and each should therefore be carried out to the number of places of significant figures needed in x. Then as the numerator consists of two or more terms ab and bc added or subtracted,

inspection under the foregoing rules for addition or subtraction will show to what decimal place each of these terms must be carried. Further, a and b must each be carried to the number of significant figures thus required in the product ab, and so on.

In complicated formulæ this process of inspection is sometimes slightly troublesome, but is essential unless the necessary precision of the components has been otherwise studied; as, for example, by the simple applications of the differential calculus as in the author's "Precision of Measurements."

Examples: 9-11, page xx. Practical examples of substitution in moderately simple formulæ.

NOTATION BY POWERS OF TEN.

Statement of the Method. - Regard the decimal point as merely an affix whose sole purpose is to indicate which is the units' place of figures. Fix the attention firmly upon the units' place as the centre of symmetry of our customary system of notation. The too universal reference to the decimal point, rather than to the units' place, in arithmetical rules and explanations, has resulted in masking this symmetry and in thus depriving the student of its important aid. In our common decimal system of notation, a digit in the units' place represents so many times unity, i.e. so many times $10^{\circ} (=1)$, or so many units. In the first place to the left of the units' place the digit represents so many times 10⁺¹, i.e. so many tens, and in the first place to the right, so many times 10⁻¹, i.e. so many tenths; in the second place to the left so many times 10+2, i.e. hundreds, and to the right so many times 10⁻², i.e. hundredths; in the sixth places, so many times 10⁺⁶ and 10⁻⁶, i.e. millions and millionths, respectively; and so on. The fundamental symmetry of the whole system about the units' place is thus obvious, and should not be lost sight of.

In counting up places, whether to right or left, always begin with the units' place as zero.

It is clear, then, that we may write numbers in this way:

```
for 90 write 9'10';

for 6000 write 6.000'10' or 6'10' as the case may require;

for 345 write 3.45'10';

for 0.00 005 write 5'10';

for 0.00 468 9 write 4.689'10';

for 850.72 write 8.5072'10'; and so on. That is,
```

Separate the number into two factors, the first being the original number with the decimal point changed in position so as to follow the first figure; the other being $10^{\pm n}$, where the sign is plus for a whole number and minus for a fraction, and where n is the number of places the decimal point has been moved.

To transform a number expressed in this way back into the ordinary form, move the decimal point n places, making the number a whole (or a larger) number if n is plus, and a fraction if n is minus.

Associate firmly in the mind the plus sign with whole numbers, the minus sign with fractions; thus avoiding confusion as to the sign of n.

In much work, the factoring need not be written out, but may merely be mental.

This notation reduces the error and work of locating the decimal point in multiplication or division, especially in expressions containing several terms in the numerator and denominator. It is very helpful in connection with the characteristic of logarithms, and the location of the decimal point in evolution, involution, and finding reciprocals. It saves space and promotes clearness in expressing large numbers or small fractions, and it is the best aid in following the decimal point while using the slide rule. It also enables one to dispense with characteristics in certain parts of computations (see Examples, page xxi).

An abbreviated notation helpful in one's own work, but perhaps not to be urged for general adoption, consists in dropping the 10, thus,

```
instead of 4.507 \cdot 10^2 write merely 4.507^2 instead of 5.3704 \cdot 10^{-3} write merely 5.3704^{-3}
```

The adoption of the bracket or parenthesis, e.g. (4.507)², for either notation in cases of possible doubt removes all risk of mistaking these indices for ordinary exponents of powers.

Examples 9, 10, 11 give incidentally illustrations of the use of the notation by powers of 10.

Symmetrical Grouping of Figures. — For writing numbers, adopt the following system of groups and spaces: —

Write 143 258.64 796 instead of 143,258.647,96, the usual method.

A still clearer method would be to write

denoting the units' place by the heavy figure, but this is impracticable. The proposed system is symmetrical about the units' place, the customary system is not. It groups together the units, tens, and hundreds of thousandths, of millionths, etc., as well as of thousandths.

sands, millions, etc. It is clearer and less liable to error by the substitution of spaces for the commas to mark off the groups Exception is usually to be made in the case of a decimal fraction containing only three or four places. Thus write 0.4612 rather than 0.4612, and 6.382 rather than 6.382.

EXAMPLES.

Example 1.—Suppose that a final result was stated as $298549. \pm 0.10$ per cent; this would mean that its uncertainty or deviation-measure or estimated measure of accuracy (see page xlii) was ± 0.10 per cent. To how many places should it be retained? 0.1 per cent of the number is $0.001 \times 300000 = 300$. Therefore the last three places are uncertain, but as the uncertainty in the first left-hand one is small (3), two uncertain places should be retained. The result, therefore, should be written $298550. \pm 0.10$ per cent.

Suppose a result given as $47.58\ 243\ 5\pm0.0062$. This would be an incorrect use of figures. The ±0.0062 shows that the result is uncertain in the third and fourth, and therefore in all subsequent decimal places.* The fifth and sixth places of significant figures are thus unreliable, so that the seventh and eighth places are entirely valueless, and should, therefore, be rejected. We should be at liberty to use our judgment as to whether the result should then be written

$$47.5824 \pm 0.0062$$
 or 47.582 ± 0.006 ,

since the uncertainty in the fifth place is large. The second is more common practice. In this example the uncertainty is $\pm 0.0062/47$. $= \pm 0.00013$, or ± 0.013 per cent. It might, therefore, have been expressed as ± 13 parts in 100,000, or ± 0.013 per cent instead of as ± 0.0062 units. It is always expressed in the same unit as the quantity itself, e.g. ft., lbs., etc., except when directly stated to be a percentage.

Example 2. Desired with an accuracy of 2 per cent, the volume of a right circular cylinder whose radius r is 6.0428 inches, and length l 12.653 inches. Volume $V = \pi r^2 l$. By the rule for multiplication, since the result is desired to worse than one per cent, the data and all steps should be carried to four places of significant figures. Hence, we should have

V =	3.142	X	6.043^{2}	×	12.65	=	1451.
-----	-------	---	-------------	---	-------	---	-------

By ordina	ary multiplic	eation:	By short	ened multipl	ication:
6.043	3.142	114.7	6.043	3.142	114.7
6.043	36.52	12.65	6.043	36.52	1 265
18129	6284	5 735	36 258	94 26	1147
24162	1 5710	68 82	240	18 84	2294
36 258	18 852	229 4	18	1 55	690
36.52	94 26	1147	36.52	6	55
	114.7	1451.		114.7	1451.

^{*}This quantity ± 0.0062 , or whatever may be its value, is the "average deviation" or the "deviation-measure" of the result; that is, the average amount by which several results similarly obtained would differ from their mean. A fuller explanation is given at page xlii. The "probable error," which is nearly identical with the average deviation, is commonly used in its stead. Either suffices.

Observe that the partial products beyond the place standing over the fifth place of the result in each multiplication are useless. Hence the obvious saving of labor in the shortened process, which is also more compact. The process is easily understood by inspection of the example. Multiply first by the first left-hand figure of the multiplier. If the resulting partial product has one more place than is desired in the result, then drop the last figure of the multiplicand when multiplying by the second figure of the multiplier; drop the last two, when multiplying by the third figure; and so on. If, however, the first partial product has not the desired number, the dropping of figures must be deferred till the third figure of the multiplier is used.

Example 3. — Desired the volume $V = \pi r^2 l$ of a right circular cylinder whose dimensions are

$$r = 6.0428 \pm \frac{1}{4} \text{ per cent}, \quad l = 12.653 \pm \frac{1}{10} \text{ per cent}.$$

The result cannot be more accurate than the least precise factor, which is obviously r. Under the rule, \(\frac{1}{4}\) per cent computations call for five places of significant figures. Hence we should have to find by multiplication or by five-place logarithms,

$$V = 3.1416 \times (6.0428)^2 \times 12.653$$
.

Note in this connection that the error in V is proportional to twice the percentage error in r, since r enters in the second power, and that in general where a number is raised to any power n the percentage error in the result is increased to n times its value in the data. These rules, however, provide sufficiently for such cases. See "Definitions and Explanations."

Example 4. — Desired the volume $V = \pi r^2 l$ of a right circular cylinder whose dimensions are given as

$$r = 6.043 \pm 0.017$$
 inches, $l = 12.653 \pm 0.038$ inches.

Under the general principle of retaining places to correspond to two uncertain figures in the result in the data, r should have four places and l five places, judging from their stated precision. But the weaker quantity fixes the number of places in the result, so that we should use but four places:

$$V = 3.142 \times (6.043)^2 \times 12.65$$
.

Example 5. — Desired the ratio of the diameter to the length in each of the Examples 2, 3, and 4.

The number of places of figures to be used would be respectively four, five, and four, just as in the above solutions. A factor in the denominator follows precisely the same rule as to places of significant figures as the one in the numerator. To contrast the ordinary and shortened solutions, the following are given:

12.65) 6.043 (0.4777	6.043 12.65
<u>5</u> 060	5060 0.4777
9830	9830
8855	8855
9750	975
8855	889
8950	86
8855	91
	

Example 6. - Desired the value to 0.6 per cent of

$$47.3489 + 174.32825 - 5.62147$$

For o.r per cent or worse (page xiv), we must retain places in the components to correspond to five places in the result. By inspection we see that the result will be slightly more than 200. Hence its fifth place will be the second decimal place, and we need retain no place beyond that in the components. Thus,

47.35 174.33 221.68 -5.62 216.06 [± an unknown amount as precision-measure].

Example 7. — Desired the algebraic sum of

$$47'.3489 \pm 0.0042$$
, $174'.32825 \pm 0.00089$, and $-5'.62147 \pm 0.0008$.

By inspection the weaker component, that is, the one whose first uncertain place is furthest to the left, is the first number. Retaining this to two uncertain figures would carry it to the fourth decimal place. It will then be useless to retain the other components beyond that place, and we shall have

47.34 89 174.32 83 221.67 72 -5.62 15 216.05 57 [± more than 0'.00 42].

Example 8. — Desired the algebraic sum of

 $47'.34.89 \pm 0.05$ per cent, $174'.32.825 \pm 0.02$ per cent, $-5'.62.147 \pm 0.1$ per cent.

0.05 per cent of 47. is 0.024; 0.02 per cent of 174. is 0.035; 0.1 per cent of 5.6 is 0.00 56. Hence the weakest component is now the second, and this, and consequently the others, should be retained to three decimal places. Thus, we have

47·349 174·328 221.677 -5.621 216.056 [± more than o'.035].

Example 9.—The horse-power, HP, which could safely be transmitted by a wrought-iron shaft of diameter d inches, running at a speed N rotations per minute, the safe shearing load of wrought iron being represented by f, is given by the expression

 $HP = \frac{2\pi^2 d^3 f N}{16.12.33000}$

[Deduced from Lanza's "Applied Mechanics," page 336. The several constants 2, 16, 12, and 33000 would of course be combined into a single constant in a working formula, but they are here left separate for purposes of better illustration.]

To how many places of significant figures should the quantities, result, and various steps of the computation be carried out to assure against a computation error in the result, sensible as compared to one per cent?

Solution. - In this and all similar problems, where the expression consists merely of a number of factors in the numerator and denominator (either or both), without additions or subtractions, the solution of the significant figure problem can be made without any knowledge of the magnitude of the component quantities, such as d, f, N, etc. In this example, as the result is desired to one per cent, according to the rules it should be carried to four places of significant figures. Hence, according to the rule, page xiii, or to Proposition II, page xii, each factor of the whole expression should be carried to four places. In this expression every quantity is a factor, either in the first or a higher power, viz. 2, π^2 , d^3 , f, N, 16, 12, and 33000. Each, therefore, should be carried to four figures. Hence, also, if direct multiplication be employed in the solution, each product and quotient must be carried to four places. If logarithms are used (they should be) four-place tables should be chosen. When a quantity enters as a factor of the nth power this is equivalent to its entering n times as a simple factor or as n separate factors, all with the same percentage error of the same sign. See also note under example 3.

The constants 2, 16, 12, and 33000 do not require to be carried to more places than they are here given because they are complete as they stand, that is, all further figures are known to be zero as a matter of definition or mathematical fact. If either of them had been an experimental constant, that is, determined by measurement, it should have been carried out to four places even if the last figure or two were zero. For instance, if experimental, the 16 should have been written 16.0, 16.00, 16.00, and so on according to the number of places to which it was known (see rule, page xii). Failure ou the part of those who write such formulæ to adhere to this convention, or to indicate in some clear way the degree of accuracy possessed by such constants, is a serious source of annoyance and trouble to those who use them.

As elsewhere it must not be inferred if certain of the quantities, e.g. d or f, in this expression cannot be carried out to this desired number of figures, that consequently the result will not have the accuracy desired in the given case. The outcome of such a condition would merely be that these factors would be liable to introduce more than a safe computation error. For instance, if f were given as 10100 lbs. per square inch, we should have no certainty that it was carried far enough. The presumption would be that it was correct to but three places, and therefore not exact enough. If, however, from a knowledge of the subject we were aware that the best known value was 10110, we should know that the error from using 10100 was only 1 in 1000 or 0.1 per cent, and hence admissible. On the other hand, if we know that the best value was 10050, we should know that the computation error in the result from using 10100 was 0.5 per cent, and hence by no means safe in the above problem.

More complete methods for ascertaining the exact accuracy needed in each component measured quantity in such formulæ, are given in the author's "Precision of Measurements." It is to be remembered that we are now dealing

merely with rules for computation errors, and these are not suited to the other problem. They are intended to secure a safe number of places for the worst case, and would, therefore, impose unduly severe requirements as to the accuracy necessary in the measurement of the components in most cases.

Numerical Substitution. — The numerical expression to be solved if written out would be

$$\begin{array}{l} \underline{2^{\cdot}3.142^{2\cdot}1.364^{3\cdot}10\ 000^{\cdot}300} \\ \underline{16^{\cdot}12^{\cdot}33\ 000} \end{array} \text{ in the ordinary notation;} \\ \\ \underline{2^{\cdot}3.142^{2\cdot}1.364^{3\cdot}\ 10^{4\cdot}3^{\cdot}10^{2}} \\ \underline{1.6^{\cdot}10^{1\cdot}1.2^{\cdot}10^{1\cdot}3.3^{\cdot}10^{4}} \end{array} \text{ in the notation by powers of 10 (page xv);} \\ \\ \underline{2(3.142)^{2}(1.364)^{8}10^{4\cdot}3^{2}} \\ \underline{1.6^{1\cdot}1.2^{1\cdot}3.3^{4}} \end{array} \text{ in the abbreviated notation by powers of 10 (page xv).} \end{array}$$

The first would be worked out in the usual manner by direct multiplication or by logarithms, as shown below.

The second would be worked as follows:

Multiply together the terms other than 10ⁿ of the

numerator, *i.e.*
$$2 \times 3.142^2 \times 1.364^3 \times 3 = 150.3$$

Multiply together the terms other than 10ⁿ of the

denominator, *i.e.*
$$1.6 \times 1.2 \times 3.3 = 6.336$$
 ide numerator by denominator $= 23.72$

Divide numerator by denominator

Add together all indices of powers of 10 in numerator, also in denominator, and subtract the latter from the former. Or, better, add (algebraically) all the indices, reversing the sign of those in the denominator, thus: 4+2-1-1-4=0.

The result is therefore
$$23.72 \cdot 10^9$$
 = 23.72

Note distinctly that all this writing out of the fraction and of the several steps is merely for the purpose of this explanation. In an actual solution such of these operations as are essential to the work would be conducted mentally, the actual multiplication and division alone being written ont.

If the solution were made by logarithms, it might assume either of the two following forms. The first is the usual one, the second shows how the use of the powers of 10 enables us, if we choose, to dispense with writing characteristics in very many places, - a saving of just so much labor. The factor 100 in the second result is, of course, obtained by summing mentally the indices of the factors 10, those in the denominator being taken with reversed sign, as in the preceding paragraph. These indices would not be written out, but taken by direct inspection of the data as originally written.

Denominator.	Usual Method.	Dropping Characteristics.	Numerator.	Usual Method.	Dropping Characteristics.
log 16.	= 1.2041	.2041	log 2.	= 0.3010	.3010
log 12.	= 1.0792	.0792	2 × log 3.142	= 0.9944	.9944
log 33 000.	= 4.5185	.5185	3 × log 1.364	= 0.4044	.4044
log denom.	$= \overline{6.8018}$.8018	log 10 000	-= 4.	•
Ü			log 300.	= 2.4771	·4771
				8.1769	2.1769
				6.8018	.8018
				1.3751	1.3751
			Result,	23.72	23.72.100

Example 10.—The crushing load of a hollow, cast-iron pillar of circular section, with concentric surfaces of diameters D and d as given by Hodgkiuson (Lanza, "Applied Mechanics," page 332) is

$$c = 109 801 \frac{\pi (D^2 - d^2)}{4}$$

Desired to ten per cent the load which a pillar of external and internal diameters 4.032 inches and 2.16 inches, respectively, would carry. How many places of figures should be used in the computation?

Ten per cent results call for three figures in all factors (page xiii). The factors in this expression are 109 801, π , (D^2-d^2) , and 4, each of which should therefore be carried to three figures. The first two should therefore be 110 000 and 3.14. The 4 is a complete number as it stands. $D^2-d^2=4.0^2-2.2^2$ roughly = 16.0 - 4.8 = 11.2. To have three figures, it should therefore be carried to the first decimal place. Then as it is made up of two quantities, one subtracted from the other, each of these should be carried (page xiv) to the decimal place desired in the result, i.e. to the tenths' place. This requires D^2 to contain three figures, 16.0, and hence D should contain three figures (since D^2 consists of the factors $D \times D$), i.e. should be written 4.03 inches. The requirement of one decimal place in d^2 calls for but two figures, 4.8, and hence two figures, 2.2 inches, in d. The numerical expression to be solved would then be

$$c = 110000 \frac{3.14(4.03^2 - 2.2^2)}{4},$$

which would be most easily worked by a simple slide rule, or by direct multiplication.

Example 11. — Desired to o.r per cent the fraction of dry steam in a sample of steam, using the following observations made with the "Barrus Calorimeter" (Peabody's "Themodynamics of the Steam Engine," page 234), the formula being

 $x = \frac{W(q_2 - q_1) + e - w(q - q_3)}{wr},$

where

x = fraction of a mixture which is dry steam.				
W = weight of cooling water				573 5 lbs.
w = weight of condensed water				29.89 lbs.
$t = \text{temperature of steam} \dots \dots \dots$				
$t_1 = \text{initial temperature of cooling water}$				37°.49 F.
$t_2 = $ final temperature of cooling water				83°.84 F.
$t_3 = $ temperature of condensed water				304°.88 F.
$q_3 =$ "heat of liquid" at t_3 , from t_3 and tables	٠.			274.4
$q_2 =$ "heat of liquid" at t_2^0 , from t_2 and tables				51.91 B. T. U.
$q_1 =$ "heat of liquid" at t_1 , from t_1 and tables				
$q =$ "heat of liquid" at t° , from t and tables				
$e = \text{radiation loss during test} \dots \dots$				•
$r = $ latent heat of steam at t° , from tables .				

What number of places of figures should be used throughout?

Solution. — For o.1 per cent the result, and therefore all factors, should have five places of figures (page xiii). The only factors of the whole expression

are the whole numerator, w, and r. They should therefore be carried to five places. Note, however, that w and r are not so given in the data. Whether, however, they are given closely enough must be determined by other means (see remark at foot of page xx). Their product must, however, be carried to five places, and five-place log tables should be employed. The numerator consists of three terms, whose values, roughly, are

$$570(52. - 6.) = 2600.$$
, 120., and $30(288. - 274.) = 420.$
 \therefore numerator = 2600. + 120. - 420. = 2300., roughly.

To have five places the numerator must be carried to one place of decimals, as also must each of its terms. The first term is composed of two factors, W and (q_2-q_1) , each of which must therefore be carried to five places. Then as $q_2-q_1 = 52$. -6 = 46. roughly, it must be carried to the third decimal place. Hence q_2 and q_1 must each be carried to the third decimal place. The third term, in order to extend to the first decimal place, must contain four figures. It consists of two factors, w and $(q-q_3)$, each of which must thus contain four figures. To make the value of $q-q_3$ contain four figures, its numerical value, 14, must be carried to the second decimal place. This would require that both q and q_3 be carried to the second decimal place, or to five figures each.

To summarize, then, putting in an interrogation point wherever a figure is wanting in the data, we have as the numerical expression to be solved

$$x = \frac{573.5^{?}(51.91^{?} - 5.53^{?}) + 120.^{?} - 29.89(287.6^{?} - 274.4^{?})}{29.89^{?} \times 891.2^{?}} = 0.988.$$

Obviously, then, on inspection, although we might carry out the products $W(q_2-q_1)$, $w(q-q_3)$, and wr, each to the necessary five figures, much doubt is cast upon the sufficiency of the data themselves to give the desired 0.1 per cent in the result. The problem would require a detailed study by other methods to decide that point, — the result of which, it may be incidentally asserted, would be adverse.

Note. — It may not be amiss in connection with these problems to call attention to the very large amount of engineering computations in which four, often three (slide rule), places of figures are abundant. In the design of machines and structures, the strength and sizes of parts, such as struts and tie rods, beams, pillars, shafting, etc., and the strains or stresses in them, often cannot, or need not, be fixed upon within an accuracy of one or even many per cent. This limit is fixed by the unreliability of materials or workmanship, or by ignorance of the exact conditions to which the parts may be subjected. Like uncertainties affect many of the data upon which specifications, estimates, and contracts for engineering work are based, and the experimental constants in sundry formulæ. More than three or four places of figures can be indulged in for such work only at an extravagant waste of time. On the other hand it is necessary to discriminate sharply such operations as linear, angular, surface, and sometimes levelling, measurements in surveying and geodetic work where the accuracy may be very high.

LOGARITHMS.

-->≥0≤∞--

Before reading the following pages become familiar with the "Notation by Powers of 10," page xv.

The common or Briggs logarithm of a given number is the exponent of that power to which 10 must be raised to produce the number. Thus, 3 is the common logarithm of 1000, since 10³ = 1000.

To multiply numbers together, add their logarithms. The sum is the logarithm of the desired product.

Proof. — The product $10^a \times 10^b \times \cdots \times 10^m$ is $10^{a+b\cdots +m}$, since powers of the same number may be multiplied together by adding their exponents. Therefore, if $A = 10^a$, $B = 10^b$, ..., $M = 10^m$, $A \times B \times \cdots \times M = 10^{a+b+\cdots +m}$. That is, $a+b+\cdots +m$ is the logarithm of $A \times B \times \cdots \times M$. But a,b,\cdots,m are respectively $\log A$, $\log B$, ..., $\log M$. Hence, $\log (A \times B \times \cdots \times M) = \log A + \log B + \cdots + \log M$.

To divide one number by another, subtract the logarithm of the latter from that of the former. The difference is the logarithm of the quotient.

Proof. — Following the foregoing notation, $A/B = 10^a/10^b = 10^a \times 10^b = 10^{a-b}$. Hence $\log A/B = a-b = \log A - \log B$.

Logarithm of a number of several figures. — As $I = Io^0$ and $Io = Io^1$, the logarithm of I is I and of I is I, and the logarithm of any number greater than I and less than I and the logarithm of any number in the units' place (whether or not followed by a decimal fraction) is less than I, that is, it is a fraction. It is expressed as a decimal fraction.

From the definition of a logarithm it is obvious that the logarithm of any stated power of 10 is the index of the power; *i.e.* log $10^{\pm n} = \pm n$ when $\pm n$ is any number, whole or fractional, positive or neg-

ative. Hence, taking first a specific example, the logarithm of 306.2, being of course the same as the logarithm of its equal, is the same as the logarithm of $3.062 \cdot 10^2$ (see "Notation by Powers of 10," page xv), which is, $\log 3.062 + \log 10^2 = .4860 + 2$, which is usually written 2.4860. The .4860 is found from tables, as shown later.

Similarly, $\log 0.00 \ 306 \ 2 = \log 3.062 \cdot 10^{-3} = \log 3.062 + \log 10^{-3} = .4860 - 3.$, which is usually written either 3.4860 or 7.4860 - 10, as will be further explained.

The logarithm then consists of, or may be separated into, two parts, viz. first, the decimal part called the mantissa, which is the logarithm of the first factor in the above separation; second, the integral part, or whole number, preceding the decimal point, and called the **characteristic** or **index**, which is the logarithm of the second factor $10^{\pm n}$, and which, therefore, is $\pm n$.

Tables of logarithms contain the logarithms of the numbers from 1. to 10., by steps larger or smaller, and to as many decimal places as may be requisite for the accuracy sought in the work in which they are to be employed. But all numbers whatever, from o to ∞ , are one of these numbers 1. to 10. multiplied by some power of ten, *i.e.* by $10^{\pm n}$. For example,

$$4628326 = 4.628326 \cdot 10^6$$
, and $0.03986 = 3.986 \cdot 10^{-2}$.

Hence, the tables enable one, by merely prefixing to the tabular value the proper "characteristic" $\pm n$, to obtain the logarithm of any number whatever, from zero to infinity. The quantity directly given in the table is obviously the mantissa of the desired logarithm, and is therefore always a decimal fraction.

Since any table gives the mantissa to only a specified number of decimal places, it can represent only a correspondingly restricted number of places of significant figures in the original number. It is to be remembered that a change of one unit in the last decimal place of the mantissa corresponds at all points throughout a table to a constant percentage change ("Definitions and Explanations") in the number corresponding. The amount of this change is such that it becomes the proper custom to use logarithm tables giving the mantissa to a number of places equal to the number of significant figures retained in the original quantities. Thus, if the numbers entering into the computation are properly retained to four places of significant figures, a four-place logarithm table should be used in connection with them; if to five significant figures, a five-place table; and so on.

Four-place logarithm tables contain the logarithms to four decimal places of all numbers of three figures from 1.00 to 9.99, and enable one by interpolation to obtain the four-place logarithm of any four-place number from 1.000 to 9.999. By merely prefixing the proper characteristic $\pm n$, therefore, the four-place logarithm of any four-place number from 0 to ∞ is obtained, or, in other words, the four-place logarithm of any number whatever from 0 to ∞ in so far as this is governed by the first four significant figures of the number. Four-place tables should not be employed upon work of an accuracy exceeding one-half of one per cent.

Five-place tables give directly the logarithms to one place further than four-place tables, *i.e.* to five decimal places, for numbers from 1.000 to 9.999, and thence, by interpolation, from 1.0000 to 9.9999. Thus, with the proper characteristic, these tables furnish the logarithms of all five-figure numbers from 0 to ∞ , that is, of any number whatever in so far as this is governed by the first five significant figures of the number. Five-place tables should not be employed in work of an accuracy exceeding one-twentieth of one per cent.

Six-place tables are sometimes arranged with the same steps as five-place, *i.e.* giving directly the logarithm to six decimal places of numbers from 1.000 to 9.999 only. Such tables are of no practical service; for it is entirely useless to employ six-place logarithms in work on five-place numbers, and interpolation for six-place numbers in tables of so large steps as this, besides being less reliable, is more laborious and annoying than is the use of the more bulky tables of smaller steps.

If six-place tables are desired, it is usual to employ, dropping the last place, tables which give directly seven-place logarithms of numbers from 1.0000 to 9.9999 with convenient interpolation tables for the next place. Of these, the Vega tables are among the most convenient, legible, and reliable, being also comparatively inexpensive. The seventh place is very rarely demanded by physical, chemical, or engineering work.

The relative labor in using four, five, and six place tables lies probably between the ratios 1:2:3 and 2:3:4. Assuming the first estimate to hold, the labor is doubled by using a five-place instead of a four-place table, and is increased one-half by using a six instead of a five place table. Hence, as there is no sensible gain from using an excess of places, it is obviously very important to employ a table of the smallest admissible number of places. But, on the other hand, the use of too few places must be guarded against. As an instance of a somewhat dangerous practice may be cited the use of four-place

tables in 0.1 per cent work. This is a not infrequent practice, most common perhaps in chemical computation, and, of course, arising from the exceeding convenience of cards containing four-place logarithms. It will be shown at page xliv, that four places are not sufficient for 0.1 per cent direct computations, and the error if four-place logarithms are used is sensibly the same. The computation error may easily rise to 0.2 or 0.3 per cent with four-place tables even in ordinary computations.

To Find the Logarithms of a Number.

Rule. — Regard the number Q as separated into two factors $q \times 10^{\pm n}$, where q begins in the units' place (see "Notation by Powers of 10," page xv). Find in the tables the logarithm of q. This will be the mantissa of the desired logarithm. Prefix to this the characteristic or index $\pm n$.

A few examples will sufficiently elucidate the process.

Example.—Desired the logarithm to four decimal places of the number 306. Write the number, or, better, merely consider it as if factored in the form $3.06 \cdot 10^2$. In the four-place table, on the line 3.0 and in the column headed 6 will be found .4857, which is $\log 3.06$. Obviously, $\log 10^2 = 2$. Therefore $\log 306 = \log 3.06 + \log 10^2 = .4857 + 2$, which is usually written 2.4857.

Further Examples. Interpolation.—Desired to four decimal places the logarithm of 306.2.

This will lie between the logs of 306 and 307 (and approximately 0.2 of the way), and as the table is not carried out further we must interpolate.

```
For 3.07 we find .4871 Difference = .0014, usually written For 3.06 we find .4857 Interpolation, 0.2 of 14 = 2.8 = 3 ... \log 3.062 = \log 3.062 + \log 10^2 = 2.4860 we must add to the former number 0.214. = 3.
```

The interpolation may always be made by subtracting and multiplying as in this example, but to save the labor, logarithm tables are usually provided with marginal interpolation tables, by the aid of which interpolations may easily be made mentally.

Thus in taking out $\log 3.062$ we find $\log 3.06 = .4857$. By inspection, difference = 14. In the interpolation table headed 14, line 2, stands 3, which is therefore the desired 0.2 of 14. Therefore $\log 3.062 = .4860$. This operation could, of course, be carried out mentally.

The present tables are arranged so that the interpolation tables stand opposite, or nearly so, to the logarithms to which they correspond. This not only gives them a convenient location but enables the computer usually to avoid even the mental subtraction of the successive logarithms to find the difference, since this will, of course, be that at the head of the nearest difference table. Usually also the error introduced by using an interpolation table slightly too large or too small is negligible.

Interpolation becomes more laborious and more liable to error, if conducted mentally, in proportion as the difference is large. is therefore greatest in the first quarter of any logarithm table. But it happens that in physical, chemical, and engineering computations there very often enter correction or reduction factors and other terms of the form (1+a) or 1/(1-a), where a is a decimal fraction rarely as large as o.i. The frequency of such terms calls for a disproportionately large number of the more laborious interpolations. To avoid this labor and increased chance of error, the excellent practice has been adopted in some five-place tables of inserting two pages giving the logarithms from 1.0 to 1.1, by steps only onetenth as large as in the rest of the tables, thus doing away with all interpolation in this most used and most troublesome portion of the table, without adding seriously to its bulk. Such a table has here been prefixed to the five-place table. In the four-place table the same result has been accomplished here, in a manner which is perhaps novel, by the insertion of ten additional lines at the head of the table. The Vega seven-place tables unfortunately lack this feature.

To find Logarithm of a Decimal Fraction.—The procedure is precisely the same as for a whole number. Note that the logarithm of a decimal fraction is always negative, and, conversely, that a negative characteristic always denotes a decimal fraction.

Example. — Desired the log of 0.00 306 2.

```
\begin{array}{c|c} \log 0.00 \ 306 \ 2 = \log 3.062 \cdot 10^{-3} \\ \log & 3.07 = .4871 \\ & 3.06 = .4857 \end{array} | \begin{array}{c|c} \text{Difference} = 14. \\ 0.2 \ \text{of difference} = & 3 \\ \therefore \ \log & 3.062 = .4860 \\ \log & 10^{-3} = -3. \\ \therefore \ \log 0.00 \ 306 \ 2 = .4857 - 3. \end{array}
```

This is written either $\overline{3}.4857$ or 7.4857-10. The latter form is obtained by adding 10 to the characteristic and appending -10 to the whole. The numbers thus appended must in many instances, but not in all, be followed up in the computation in order to correctly locate the decimal point at the close. This is, however, usually very little trouble. The second method is the very general practice and is based on the assertion that when several logarithms are to be added, it is more convenient to have all the characteristics positive. The author is, however, of the opinion that this conventional method serves almost no useful purpose, and that it is better and less troublesome in every way to retain the negative characteristic. It is almost as easy to add a column of numbers in which some are negative, and are therefore subtracted when they are

reached instead of being added, as to add a column in which all are positive. And if the negative characteristic is retained, all care and writing of - 10 or its multiples is avoided. Moreover, the logarithm is complete in itself and shows at once that it is the log of a decimal fraction. These remarks apply not only to the logarithms of ordinary numbers but to the logarithms of the trigonometric functions.

Example of addition where some of the characteristics are negative. Places beyond the first of the mantissa are not added in this illustration.

2.4036	Beginning at the bottom of the columns we have
1.2168	5+3=8+2=10+4=14, write 4;
1.3462	carry $1 + \overline{2} = \overline{1} + 1 = 0 + \overline{1} = \overline{1} + 2 = 1$.
2.5113	Of course the figures printed in heavy type are the only ones pro-
1.4	nounced or mentally enforced.

Examples of some cases where the use of the notation by powers of 10 enable one to dispense with the characteristic in portions of computations are given incidentally at page xxi.

Grouping by Fives in the Tables. — Throughout the entire set of tables, it will be observed, the columns and lines are arranged in groups of five. This not only aids the eye to readily follow any desired line or column, but enables the computer with a little practice to enter a desired column or line without glancing at the number at the top of the column or side of the line, and similarly to read off the number of column or line without glancing off to the marginal figure. Thus the middle column in the second group is 7, the last in the first group is 4, and so on. The practice of working by observed position rather than by the marginal number should be pursued. It reduces fatigue and tends to prevent mistakes.

Indexing at Corners of Tables.— The bold type at the outer corners of the tables shows the contents of the page and its opposite. Thus on the sixth page of the five-place log table, the larger black figure 2 shows that these two pages contain the logs of all the numbers beginning with 2. The smaller black figures, 30, 47, in the margin show that the mantissæ on the two pages extend from 30 to 47 (first two figures). The indexing will be found a material help in rapidly running the page corners under the finger to find either a desired table or a desired figure in a table.

Decimal Point in Logarithm Tables. — It is the almost universal custom to omit the decimal point entirely from logarithm tables. This tends toward compactness, but is by no means essential on that score. The omission causes no serious inconvenience after slight

practice. On the other hand, the retention of the point renders the table complete and strictly self-consistent; that is, any mantissa in the table is then the completely expressed logarithm of the corresponding tabular number. This fact tends materially toward clear comprehension on the part of the beginner or occasional computer. The table is also then perfectly assimilated to the "Notation by Powers of 10," page xv, which affords not only the clearest basis of explanation of mantissa and characteristic, but by far the easiest method of obtaining and following the characteristic in computations. The points do not add necessarily to the bulk of the tables and are no hindrance to their use by computers accustomed to other rules than those here given respecting the characteristic. They are therefore retained in these tables.

Antilogarithm = Number Corresponding. — Given the logarithm to find the "number corresponding," *i.e.* the number of which this is the logarithm. This number is also called the "antilogarithm."

From the Log Tables. -

Example.—To find the antilog of 2.4857, inspect the body of the four-place log table to find the mantissa .4857 (or the next smaller than this if the exact value does not appear). It will be found to lie on line 3.0 and in column 6, and is, hence, the log of 3.06. The characteristic 2 is the log of 10².

:. antilog
$$2.4857 = 3.06 \cdot 10^2$$
 or 306 .

Example.—To find the antilog of 2.4860. In the table this mantissa does not appear exactly, but the next smaller is .4857, whose antilog is 3.06, and the difference from this to the next larger is 14.

```
.4860 - .4857 = 3, and \frac{3}{14} = .2,

.: antilog .4860 is \frac{3}{14} or 0.2 of the way from 3.06 to 3.07,

.: antilog .4860 = 3.062,

also antilog 2. = 10<sup>2</sup>,

.: antilog 2.4860 = 3.062·10<sup>2</sup> or 306.2.
```

The interpolation can be mentally made by the marginal interpolation tables. The tabular difference is 14, and it is desired to know what decimal fraction the difference 3 is of this. Looking down the column under 14 for the number nearest to 3 it is found to be 3 and to stand opposite to 2. \therefore 3 is 0.2 of 14, and antilog .4860 = 3.062.

It will be noticed that in the four-place and five-place log tables those mantissæ have been printed in heavier type in which the first figure changes from one digit to the next. This serves as a guide to the eye in looking for any desired mantissa whose antilog is sought.

From Tables of Antilogarithms.—Some computers prefer to employ a special table for antilogarithms instead of working backward in the ordinary logarithm table as in the preceding example. Whether

the small saving in time effected by this means is an equivalent to the slight additional mental effort incident to the employment in alternation of tables differently arranged, may be questioned. Where many antilogs are to be taken out in succession, the gain is, however, sensible.

Example. — To find by the table of Antilogarithms the antilog 2.4857.

Taking the mantissa first, we find on line .48, column 5, the next smaller number 3.055 with a tabular difference of 7. Hence, antilog .485 = 3.055. But antilog .4857 will be 0.7 of the way from that of .485 to .486. The amount to be added then for interpolation is $0.7 \times 7 = 5$.

antilog
$$.4857 = 3.055 + 0.005 = 3.060$$
, antilog $2.4857 = 3.060 \cdot 10^2 = 306.0$.

Interpolation tables are provided whose method of use is sufficiently obvious.

Cologarithms = Logarithms of Reciprocals. — The colog of any number p is the logarithm of the reciprocal of the number.

It is therefore
$$\log r - \log p = o - \log p$$
.

In substitution in a formula such as $x = \frac{a \cdot b \cdots}{c \cdot d \cdot e \cdots}$, which is the product of several numbers (one or more) divided by the product of several others (one or more), the direct process would be to take the sum of the logarithms of the factors in the numerator, and to subtract from this the sum of the logs of the factors in the denominator.

Example.	$-\log a = 1.2543$	$\log c = 3.8642$
	$\log b = \overline{3.8766}$	$\log d = \overline{5.2121}$
		$\log e = 2.1345$
	Numerator sum = $\overline{1.1309}$	Denominator sum = $\overline{1.2108}$

Subtract denominator sum = 1.2108

Difference $= \overline{3.9201}$

 $x = \text{number corresponding} = 8.320 \cdot 10^{-3}$, or 0.00 8320.

This process may be simplified by employing the colog. It then becomes

$$\log a = 1.2543$$

$$\log b = \overline{3}.8766$$

$$\operatorname{colog} c = \overline{4}.1358$$

$$\operatorname{colog} d = 4.7879$$

$$\operatorname{colog} e = \overline{3}.8655$$

$$\operatorname{Sum} = \overline{3}.9201$$

 $x={\rm number~corresponding}=8.320\cdot 10^{-3}$ This process is thus reduced to the simple addition of a series of numbers.

The colog may be easily taken out of the usual log table by merely looking out the logarithm and subtracting mentally from o.

Example. — Desired the colog of 306.2. Log 306.2 = 2.4860, colog = 3.5140. The use of cologs either with or without a table effects but small saving, except in case a series of substitutions in a given formula are to be made, so that a number of cologs may be looked out in immediate succession.

Table of Cologs.—The table of four-place cologarithms is arranged similarly in every respect to the table of four-place logarithms, and the cologs are taken from it just as logs from their table; noting, however, that the cologs in the table have the characteristic $\overline{\iota}$, and that the differences are subtractive.

Example. — Desired the colog of 306.2. Separate into 3.062·10².

In line 3.0, column 6, colog 3.06
$$= \overline{1.5143} \mid \text{Difference from}$$

 $0.2 \times (-14)$ by difference table $= -3 \mid \text{colog 3.07 is } -14.$
 $0.2 \times (-14)$ by difference table $= \overline{1.5140} \mid \text{colog 3.07 is } -14.$
 $0.2 \times (-14)$ by difference table $= \overline{1.5140} \mid \text{colog 3.062} \mid$

Example. — Desired the colog of 0.00 713 6.

In line 7.1, column 3, is colog 7.13
$$= \overline{1.1469}$$
 Difference is -6 .

colog 7.136 $= \overline{1.1465}$

colog 10⁻³ $= +3$.

colog 0.00 713 6 $= -3$ colog 7.136 $= -3$ $= -3$ 2.1465

Habit in Reading off Numbers or Logarithms. — Time can be economized, strain on the attention reduced, and liability to mistake lessened by an easily acquired habit of grouping and emphasizing the figures in reading off the numbers, the mantissa, and the numbers corresponding (antilogs) in using tables.

A good method of reading is as follows:

In reading a number or antilog pay no regard to the decimal point. Emphasize the first figure; pause, read second and third figures; pause, read remaining figures in groups of three. Thus: Desired the log of 30.62 0472. Read this as 3 06 204 72, i.e. three . . . naught six . . . two naught four . . . seven two.

In reading off a mantissa use no emphasis, but group the first two figures together, and the subsequent figures by threes. Thus, the mantissa .4869 would be read as 4869, *i.e.* forty-eight . . . sixtynine; and .48601 as 48601, *i.e.* forty-eight . . . six naught one.

In taking from the log table the numbers corresponding (antilog) to .48601, it would be read 3062, three . . . naught six . . . two, precisely as under the above rule for reading a number.

These rules apply equally well to four or five place tables. In tables of six or seven places the first three figures of the mantissa are grouped together in printing, and are therefore more conveniently read off together. Also, it is more convenient to read off six-place numbers and antilogs with three figures instead of two in the second group; thus, 781462.

The difference between a number and a mantissa thus read off, whether audibly or mentally, almost precludes the possibility of mistaking one for the other, so that less strict attention will be required to avoid entering the number column of a table with a mantissa, or vice versa. It also avoids the mental or verbal employment of words of instruction. Thus, if a computer reads off 782 he knows, or his assistant using the log tables knows, as soon as the first figure bas been read that the logarithm of the number is desired. Conversely, if he reads off 43 857, the first two figures alone show that the quantity is a mantissa, and that the antilog is required. Thus, no words of instruction need be used throughout an entire computation, and yet no possibility of error need enter.

It is also to be noted that this grouping is consistent with the symmetrical grouping advocated at an earlier page; adapts itself perfectly to the employment of the notation by powers of 10; and coincides with the most convenient grouping in the five-place tables.

Powers and Roots by Logarithms. — If $a = 10^m$ (so that $m = \log a$) then $(a)^n = (10^m)^n$ and $\log (a^n) = n \log a$. Here both m and n may be either positive or negative, and either an integer or a fraction.

Hence, to raise any number, whole or fractional, to any power, integral or fractional, and positive or negative, multiply the logarithm of the number by the exponent of the power of the number.

Since a root is a fractional power, i.e. $\sqrt[n]{a} = a^{\frac{1}{n}}$, the above rule includes the extraction of a root. In the case of decimal fractions the fact that the characteristic is negative while the mantissa is positive, must be regarded. The correct result will be assured if the mantissa and characteristic are separately multiplied (or divided) by the exponent, and the latter result then subtracted from the former, as will be further shown. Certain special procedures will also be described.

The one exception to this is where the index of the power is a single figure and positive. This case takes care of itself without special attention.

It may seem that the use of the negative characteristic thus increases labor over the usual notation explained at the foot of page xxviii. Inspection of examples will show that the only case in which it does so is where the index of the power or root is other than a single digit.

Powers and Roots of Numbers greater than Unity. -

Examples. — Desired the cube of 47.16, i.e. $(47.16)^3$.

log 47.16 = 1.6735
Multiply by 3
log
$$x$$
 = 5.0205 $\therefore x = 1.048 \cdot 10^5$, or 104 800.
Desired $\sqrt[5]{471.6}$.
log 471.6 = 2.6735
Divide by 5
log x = 0.5347 $\therefore x = 3.425$.

Example. — Desired the 2.416 power of 65 830.

log 65 830. =
$$4.8184$$
Multiply by $\frac{2.416}{9.6368}$
 1.92736
 4.818
 2.892
 \therefore log $(65 830)^{2.416} = 11.6413$
 \therefore $(65 830)^{2.416} = 4.378 \cdot 10^{11} = 437.800 \cdot 000 \cdot 000.$

To avoid the direct multiplication of the logarithm by the index of power, when this contains several figures, their logs may be taken. Thus

When the log of a log is thus taken, a table giving at least one place more in the mantissa should be used than would be otherwise needed in order to protect the last place of figures in the result, as is shown in the above example, which is by no means an extreme case. If the quantity is a decimal fraction, the negative characteristic must be separately treated and the result subtracted from the result obtained with the mantissa.

Powers of Decimal Fractions. — Here it is necessary to notice that the logarithm of a decimal fraction is composed of two parts, one positive the other negative. Thus,

$$\log 0.06831 = \overline{2.8345}$$
 or $8.8345 - 10.$

according to the notation chosen. In the first form (the one here recommended) the logarithm consists of a negative characteristic

and a positive mantissa; in the second form it consists of a positive logarithm (both characteristic and mantissa) followed by a negative characteristic.

No new procedure is necessary, but it is essential to be consistent as to sign of each part, and to remember that both parts must be subjected to any operation performed upon either. Whenever the exponent has more than one figure, the negative characteristic and the positive mantissa should be separately multiplied by the index, and the former subtracted from the latter.

Example. — Desired (0.00 4716)4.

log 0.00 4716 =
$$\overline{3}$$
.6735 or 7.6735 - 10
Multiply by 4 4 $\overline{10}$.6940 or $\overline{30}$.6940 - 40, or 0.6940 - 10

... $(0.004716)^4$ = number corresponding, or antilog, = $4.943.10^{-10}$ or 0.00 000 000 049 43.

Example. — Desired (0.00 4716)4.82.

... (0.00 4716)^{4.32} = 2.962·10⁻¹¹.

Roots of Decimal Fractions.—To extract the root of a decimal fraction, divide separately the negative characteristic and the positive mantissa by the index of the desired root. Subtract the former quotient from the latter. The difference will be the logarithm of the desired root. In other words, treat the characteristic separate from the logarithm. This procedure is always the safest to adopt when there is any doubt in the mind of the computer.

Example. — Desired
$$\sqrt[3]{0.06831}$$
.

$$\begin{array}{rcl} & \log & 0.06831 = & \overline{2.8345} \\ & \log & 0.06831 = & \overline{2.8345} \\ & \log & 0.0667 \\ & \log & 0.0667 \\ & \log & \sqrt[3]{0.06831} = & \overline{1.6115} \\ & \sqrt[3]{0.06831} = & 1.088\cdot 10^{-1}. \end{array}$$

A method easily understood by inspection is this: Add to the negative characteristic of the logarithm a number equal to mr where r is the index of the desired root and m is a whole number large enough to make mr larger than or equal to the characteristic, in other words, large enough to extinguish the negative sign of the characteristic. Write this number with a negative sign after the logarithm. Then divide the whole by the index r. The quotient will be the logarithm of the desired root. Usually m=1, i.e. mr=r.

```
Example. — Desired \sqrt[3]{0.06831}. log 0.06 831 = \overline{2}.8345, adding and subtracting 3 gives dividing by 3 gives 0.6115 - 1 = \overline{1}.6115. \sqrt[3]{0.06831} = number corresponding = 4.088\cdot10^{-1} or 0.4088.
```

SQUARES AND SQUARE ROOTS.

It is common to give separate tables of squares and of square roots by which, respectively, the square or square root of any number may be taken out. Inspection, however, shows that the fourplace table of square roots must occupy four pages, the first two containing the numbers from 1.0 to 10., the second two from 10. to 100.; the corresponding roots ranging from 1. to 10.; while a table of squares would occupy but two pages, containing numbers from 1.0 to 10., the squares ranging from 1. to 100. Hence the tabular differences in the table of square roots will be much smaller than in the table of squares. For this reason the table of squares may advantageously be dispensed with, and squares be taken out when desired from the table of square roots, as the numbers corresponding (antilogarithms) are taken out of a table of logarithms. The smallness of the differences makes interpolation easier and more rapid than in a table of squares, and this more than offsets the slight disadvantage of the reverse process of interpolation. The tables at page 30 give square roots to four places. As in the logarithm tables, the numbers in the body of the table are printed in stronger type wherever the second figure changes, in order to assist the eye in the reverse use of the table.

In the table of square roots the insertion of the extra section giving 1.00 to 1.10 to form places direct to avoid interpolation is not called for as in logarithms because the interpolation is very easy, and because the squares of terms of the form $(\mathbf{1} + a)$ are not frequently required.

To find the square of any number, factor the number as described in the "Notation by Powers of 10," page xv. Enter the body of the table with the first factor, and find the corresponding marginal reading and column heading which will be the first three figures of the square. Interpolate for the fourth figure. Square the factor $10^{\pm n}$, which makes it $10^{\pm 2n}$. Multiply together these two squares.

Example. — Desired the square of 34 850.

$$34.850.^2 = (3.485.10^4)^2 = 3.485^2.10^2 \times 4$$

In the table 3.479 (the next smallest value to 3.485) stands in line 12, column 1. The tabular difference is 14, of which our difference (=3.485-3.479=6) is $\frac{6}{11}$, or 0.4 (as may be seen at once from the interpolation table headed 14).

Hence
$$34.850.^2 = 12.14 \cdot 10^8 = 121.400.000$$
.

$$(0.0004981)^2 = 4.981^2 \cdot 10^{-4 \times 2} = 24.83 \cdot 10^{-8} = 0.0000002483$$
.

To find the square root of any number, factor it as in the "Notation by Powers of 10," page xv, except that n must be now an even number, while the first factor must have either one or two digits preceding the decimal point, whichever may be necessary, in order to permit n to be made even.

Find, then, from the table, interpolating if necessary, the square root of the first factor, and multiply this by $ro^{\pm n/2}$, the square root of the second factor; the product is the desired square root.

Example. — Desired the square root of 347.6.

$$(347.6)^{\frac{1}{2}} = (3.476 \cdot 10^2)^{\frac{1}{2}}.$$

In the table, line 3.4, column 7, gives $(3.47)^{\frac{1}{2}} = 1.863$ Interpolations by table gives 0.6 difference = 1

$$(3.476)^{\frac{1}{2}} = \overline{1.864}$$

$$(347.6)^{\frac{1}{2}} = 1.864 \cdot 10^{\frac{1}{2}} = 18.64.$$

Example. — Desired $\sqrt{875}$ 200.

$$\sqrt{87.52 \cdot 10^4} = 9.355 \cdot 10^2 = 935.5.$$

Example. — Desired $(0.05643)^{\frac{1}{2}}$.

$$(5.643 \cdot 10^{-2})^{\frac{1}{2}} = 2.376 \cdot 10^{-1} = 0.2376.$$

Example. - Desired 0.00 006 784.

$$67.84 \cdot 10^{-6} = 8.236 \cdot 10^{-3} = 0.008236.$$

RECIPROCALS.

This table, page 34, contains the reciprocals to four places of numbers from 1. to 9.99, and by interpolation from 1. to 9.999. The reciprocal to four places of any number from zero to infinity is, of course, one of these tabular values multiplied by a suitable power of 10. In this table, the reciprocals of numbers from 1. to 1.100 are given directly in the first ten lines to avoid interpolation in finding the reciprocals of terms of the form (1+a), where a is a small decimal fraction.

N.B.—The approximation 1/(1+a)=(1-a) approx., is frequently employed in computations to avoid dividing by (1+a). This useful approximation, however, must be used with caution. The error from its employment is a^2 ; that is, if a=0.1, the error from multiplying by (1-a) instead of dividing by (1+a) is $0.1^2=0.01$, or 1 per cent; if a=0.03, the error is $0.03^2=0.009$, or nearly 0.1 per cent, and so on.

To find the reciprocal of a number, factor it by the "Notation by Powers of 10," page xv. Find the reciprocal of the first factor by the table and multiply this by the second factor $10^{\pm n}$ with the algebraic sign of its exponent reversed, i.e. by $10^{\pm n}$.

```
Example. — Desired 1/4486, i.e. (4486)^{-1}.
(4486.)^{-1} = (4.486 \cdot 10^{3})^{-1} = (4.486.)^{-1} \cdot 10^{-8}.
In table, line 4.4, col. 8, (4.48)^{-1} = 0.2232
By difference table, 0.6 difference = \frac{-3}{4.486}
Reciprocal of 4.486 = 0.2229
(4486.)^{-1} = (4.486)^{-1} \cdot 10^{-8} = 0.2229 \cdot 10^{-3} = 0.0002229.
```

Example. — Desired
$$1/0.00 327 5$$
.
 $(0.00 327 5)^{-1} = (3.275)^{-1} \cdot (10^{-8})^{-1} = 0.3054 \cdot 10^{8} = 305.4$.

NATURAL SINES, COSINES, TANGENTS, AND COTANGENTS.

It is frequently convenient to have a table giving rough values of the natural trigonometric functions for use in preliminary, check, or approximate computations. The four-place tables of the above four functions cover all ordinary needs. Interpolation can be made in these tables to o°.or by the interpolation tables, or to 1' by mental computation, since the step between successive columns is o°.1, or 6'.

Example. — Desired the natural sine of 37°.75.

On line 37° under heading °.7 is 0.6115. To interpolate for the remaining figure we must add 0.5 of the tabular difference, which, by inspection, is 14. 0.5 × 14 = 7, as can be seen at once in the interpolation table 14 opposite the line 37° .

$$\sin 37^{\circ}.75 = 0.6115 + .0007 = 0.6122.$$

Example. — Desired the natural cotangent of 72°.28.

The cosines and cotangents read upward in the right-hand degree column.

Line 72°, column °.2, gives 0.3211 o.8 of difference (19), to be subtracted,
$$-15$$
 \therefore natural cotangent 72°.28 = 0.3196

All of the tables are used similarly.

LOGARITHMS OF SINES, COSINES, TANGENTS, AND COTANGENTS.

Two sets of tables are given, four-place and five-place, respectively. The four-place tables read to tenths and hundredths of degrees, and are convenient for general rough work and with instruments reading to tenths of a degree. The five-place tables give values to minutes direct. They are adapted to a very large part of the angular measurements ordinarily made in experimental work. Interpolation to half or quarter minutes is easily made in them mentally. A computer working closer than that would naturally employ the Vega, or other conveniently arranged six- or seven-place tables, dropping unnecessary places.

For the reasons stated under the discussion of logarithm tables, page xxviii, the negative characteristic is here retained instead of the more customary 9, with the appended -10.

The use of the tables needs little explanation. The four-place tables are used precisely as the tables of the natural functions. In the five-place tables, for less than 45°, read the tables downwards, using the minute column at the left hand. For angles greater than 45°, read the tables upwards, using the minute column at the right hand of the table, and take care to employ the column-headings given at the foot of the table.

Log sin
$$31^{\circ}$$
 $22' = \overline{1}.71643$.
Log tan 54° $46' = 0.15101$.

SLIDE WIRE RATIOS.

The increasing use of the slide wire in electrical measurements, notably in connection with physical chemistry, renders the table of values of

$$\frac{a}{1000-a}$$

a decided convenience. The work to which the slide wire is thus for the most part employed demands but four-place tables.

To use the table, let a be the reading in millimetres on the slide wire, which is supposed to be one metre long with millimetre subdivision, or of any other length with division into thousandths. Find the first two figures of a in the first column, and run out on this line to the column headed with the third figure. The number there found will give the value of the above fraction, which is the ratio of the length of one section of the wire to the other. If a contains a fourth figure, that is, if read to tenths of a millimetre, interpolation must be made in the usual manner.

Example. - The slider reads 415.6 millimetres.

In line 41 under 5 is found 0.7094. Interpolating by adding 0.6 of the tabular difference 29, gives

$$x = 0.7094 + 0.6 \times 29$$

= $0.7094 + .0017 = 0.7111$.

DEFINITIONS AND EXPLANATIONS

UNDERLYING THE COMPUTATION RULES.

The following statements call for the attention of those only who find unfamilar terms in the foregoing rules.

A Digit is any one of the ten characters 1, 2, 3, 4, 5, 6, 7, 8, 9, o.

A Significant Figure is any digit used to denote or signify the amount of the quantity in the place in which it stands. Thus zero may be a significant figure when it is written not merely to locate the decimal point, but to indicate that the quantity in the place in which it stands is known to be nearer to zero than to any other digit.

For example, if a distance has been measured to the nearest fiftieth of an inch and found to be 205.46 inches, all five of the figures, including the zero, are significant. And similarly if the measurement had shown the distance to be nearer to 205.40 than to 205.41 or to 205.39 the *final zero* would be also significant, and *should invariably be retained*, since its presence serves the most useful purpose of showing that this place of figures had been measured as well as the rest. If in such a case the quantity had been written 205.4 instead of 205.40, the inference would be drawn either that the hundredths of an inch had not been measured, or that the person who wrote the number was ignorant or careless of the proper numerical usage. Failure to follow this simple rule is a common source of annoyance and uncertainty.

A zero when used merely to enable the decimal point to be retained is of course not a significant figure in the above sense. E.g. If the distance were measured as 286. centimetres within \pm 1 centimetre, it might be retained as 2.86 metres, or 0.00 286 kilometres, or 2860. millimetres. In this case neither of the zeros would be significant.

From this last example it is obvious that when the first zero, or zeros, precede the decimal point, they fail to indicate intrinsically whether or not they are significant. E.g. The number 2860. millimetres or 28 600. millimetres, standing apart from explanatory context, would afford no clew to whether the last place, or the last two places, had been measured. In writing such a number, therefore, whenever it is desirable to convey this information some statement of the reliability of the quantity must be appended. This is usually done by writing after the number $\pm a$ where a is a number, of two significant figures only, representing the estimated measure of the accuracy or unreliability of the result. (See later.)

Places of Figures are the places in which figures stand in the number as actually written. Places of significant figures are those in which significant figures stand. These two terms being merely, although not actually, identical, are often used interchangeably.

Example.—426 o18. has six places of figures and of significant figures 3 479 100. has seven places of figures, but whether its number of places of significant figures is more than five is indeterminate. 0.02 7680 has seven places of figures with five places of significant figures. 2.7680·10⁻² has five places of figures and five significant figures.

Places of Decimals. — These, of course, are the places following the decimal point as the number happens to be written. E.g. 0.02 768 0 has six decimal places. 2.76 80·10⁻² has four decimal places, although its magnitude is the same as that of the preceding quantity.

From the foregoing six examples it will be seen that the number of decimal places and the number of places of significant figures have no necessary mutual relation.

Accuracy; Reliability. - To know the exact accuracy of a given quantity it would be necessary, of course, to know the true value of that quantity. In the case of a few mathematical constants (such as $\pi = 3.14159265...$) the true value is known, at least far beyond ordinary requirements. But in case of all measurements the same is obviously not true, for if the true value were known. measurements would be unnecessary. Some approximate expression of the accuracy of a measured result can, however, usually be obtained, and is necessary. Sometimes this is afforded by a knowledge of the instrument used and the degree of care employed. Thus, suppose the distance of about 3 feet $6\frac{3}{64}$ inches = 3.5039 feet between two marks to have been carefully once measured with a good foot-rule, it could safely be assumed from our previous knowledge of such work that if a series of these measurements were undertaken, the results would vary from their mean by less than $\pm \frac{1}{32}$ of an inch; also, that the error in the rule itself, and from other unavoidable or unavoided sources, would not on the average materially increase the error of measurement. $=\pm$ 0.0026 ft. would be taken as the estimated measure of accuracy of the result. Instead of expressing the accuracy in units, e.g. inches or feet, it is usually more convenient or intelligible to express it as a fraction; or, better still, in percentage. Thus, the foregoing will be

$$\pm \frac{0.0026}{3.5} = \pm 0.00 \text{ o74}, i.e. \frac{74}{100000}, \text{ or } 100 \left(\pm \frac{0.0026}{3.5}\right) = \pm 0.074 \text{ per cent.}$$

If in this example the reliability had not been estimated at $\frac{1}{32}$ inch, but if several measurements had been made, and these had been found upon inspection to deviate from their mean by about $\frac{1}{32}$ of an inch, then, other things being the same, the measure of accuracy of any single measurement taken without knowledge of the others would be regarded as $\pm \frac{1}{32}$ inch, or \pm 0.074 per cent.

Mean; Average; Deviation Measure. — When the result is the arithmetical mean or average of several separate measurements of the same quantity, its reliability or accuracy is taken to be in proportion to the square root of the number of such observations. Thus, in the last preceding example, if there had been n=9 single observations made, the measure of accuracy of the mean of these would be

$$\pm \frac{1}{3^2} \pm \sqrt{n} = \pm \frac{1}{3^2} = \pm \frac{1}{96} = \pm \text{ 0.010 inch, or } \pm \text{ 0.025 per cent.}$$

The differences of the single observations taken under like conditions from their mean will be called deviations, and their numerical average (i.e. their sum omitting their algebraic sign, divided by their number) will be called the average deviation of the single observation from the mean, and will be denoted by ad. This quantity divided by the square root of n would be called the average deviation of the mean, and will be denoted by AD. It is the average amount by which any one such mean would be found to deviate from the average of a number of such means all taken under like conditions. The term deviation measure will be used in referring to either of these quantities.

Briefly, then, the meaning of the terms may be summarized as follows: By the statement that the accuracy or reliability of a result is of a quoted amount is meant that the deviation measure of this result is estimated or found to be of this stated amount, and that so far as this can be discovered by inspection, no other sources of error exist which affect the result by an amount sensible as compared with this.*

It is essential to bear in mind in connection with all quantities that are the result of measurement that no absolute numerical expression of the accuracy or error is possible; that any expression which is given is usually merely a deviation measure; that is, an approximate average value of the effect of the variable parts of the errors, accompanied by an assurance, expressed or implied, that a study of the discoverable sources of error of the process has been made, and that these have been corrected for or found to be negligible compared to the deviation measure.

In specifying the accuracy desired in the result, it must be understood that merely the converse of this is meant; or, at least, that only the converse is possible of attainment.

Rules for Significant Figures.—The rules are so framed that, barring mistakes, the greatest possible computation error entering into the result of any ordinary computation (e.g. one involving a total of not much exceeding 20 component numbers, steps, or operations, where a rejection error may occur) shall not be sensible compared with the errors of the measurements or data, or shall not sensibly affect the accuracy of the result. They are, therefore, safe rules in the worst possible cases. But in order to be so they are necessarily more than sufficiently stringent for some classes of comparatively rough work, where the infrequent undetected entrance of a computation error two to four times as large as the experimental error would be permissible. For such work one less place of figures may be used, but when the rules are thus relaxed the possible consequence should be borne in mind, and special scrutiny applied to the various stages of the computation, special attention being directed to quantities beginning with 1 or 2.

Rejection Error. — Whenever it becomes necessary to throw off places of figures, a "rejection error" may enter into the result; e.g. suppose that for any reason the last two figures are to be rejected in

24 375 291, 24 375 300.

making it

The rejection error in the new form is evidently +9.

In rejection, the last figure retained is always to be increased by 1 when the rejected figure next it is 5 or over, but remains unchanged if that figure is less than 5.

^{*}For a more extended discussion of this and allied subjects see the author's "Precision of Measurements."

Thus, calling the last place retained the rth place, the limits of the rejection error entering into that place are + 0.5 and - 0.5, and as all amounts between these limits are equally likely to occur, the average rejection error in the long run will be 0.25 in the rth place.

Law and Amount of Accumulated Rejection Error. - Let the last place of significant figures retained in a number, e.g. the fourth, fifth, etc., be called the rth place. Then the error entering from rejection of figures beyond the rth will be at most ± 5 in the (r+1) place, and any error between these limits. + 5 and - 5 in the (r+1) place, will be equally likely to occur in any given case, and therefore will be of equal frequency in the long run. The average rejection error in any considerable number of rejections will therefore be ± 2.5 in the (r+1) place. If then in direct processes of multiplication, division, evolution, or involution (separate or combined) each factor, product, and quotient in the operation be carried out to the same number r of places, what will be the accumulated fractional rejection error if n such rejections are made during the entire operation? This error we shall call for brevity the computation error, or simply the rejection error. This question might easily be answered in a form giving the average accumulated error, but we are at present concerned chiefly with the maximum possible error, since our object is to frame rules which will reduce the worst possible computation error to negligible dimensions. maximum computation error would arise when every single rejection error was 5 in the (r + 1) place, and all had the same sign; and this would be the greatest fraction of the final result when that result and all the factors (and therefore all the intermediate products, quotients, etc.) began with 1 and had o in the other places, i.e. were each 10^{r-1} with the decimal point wherever it might happen to stand. If there were n of these factors, products, quotients, etc., at which rejections were made, the maximum possible computation error in the result would, therefore, be $n \times 5$ in the (r+1) place, and the fractional error would be $5n/10^r$. Since this maximum error would be exceedingly rare unless n were very small, and any approaching one-half of it would be very rare, we may properly assume that our rules will be sufficiently stringent if we allow this maximum error to have the same magnitude as the desired accuracy in the result as expressed on the basis of the precision measure, or deviation measure, explained at page xlii. To determine most simply what number r of places this limitation would call for in the processes under consideration, let us take specific cases. Suppose the work is desired to possess an accuracy of 1 per cent. Then $5 n/10^r$ must be equal to or less than 1 per cent; i.e. $5 n \ge 1/100$. Hence, we have to solve

$$\frac{5 n}{10^r} = \frac{1}{100}.$$

By inspection, if
$$r = 3$$
, $5n = 10$, $\therefore n = 2$, if $r = 4$, $5n = 100$, $\therefore n = 20$.

But obviously n will almost never be as small as 2, and rarely as large as 20, lying with greatest frequency between 5 and 10 and averaging below 7. This will give a maximum error of 0.0035 or $\frac{1}{3}$ per cent with n=7, r=4, which would be insignificant, and rising to 1 per cent only when n=20. Hence, in work of multiplication, division, etc., where 1 per cent accuracy, or a little better, is desired (remembering that by this we mean only a deviation measure of 1 per cent) r=4 will be an entirely safe but not an excessive value; that is, the reten-

tion of four significant figures throughout will insure entirely sufficient freedom from computation error in every case when the number of rejections is less than the very unusual total of about 20, and fewer places would not be warranted. Similarly five places will suffice for work to 0.1 per cent, i.e. better than 1 per cent, but not much better than 0.1 per cent; six places for work of 0.01 per cent, and so on.

As to relaxation of the rules in special cases, it is evident that but little can be safely done. The maximum error with n=7, r=4, will be 0.35 per cent, and an error of $\frac{1}{3}$ of this, say, of 0.1 per cent, will not be of very uncommon occurrence. In fact, with only two rejections the error might be 0.1 per cent. Hence, four places cannot be considered as safe to 0.1 per cent, even for short computations. Four places might properly enough be used in short computations up to $\frac{1}{3}$ per cent. Similar statements of course hold for the other rules.

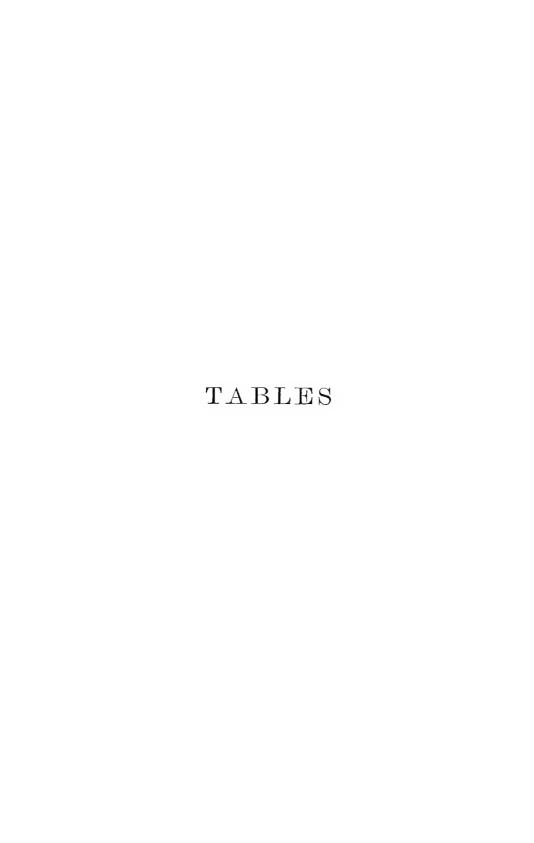
When logarithms are used for multiplication, division, etc., tables should be used giving the mantissa to the same number of places of figures as required by the foregoing rules for direct multiplication and division. Hence, one would employ four-place tables for 1 per cent work, five-place tables for 0.1 per cent work, and so on. The numbers, antilogs, and mantissæ should all be carried out to the same number of places. This conforms to the customary and only convenient practice.

This rule is based primarily on the fact, next to be shown, that under them the maximum computation error in the use of logarithms arises chiefly from the rejection in the numbers and antilogs themselves and not sensibly from the rejected places in the logarithms. In logarithms, a change of the rth figure by 1 produces the same fractional error in the antilog whatever its value, viz. 2.4/10, as may be seen easily by inspection of tables. Hence, as the maximum rejection error in the tabular value of a logarithm is 5 in the (r + 1) place of the mantissæ, which may be doubled by the process of interpolating, the maximum fractional error in a result due to the maximum rejection error in any mantissa is $2.4/10^r$. But if only r places are retained in the number or antilog, the maximum error in it due to rejection of its further places is 5/10, compared to which 2.4/10" is negligible. Hence, as the number of rejections from number and antilog together is usually about the same as from mantissæ, the accumulated error will be due almost wholly to the rejections from the numbers and antilogs. And of these rejections there will ordinarily be about as many if the computation is carried ont by logarithms as if by direct multiplication or division. The above rule is thus justified.

In addition or subtraction the maximum rejection error will be obviously 5n in the (r+1) place. Under the above stated rule that the weakest quantity shall be carried to four significant figures (or two uncertain places) for 1 per cent work, the smallest value of the deviation measure or uncertainty of the result will be 10 in the rth place, which is 100 in the (r+1) place. Hence,

$$5 n \ge 100$$
. .. $n = 20$.

The maximum accumulated error would then attain the size of the smallest deviation measure, *i.e.* the worst possible case would occur, only when the number of rejections was as great as twenty. Hence, the rule of four places for 1 per cent work, five for 0.1 per cent work, and so on, as before given, is sufficient.



FOUR PLACE LOGARITHMS.

LOGS. 4 PL.

No.	0	I	2	3	4	5	6	7	8	9	INTERPO TASI	
1.00	.0000	.0004	.0009	.0013	.0017	.0022	.0026	.0030	.0035	.0039	38 36	34 32
.01	0043	0048	0052	0056	0060	0065	0069	0073	0077	0082	4 4	3 3
.02	0086	0090	0095	0099	0103	0107	0111	0116	0120	0124	8 7	76
.03	0128	0133	0137	0141	0145	0149	0154	o1 58	0162	0166	11 11	
.04	0170	0175	0179	0183	0187	0191	0195	0199	0204	0208	15 14	14 13
1.05	.0212	.0216	.0220	.0224	.0228	.0233	.0237	.0241	.0245	.0249	19 18	17 16
.06	0253	0257	0261	0265	0269	0273	0278	0282	0286	02 90	23 22	20 19
.07	0294	0298	0302	0306	0310	0314	0318	0322	0326	0330	27 25	
.08	0334	0338	0342	0346	0350	0354	0358	0362	• .	0370	30 29	•
.09	0374	0378	0382	0386	0390	0394	0398	0402	0406	0410	34 32	31 29
1.0	.0000	.0043	.0086	.0128	.0170	.0212	.0253	.0294	.0334	.0374	30 28	26 24
1.	0414	0453	0492	0531	0569	0607	0645	0682	0719	O755	3 3	3 2
.2	0792	0828 1173	0864 1206	0899	0934	0969	1004	1038,		1106	6 6	5 5
·3 ·4	1461	1492	1523	1239	1271 1584	1303 1614	1335	1367	1399	1430	9 8	8 7
	1 .						1644	1673	1703	1732	12 11	
1.5	.1761	.1790	.1818	.1847	.1875	.1903	.1931	.1959		▶.2014	15 14	
.6	2041	2068	2095	2122	2148	2175	2201	2227	2253	2279	18 17	
.7 .8	2304	2330	2355 2601	2380 2625	2405 2648	2430	2455	2480	2504	2529	21 20	
.9	2788	2577 2810	2833	2856	2878	2672	2695	2718	2742	2765	24 22	-
	1			-		2900	2923	2945	2967	2989	27 25	_
2.0	.3010	.3032	.3054	.3075	.3096	.3118	.3139	.3160	.3181	.3201	4	18 16
I.	3222	3243	3263	3284	3304	3324	3345	3365	3385	3404	2 2	2 2
.2	3424	3444	3464	3483	3502	3522	3541	3560	3579	3598	4 4	4 3
•3	3617	3636	3655	3674	3692	3711	3729	3747	3766	3784	7 6	5 5
.4	3802	3820	3838	3856	3874	3892	3909	39 2 7	3945	3962	98	76
2.5	-3979	-3997	.4014	.4031	.4048	.4065	.4082	.4099	.4116	.4133	11 10	98
.6	4150	4166	4183	4200	4216	4232	4249	4265	4281	4298	13 12	
.7	4314	4330	4346	4362	4378	4393	4409	4425	4440	4456	15 14	
.8	4472	4487	4502	4518	4533	4548	4564	4579	4594	4609	18 16	
.9	4624	4639	4654	4669	4683	4698	4713	4728	4742	4757	20 18	•
3.0	·4771	.4786	.4800	.4814	.4829	.4843	.4857	.4871	.4886	.4900	15 14	
I.	4914	4928	4942	4955	4969	4983	4997	5011	5024	5038	2 I	1 1
.2	5051	5065	5079	5092	5105	5119	5132	5145	5159	5172	3 3	
•3	5185	5198	5211	5224	5237	5250	5263	5276	5289	5302	5 4	4. 4
٠4	5315	5328	5340	5353	5366	5378	5391	5403	5416	5428	6 6	5 5
3.5	-5441	•5453	.5465	.5478	.5490	.5502	.5515	·5527	.5539	·5551	8 7	7 6
.6	5563	5575	5587	5599	5611	5623	5635	5647	5658	5670	9 8	8 7
.7	5682	5694	5705	5717	5729	5740	5752	5763	5775	5786	11 10	9 8
.8	5798	5809	5821	5832	5843	5855	5866	5877	5888	5899	12 11	
.9	5911	5922	5933	5944	5955	5966	5977	5988	5999	6010	14 13	
4.0	.6021			.6053		.6075			.6107	•	11 10	9 8
I,	6128	6138	6149	6160	6170	6180	6191	6201	6212	6222	II	II
.2	6232	6243	6253	6263	6274	6284 6385	6294	6304	6314	6325	.2 2	2 2 3 2
•3	6335	6345	6355 6454	6365 6464	6375	6385 6484	6395 6493	6405	6415	6425	3 3	~
-4	6435	6444			6474			6503	6513	6522	4 4	4 3
4.5	.6532	.6542	.6551	.6561	.6571	.6580	.6590	.6599	.6609	.6618	6 5	5 4
.6	6628 6721	6637	6646	6656	6665	6675	6684	6693	6702	6712	7 6	5 5 6 6
		6730	6739	6749	6758	6767	6776	6785	6794	6803	8 7	
.7	1					68==	6866	68	688.	6800	0 8	7 6
.7 .8 .9	6812 6902	6821 6911	6830 6920	6839 6928	6848 6937	6857 6946	6866 6955	6875 6964	6884 6972	6893 6981	98	7 6 8 7

FOUR PLACE LOCARITHMS.

4 PL. LOGS.

No.	О	I	2	3	4	5	6	7	8	9	INTER TA	POLAT BLES	
5.0	.6990	.6998	.7007	.7016	.7024	.7033	.7042	.7050	.7059	.7067	9	8	7
1.	7076	7084	7093	7101	7110	7118	7126	7135	7143	7152	I		1
.2	7160	7168	7177	7185	7193	7202	7210	7218	7226	7235	2	2	1
•3	7243	7251	7259	7267	7275	7284	7292	7300	7308	7316	3		2
•4	7324	7332	7340	7348	7356	7364	7372	7380	7388	7396	4	3	3
5.5	.7404	.7412	.7419	.7427	·7435	·7443	·745I	·7459	.7466	·7474	5	4	4
.6	7482	7490	7497	7505	7513	7520	7528	7536	7543	7551	5		4
•7	7559	7566	7574	7582	7589	7597	7604	7612	7619	7627	6		5
.8	7634	7642	7649	7657	7664	7672	7679	7686	7694	7701	7		6
.9	7709	7716	7723	7731	7738	7745	7752	7760	7767	7774	8	•	6
6.0	.7782		.7796	.7803	.7810	.7818	.7825	.7832	.7839	.7846	7		6
.I	7853	7860	7868	7 ⁸ 75	7882	7889	7896	7903	7910 7980	7917 7987	I		I I
.2	7924	7931 8000	7938 8007	7945 8014	7952 8021	7959 8028	7966 8035	7973 8041	8048	79°7 8055	2		2
•3	7993 8062	8069	8075	8082	8089	8096	8102	8109	8116	8122	3		2
4		-	.8142	.8149	.8156	.8162	.8169	.8176		.8189	1		
6.5	.8129	.8136 8202	8209	8215	8222	8228	8235	8241	8248	8254	4		3
.6	8195 8261	8267	8274	8280	8287	8293	8299	8306	8312	8319	5		4 4
·7· .8	8325	8331	8338	8344	8351	8357	8363	8370	8376	8382	6		5
.9	8388	8395	8401	8407	8414	8420	8426	8432	8439	8445	6		5
		.8457	8462	.8470	.8476	.8482	.8488	.8494	.8500	.8506	6		5
7.0	.8451	8519	8525	8531	8537	8543	8549	8555	8561	8567	1 1		1
.I .2	8573	8579	8585	8591	8597	8603	8609	8615	8621	8627	ı		ī
-3	8633	8639	8645	8651	8657	8663	8669	8675	8681	8686	2		2
.4	8692	8698	8704	8710	8716	8722	8727	8733	8739	8745	2		2
7.5	.8751	.8756	.8762	.8768	.8774	.8779	.8785	.8791	.8797	.8802	3		3
.6	8808	8814	8820	8825	8831	8837	8842	8848	8854	8859	4		3
.7	8865	8871	8876	8882	8887	8893	8899	8904	8910	8915	4		4
.8	8921	8927	8932	8938	8943	8949	8954	8960	8965	8971	5		4
•9	8976	8982	8987	8993	8998	9004	9009	9015	9020	9025	5		5
8.0	.9031	.9036	.9042	.9947	.9053	.9058	.9063	.9069	.9074	.9079	6		5
.I	9085	9090	9096	9101	9106	9112	9117	9122	9128	9133	1		I
.2	9138	9143	9149	9154	9159	9165	9170	9175	9180	9186	I		I
-3	9191	9196	9201	9206	-	9217	9222	9227	9232 9284	9238	2 2		2
•4	9243	9248	9253	9258	9263	9269	9274	9279		9289	ŀ		
8.5	.9294		.9304	.9309		.9320	.9325	.9330	•9335	.9340	3		3
.6	9345	9350	9355	9360	9365	9370	9375 9425	9380	9385	9390 9440	4		3 4
·7 .8	9395	9400	9405	9410 9460	9415 9465	9420 9469	9425	9430 9479	9435 9484	9440	5		4
.8	9445 9494	9450 9499	9455 9504	9509	9513	9518	9523	9528	9533	9538	5		5
		9547			.9562	.9566	.9571		.9581	.9586	5		4
9.0	9590	9547	9600	·9557 9605	9609	9614	9619	9624	9628	9633	ı		0
.2	9638	9595	9647	9652	9657	9661	9666	9671	9675	9680	I		I
•3	9685	9689	9694	9699	9703	9708	9713	9717	9722	9727	2		1
-4	9731	9736	9741	9745	9750	9754	9759	9763	9768	9773	2		2
9.5	.9777		9786	.9791	.9795	.9800	.9805	.9809	.9814	.9818	3		2
.6	9823	9827	9832	9836	9841	9845	9850	9854	9859	9863	3		2
.7	9868	9872	9877	9881	9886	9890	9894	9899	9903		4		3
.8	9912	9917	9921	9926	-	9934	9939	9943	9948		4		3
.9	9956	996 1	9965	9969	9974	9978	9983	9987	9991	9996	5		4

FOUR PLACE ANTILOGARITHMS. ANTILOGS. 4 PL.

Mant.	o	I	2	тн с 3	4 4	л р т 5	н s. 6	7	8	9	INTERPO TABLE	
.00	1.000	1.002	1.005	1.007	1.009	1.012	1.014	1.016	1.019	1.021	2	3
.01			=	1.030				1.040			0	0
.02	_			1.054				1.064			0	I
.03		_		1.079		1.084	1.086	1.089	1.091	1.094	1	1
.04			-	1.104				1.114			1	I
.05			1.127		1.132			1.140			1	
.06				1.156		1.161	1.150	1.167	1.143	1.140	1	2
.07				1.183		1.180	1.104	1.194	1.109	1.172	1 1	2
.08				1.211		1.216	1 210	1.222	1.19/	1.199	2	2
.09				1.239		1.245	1.247	1.250	1.253	1.256	2	3
.10	1.250	1.262	1.265	1.268	1.271			1.279		_	3	4
.11	1.288	1.201	1.204	1.207	1.300	1.303	1.306	1.309	1.202	1.205	1	0
.12	1.318	1.321	1.324	1.327	1.330		1 227	1.340	1 242	1.315	ı	
.13				1.358		1.265	T 268	1.340	1 274	1.377	1 1	I
.14	1.380	1.384	1.387	1.390	1.303	1.306	1.400	1.403	1.406	1.3//: 1.400	1 1	I
		_										2
.15				1.422		1.429	1.432	1.435	1.439	1.442	2	2
.16					1.459	1.402	1.466	1.469	1.472	1.476	2	2
.17				1.489		1.496	1.500	1.503	1.507	1.510	2	3
.18					1.528	1.531	1.535	1.538	1.542	1.545	2	3
.19	1.549	1.552	1.556	1.560	1.563	1.567	1.570	1.574	1.578	1.581	3	4
.20					1.600	1.603	1.607	1.611	1.614	1.618	3 4	5
.21	1.622	1.626	1.629	1.633	1.637	1.641	1.644	1.648	1.652	1.656	0 0	1
.22	1.660	1.663	1.667	1.671	1.675	1.679	1.683	1.687	1.690	1.694	II	I
.23	1.698	1.702	1.706	1.710	1.714	1.718	1.722	1.726	1.730	1.734	11.	2
.24				1.750		1.758	1.762	1.766	1.770	1.774	I 2	2
.25	1.778	1.782	1.786	1.791	1.795	1.799	1.803	1.807	1.811	1.816	2 2	3
.26	1.820	1.824	1.828	1.832	1.837			1.849			2 2	3
.27	1.862	1.866	1.871	1.875	1.879	1.884	1.888	1.892	1.897	1.901	2 3	4
.28	1.905	1.910	1.914	1.919	1.923	1.928	1.932	1.936	1.941	1.945	2 3	4
.29					1.968			1.982			3 4	5
.30	1.995	2,000	2.004	2.009	2.014	2.018	2.023	2.028	2.032	2.037	4 5	6
.31		_			2.061			2.075			ОІ	I
.32	_		-	-	2.109			2.123			1 1	1
•33				2.153	- 1			2.173			I 2	2
•34				2.203		2,213	2.218	2,223	2.228	2.234	2 2	2
-35				2.254				2.275			2 3	3
.36	-	-	-	2.307	-			2.328			2 3	4
•37					2.366			2.382				4
.38					2.421			2.438				5
•39	2.455	2.460	2.466	2.472	2.477	2.483	2,489	2.495	2.500	2.506	4 5	5
.40	2.512	2.518	2.523	2.529	2.535	2.541	2.547	2.553	2.559	2.564	567	8
.4I						2.600					III	I
.42	2.630	2.636	2.642	2.649	2.655			2.673			111	
·43	2.692	2.698	2.704	2.710	2.716	2.723	2.729	2.735	2.742	2.748	2 2 2	
-44				2.773				2.799			2 2 3	3
-4 5				2.838		2.851					3 3 4	
.46				2.904		2.917	2.924	2.931	2.938	2.944	3 4 4	
-47	2.951	2.958	2.965	2.972	2.979	2.985	2.992	2.999	3.006	3.013	4 4 5	6
.48	3.020	3.027	3.034	3.041	3.048	3.055	3.062	3.069	3.076	3.083	456	6
•49	3.090	3.097	3.105	3.112	3.119	3.126	3.133	3.141	3.148	3.155	5 5 6	7

FOUR PLACE ANTILOGARITHMS.

4 PL. ANTILOGS.

				тно	U S	AND	гн 8.				INTERPOLA.
Mant.	0	I	2	3	4	5	6	7	8	9	TABLES.
.50	3,162	3.170	3.177	3.184	3.192	3.199	3.206	3.214	3.221	3.228	789
.51	3.236	3.243	3.251	3.258	3.266	3.273	3.281	3.289	3.296	3.304	1 1 1
.52	3.311		3.327			3.350			3.373	3.381	I 2 2
•53	3.388	3.396	3.404	3.412	3.420	3.428	3.436	3.443	3.451	3.459	2 2 3
•54	3.467	3.475	3.483	3.491	3.499	3.508	3.516	3.524	3.532	3.540	3 3 4
•55	3.548	3.556	2.565	3.573	3.581	3.589	3.597	3.606	3.614	3.622	4 4 5
·55 .56	3.631		3.648		3.664	3.673	3.681		3.698	3.707	4 5 5
•57			-	3.74I	3.750	_			3.784		5 6 6
·5/ ·58	3.802			3.828	3.837	3.846	3.855	3.864	3.873	3.882	6 6 7
.59	3.890	3.899		3.917	3.926	3.936	3.945	3.954	3.963	3.972	6 7 8
			-		•		-	-			, ,
.60	3.981		3.999						4.055	4.064	9 10 11 12
.61			4.093		•	•			4.150		1111
.62			4.188				-		4.246		2 2 2 2
.63			4.285		4.305				4.345		3 3 3 4
.64	4.365	4.375	4.385	4.395	4.406				4.446		4 4 4 5
.65	4.467	4.477	4.487	4.498	4.508	4.519	4.529	4.539	4.550		5 5 6 6
.66	4.571	4.581	4.592	4.603	4.613	4.624	4.634	4.645	4.656	4.667	5 6 7 7
.67			4.699						4.764	4.775	6 7 8 8
.68	4.786	4.797	4.808	4.819	4.831			4.864	4.875	4.887	78910
.69	4.898	4.909	4.920	4.932	4.943	4.955	4.966	4.977	4.989	5.000	8 9 10 11
.70	5.012	5.023	5.035	5.047	5.058	5.070	5.082	5.093	5.105	5.117	12 13 14 15
.71	5.129	5.140	5.152						5.224		1112
.72	5.248	5.260	5.272	5.284	5.297	5.309	5.321	5.333	5.346	5.358	2 3 3 3
·73	5.370	5.383	5.395	5.408	5.420	5.433	5.445		5.470	5.483	4 4 4 5
∙74	5.495	5.508	5.521	5.534	5.546	5.559	5.572	5.585	5.598	5.610	5 5 6 6
∙75	5.623	5.636	5.649	5.662	5.675	5.689	5.702	5.715	5.728	5.741	6778
.76	5.754	5.768		5.794				5.848		5.875	7889
.77	5.888		5.916	5.929	5.943				5.998	6.012	8 9 10 11
.78	6.026	6.039	6.053	6.067	6.081	6.095	6.109	6.124	6.138	6.152	10 10 11 12
∙79	6.166	6.180	6.194	6 .20 9	6.223	6.237	6.252	6.266	6.281	6.295	11 12 13 14
.80	6.310	6.324	6.339	6.353	6.368	6.383	6.397	6.412	6.427	6.442	16 17 18 19
.81			6.486		6.516	6.531	6.546	6.561	6.577	6.592	2 2 2 2
.82	6.607	6.622	6.637	6.653	6.668	6,683	6.699	6.714	6.730	6.745	3 3 4 4
.83	6.761	6.776	6.792	6.808	6.823	6.839	6.855	6.871	6.887	6.902	5 5 5 6
.84	6.918	6.934	6.950	6.966	6.982	6.998	7.015	7.031	7.047	7.0 63	6778
.85	7.079	7.096	7.112	7.129	7.145	7.161	7.178	7.194	7.211	7.228	8 9 9 10
.86	7.244	7.261	7.278	7.295	7.311	7.328	7.345	7.362	7.379	7.396	10 10 11 11
.87	7.413	7.430	7.447	7.464	7.482	7.499		7.534	7.551	7.568	11 12 13 13
.88	7.586	7.603	7.621	7.638	7.656	7.674	7.691	7.709	7.727	7.745	13 14 14 15
.89	7.762	7.780	7 .7 98	7.816	7.834	7.852	7.870	7.889	7.907	7.925	14 15 16 17
.90	7.043	7.962	7.980	7.998	8.017	8.035	8.054	8.072	8.091	8.110	20 21 22 23
.91	8.128	8.147	8.166	8.185	8.204	8.222	8.241	8.260	8.279	8.299	2 2 2 2
.92			8.356						8.472		4 4 4 5
.93			8.551						8.670		6677
٠94			8.750						8.872		8899
·95	•	• -	8.954						9.078		10 11 11 12
.96			9.162						9.290		12131314
.97			9.376			-		_	9.506		14 15 15 16
.98			9.594						9.727		16 17 18 18
.99			9.817						9.954		18 19 20 20
l											

FOUR PLACE COLOGARITHMS

COLOGS, 4 PL.

NOTE THE CHARACTERISTIC T.

No.	0	I	2	3	4	5	6	7	8	9	INTERPOLATION TABLES.
1.00		ī.9996 ī	1.9991	ī.9987	1.9983	ī.9978	ī.9974	1.9970	1.9965	ī.9961	
10,	ī.995 7	9953	9948	9944	9940	9935	9931	9927	9923	9918	
.02	9914	9910	9905 9863	9901	9897	9893	9887	9884	9880	9876	
.03 .04	9872 9830	9867 9825	9821	98 5 9	9855 9813	9851 9809	9846 9805	9842 9801	9838 9796	9834 9792	Use the first ten
1.05	1.9788	, ,	-			1.9767	- •	-		•	lines to avoid in- terpolating
.06	9747	9743	9739	9735	9731	9727	9722	9718	9714	9710	from 1.000 to 1.100.
.07	9706	9702	9698	9694	9690	9686	9682	9678	9674	9670	10 1,100,
.08	9666	9662	9658	9654	9650	9646	9642	9638	9634	9630	
.09	9626	9622	9618	9614	9610	9606	9602	9598	9594	9590	
1.0	0.0000					ī.9788			-	•	44-40-36-32
.I .2	9208	9547 9172	9508 9136	9469 9101	943 1 9066	9393 9031	9355 8996	9318 8962	9281 8928	9 245 8894	9 8 7 6
•3	8861	8827	8794	8761	8729	8697	8665	8633	860I	8570	9 8 7 6
.4	8539	8508	8477	8447	8416	8386	8356	8327	8297	8268	18 16 14 13
1.5	ī.8239	1.8210	ī.8182	1.8153	1.8125	ī.8097	ī.8069	1.8041	ī.8013	ī.7986	22 20 18 16
.6	7959	7932	7905	7878	7852	7825	7799	7773	7747	7721	26 24 22 19
.7	7696	7670	7645	7620	7595	7570	7545	7520	7496	747 I	31 28 25 22
.8	7447 7212	7423 7190	7399 7167	7375 7144	7352 7122	7328 7100	7305 7077	7282 7055	7258 7033	7235 7011	35 32 29 26
.9	i '		• •		•	•				•	40 36 32 29
2.0		T.6968						T.6840			-28-26-24-22
I.	6778 6576	6757 6556	6737 6536	6716 6517	6696 6497	6676 6478	6655 6459	6635 6440	6615 6421	6596 6402	3 3 2 2
.2 .3	6383	6364	6345	6326	6308	6289	6271	6253	6234		8 8 7 7
-4	6198	6180	6162	6144	6126	6108	6091	6073	6055	6038	11 10 10 9
2.5	1.6021	ī.6003	ī.5986	ī.5969	ī.5952	1.5935	7.5918	ī.5901		1.5867	14 13 12 11
.6	5850	5834	5817	5800	5784	5768	5751	5735	5719	5702	17 16 14 13
-7	5686	5670	5654	5638	5622	5607	5591	5575	5560	5544	20 18 17 15
.8	5528		5498	5482	5467	5452	5436	5421	5406 5258	5391	22 21 19 18
•9	5376		5346	5331	5317	5302	5287 -	5272 -	_	5243 _	25 23 22 20
3.0		1.5214						1.5129	- :		-18-16-14-12
1,	5086 4948	5072 4935	5058 4921	5045 4908	5031 4895	5017 4881	5003 4868	4989 4855	4976 4841	4962 4828	2 2 I I 4 3 3 2
.2 .3	4815	4802	4789	4776	4763	4750	4737	4724	4711	4698	5 5 4 4
·4	4685	4672	4660	4647	4634	4622	4609	4597	4584	4572	7 6 6 5
3.5	T.4559	ī.4547	ī.4535	ī.4522	ī.4510	ī.4498	ī.4486	ī.4473	ī.4461	ī.4449	9876
.6	4437	4425	4413	4401	4389	4377	4365	4353	4342	4330	11 10 8 7
.7	4318	4306	4295	4283	4271	4260	4248	4237	4225	4214	13 11 10 8
.8	4202 4089	4191 4078	4179 4067	4168 4056	4157 4045	4145 4034	4134 4023	4123 4012	4112	4101 3990	14 13 11 10
•9								•		0,,,	, ,
4.0	ī.3979					7.3925				_	-11-10 -9 -8
I.	3872 3768	3862 3757	3851 3747	3840 3737	3830 3726	3820 3716	3809 3706	3799 3696	3788 3686	3778 3675	2 2 2 2
.2 .3	3665	3655	3645	3635	3625	3615	3605	3595	3585		3 3 3 2
·4	3565	3556	3546	3536	3526	3516	3507	3497	3487		4 4 4 3
4.5	ī.3468	ī.3458	ī.3449 ī	ī.3439	ī.3429	ī.3420	ī.3410	ī.3401	ī.3391		6 5 5 4
.6	3372	3363	3354	3344	3335	3325	3316	3307	3298	3288	7 6 5 5
.7	3279	3270	3261	3251	3242	3233	3224	3215	3206 3116	3197	8 7 6 6
.8	3188 3098	3179 3089	3170 3080	3161 3071	3152 3063	3143 3054	3134 3045	3125 3036	3028	3107 3019	9876
.9	3090	3009	5000	3-1-	J- ~J	J~J +	J-47	J-J-	J-20	J-*7	- , , ,

FOUR PLACE COLOGARITHMS. 4 PL. COLOGS.

No.	0	I	2	3	4	5	6	7	8	9		POLATION ABLES.
5.0	ī.3010	Ī.3002	1.2003	1.2084	ī.2076	ī.2967	ī.2058	1.2050	1.2041	1.2033	-9	-8 -7
0.0 1.	2924	2916	2907	2899	2890	2882	2874	2865	2857	2848	1	1 1
.2	2840	2832	2823	2815	2807	2798	2790	2782	2774	2765	2	2 I
-3	2757	2749	2741	2733	2725	2716	2708	2700	2692	2684	3	2 2
.4	2676	2668	2660	2652	2644	2636	2628	2620	2612	2604	4	3 3
5.5	ī.2596	ī.2588	1.2581	ī.2573	1.2565	1.2557	ī.2549	ĩ.2541	1.2534	1.2526	5	4 4
.6	2518	2510	2503	2495	2487	2480	2472	2464	2457	2449	5	5 4 6 5
.7	2441	2434	2426	2418	2411	2403	2396	2388	2381	2373	6	
.8	2366	2358	2351	2343	2336	2328	2321	2314	2306	2299	7	6 6
.9	2291	2284	2277	2269	2262	2255	2248	2240	2233	2226	8	7 6
6.0	1.2218	1.2211	1.2204			7.2182					-7	-6
.I	2147	2140	2132	2125	2118	2111	2104	2097	2090	2083	1	1
.2	2076	2069	2062	2055	2048	2041	2034	2027	2020	2013	1	I
•3	2007	2000	1993	1986	1979	1972	1965	1959	1952	1945	2	2
•4	1938	1931	1925	1918	1911	1904	1898	1891	1884	1878	3	2
6.5		_	1.1858			1.1838					4	3
.6	1805	1798	1791	1785	1778	1772	1765	1759	1752	1746	4	4
.7	1739	1733	1726	1720	1713	1707	1701 1637	1694	1688 1624	1681 1618	5	4
.8	1675	1669 1605	1662 1599	1656 1593	1649 1586	1643 1580	1574	1630 1568	1561	1555	6	5
.9		_	_			-	_	_	-		"	5
7.0	1.1549					7.1518	_	_	_		-6	-5
1.	1487	1481	1475	1469	1463	1457	1451	1445	1439	1433	I	1
.2	1427	1421	1415	1409	1403	1397	1391	1385	1379	1373	I	I
•3	1367 1308	1361 1302	1 355 1 296	1349 1290	1343 1284	1337 1278	1331	1325 1267	1319 1261	1314 1255	2	2
•4		-	-		•			•			2	2
7·5 .6	1.1249 1192	1.1244	111230	1.1232	11169	ī.1221 1163	1158	11152	11146	1.1190	3	3
.5 •7	1135	1129	1124	1118	1113	1103	1101	1096	1090	1085	4	3
.7 .8	1079	1073	1068	1062	1057	1051	1046	1040	1035	1029	5	4
.9	1024	1018	1013	1007	1002	0996	0991	0985	0980	0975	5	4 5
8.0	ī.0969	ī.0964	T.0958	Ī.0953	ī.0947	1.0942	.0937	1.0931	ī.0926	1,0921	-6	-5
J.J	0915	0910	0904	0899	0894	0888	0883	0878	0872	0867	I	I
.2	0862	0857	0851	0846	0841	0835	0830	0825	0820	0814	I	I
-3	0809	0804	0799	0794	0788	0783	0778	0773	0768	0762	2	2
•4	o757	0752	0747	0742	0737	0731	0726	0721	0716	0711	2	2
8.5	ī.0706	1.0701	ī.0696	1,0691		1.068o		1.0670	ī.0665	ī.066o	.3	3
.6	0655	0650	0645	0640	0635	0630	0625	0620	0615	0610	4	3
•7	0605	0600	0595	0590	0585	0580	0575	0570	0565	0560	4	4
.8	0555	0550	0545	0540	0535	0531	0526	0521	0516	0511	5	4
.9	0506	0501	0496	0491	0487	0482	0477	0472	0467	0462	5	5
9.0	7.0458					1.0434				_	-5	-4
.I	0410	0405	0400	0395	0391	0386	0381	0376	0372	0367	1	0
.2	0362	0357	0353	0348	0343	0339	0334	0329	0325	0320	I	I
•3	0315	0311	0306	0301	0297	0292	0287	0283	0278	0273	2	I
•4	0269	0264	0259	0255	0250	0246	0241	0237	0232	0227	2	2
9.5	1.0223				_	1.0200		_			3	2
.6	0177	0173	0168	0164	0159	0155	0150	0146	0141	0137	3	2
.7	0132 0088	0128	0123	0119	0114	0066	0106	0101	0097	0092 0048	4	3
.8	0044	0039	0079 0035	0074	0070 0026	0000	0001	0057	0009	0004	4	3
.9			~ స్త్రేస	~~ <u>``</u>	5520	5522	5517	0013	5509	5554	5	4

TABLE OF FIVE PLACE LOGARITHMS,

CONTAINING

An Abbreviated Table for One and Two Place Numbers;

A Table for Five Place Numbers from 1.0 to 1.1 Avoiding Interpolation;

A Table for All Four Place Numbers with Interpolation Tables for the Fifth Place.

No.	log.	No.	log.	No.	log.	No.	log.	No.	log.
0	- ∞	2.0	.30 103	4.0	.60 206	6.0	.77 815	8.0	.90 309
1	.00 000	2.1	.32 222	4.I	.61 278	6.1	.78 533	8.1	.90 849
2	.30 103	2.2	.34 242	4.2	.62 325	6.2	.79 239	8.2	.91 381
3	.47 712	2.3	.36 173	4.3	.63 347	6.3	-79 934	8.3	.91 908
4	.60 206	2.4	.38 021	4.4	.64 345	6.4	.80 618	8.4	.92 428
5	.69 897	2.5	·39 794	4.5	.65 321	6.5	.81 291	8.5	.92 942
6	.77 815	2.6	41 497	4.6	.66 276	6.6	.81 954	8.6	. •93 450
7	.84 510	2.7	.43 136	4.7	.67 210	6.7	.82 607	8.7	.93 952
8	.90 309	2.8	.44 716	4.8	.68 124	6.8	.83 251	8.8	.94 448
9	.95 424	2.9	.46 240	4.9	.69 020	6.9	.83 885	8.9	94 939
1.0	.00 000	3.0	.47 712	5.0	.69 897	7.0	.84 510	9.0	.95 424
1.1	.04 1 39	3.1	.49 136	5.1	·7º 757 _.	7.1	.85 126	9.1	.95 904
1.2	.07 918	3.2	.50 515	5.2	.71 600	7.2	.85 733	9.2	.96 379
1.3	.11 394	3.3	.51 851	5.3	.72 428	7.3	.86 332	9.3	.96 848
1.4	.14 613	3.4	.53 148	5.4	.73 239	7.4	.86 923	9.4	.97 313
1.5	.17 609	3.5	.54 407	5.5	.74 036	7.5	.87 506	9.5	.97 772
1.6	.20 412	3.6	.55 630	5.6	.74 819	7.6	.88 081	9.6	.98 227
1.7	.23 045	3.7	.56 8.20	5.7	.75 587	7.7	.88 649	9.7	.98 677
1.8	.25 527	3.8	.57 978	5.8	.76 343	7.8	.89 209	9.8	.99 123
1.9	.27 875	3.9	.59 106	5.9	.77 085	7.9	.89 763	9.9	.99 564

5 PL. LOGS. ABBREV. TAB.

FIVE PLACE LOGARITHMS.

1.0-1.1. LOGS. 5 PL.

	No.	0	1	2	3	4	5	6	7	8	9
.00	1.000	00,000	00.004	.00 009	.00.01.2	.00.017	.00.022	.00 026	.00.030	00.025	00.030
.04	1.000			00 052				00 069			
	.002			00 095			00 108	00 113	00 117	00 121	00 126
1	.003			00 1 39			00 152	00 156	00 160	00 165	00 169
	.004	00 173	00 178	00 182	00 186	.00 191	00 195	00 199	00 204	y 00 208	00 212
	1.005		_	.00 225	_		.00 238	.00 243	.00 247	.00 251	.00 255
	.006			00 268			00 281	00 286	00 290	00 294	00 299
	.007			00 312			00 325	00 329	00 333	00 337	00 342
	.008			oo 355 oo 398			00 308	00 372	00 376	00 381	00 385
	.009	00 309	00 393	00 390	00 402	00 400	00 411	00 415	W419	00 424	00 428
	1.010			,00 441			.00 454	.00 458	.00 462	.00 467	.00 471
	110.			00 484			00 497	00 501	00 505	00 509	00 514
	,012	00 518	00 522	00 527	00 531	00 535	00 540	00 544	00 548	00 552	∞ 557
	,013			00 570			00 582	00 587	00 591	00 595	00 600
	.014			00 612				00 629			
	1.015			.00 655			.00 668	.00 672	.00 677	.00 681	.00 685
	.016	,	_	00 698			00 711	00 715	00 719	00 724	00 728
	.017 .018	. 00 732		00 741				00 758			
	.019			00 826			00 790	00 800 00 843	00 805	00 809	00 813
		0001,	00 022	00 020	00 0 30	00 034					1
	1.020	.00 860	.00 864	.00 869	.00 873	.00 877	.00 881	.00 886	.00 890	.00 894	.00 898
	.021			00 911			00 924	00 928	00 932	00 937	00 941
	.022	1		00 954		-		00.971			
	.023			00 996		_		01 013			
	.024			01 038				01 055		-	
	1.025			.01 081				.01 098			
	.026			01 123 01 166				01 140 01 182			
	.027 .028			01 208			-	OI 225	-		
	.029					01 258		01 267			
								-	-		
	1.030			.01 292				.01 309			
	.031			01 334		_		01 351			
	.032			01 376 01 418				01 393 01 435			
	.034	01 452	01 414	01 460	01 465	01 469		01 477			
				.01 502				.01 519			
	1.035 .036			01 544				01 561			
	037			01 586				01 603			
	.038			01 628				01 645			
	.039		-	_		от 678	or 682	oi 687	01 691	01 695	01 699
			O7 F0 ⁰	01.510	07 = 16	07 520	07.724	01.528	01 777	01 727	01.741
	1.040	.01 703	.01 708	.01 712 01 753	01 758	01 762		.01 728 01 770			
	.041 .042	01 787	01 701	01 795	01 700	01 803		01 812			
	.043			01 837				01 853			
	.044			o1 878				01 895			
	1.045			.01 920				.01 937			
.00	.046	01 953	OI 957	01 961	or 966	01 970		01 978			
.04	.047	01 995	o i 999	02 003	02 007	02 OI I		02 020			
	.048	02 036	02 040	02 044	02 049	02 053	02 057	02 061	02 065	02 069	02 073
	.049	02 078	02 082	02 086	02 090	02 094	02 098	02 102	02 107	02 111	02 115

LOGS. 5 PL. 1.0-1.1.

									0 P	
No.	0	1	2	3	4	5	6	7	8	9
1.050	.02 110	.02 123	.02 127	.02 131	.02 135	.02 140	.02 144	.02 148	.02 152	.02 156
.051		02 164								02 197
.052		02 206							02 235	
.053	1	02 247							02 276	
.054		02 288	_						02 317	
1.055		.02 329	-		-				.02 358	-
.056		02 371							02 399	
.057		02 412							02 440	
.058		02 453		_	_				02 481	
.059					02 506					02 526
1.060	.02 531	.02 535	.02 539	.02 543	.02 547	.02 551	.02 555	.02 559	.02 563	.02 567
.061		02 576				~~			02 604	
.062		02 617								02 649
.063		02 657							02 686	
.064		02 698							02 727	
1.065	ļ.	.02 739					-		.02 768	
.066		02 780							02 808	
.067		02 821							02 849	
.068		02 861							02 890	
.069		02 902							02 930	
1.070	.02 938	.02 942	.02 946	.02 951	.02 955	.02 959	.02 963	.02 967	.02 971	.02 975
.071		02 983							03 011	
.072		03 024							03 052	
.073		03 064							03 092	
.074		03 104								03 137
1.075	l *	.03 145	• •			_		-	.03 173	
.076		03 185				_			03 214	
.077	02 222	03 226	03 220	02 224	02 228				03 254	
.078		03 266							03 294	
.079					03 318					03 338
1.080	.03 342	.03 346	.03 350	.03 354	.03 358	.03 362	.03 366	.03 371	.03 375	.03 379
.081					03 399				03415	
.082		03 427							03 455	
.083		03467							03 495	
.084					03 519				03 535	
1.085	02 542	.03 547	.02 551	.03 555	.03 550	.03 563	.03 567	.03 571	.03 575	.03 570
.086		03 587								03 619
.087					03 639					03 659
.088					03 679					03 699
.089					03 719					03 739
1.090	.03 743	.03 747	.03 751	.03 755	.03 759	.03 763	.03 767	.03 771	.03 775	.03 778
.091	03 782	03 786	03 790	03 794	03 798				03 814	
.092		°03 826							03 854	
.093		03 866							03 894	
.094		03 906							03 933	
1.095	1	.03 945							.03 973	
.096		03 985							04 01 3	
.097					04 036					04 056
.098		04 064								04 096
.099					04 116	04 120	04 123	04 127	04 131	04 135

1. FIVE PLACE LOGARITHMS.

	No.	0	I	2	3	4	5	6	7	- 8	9	INTERPO. TABLES.
	1.00		_	.00 087					.00 303			
30	.01			00 518					00 732 01 157			
	.03			or 368			oi 494	01 536	01 578	01 620	01 662	For log 1.0 to log 1.1
	1.05			.02 202					01 995 .02 407			interpolated values are
ı	.06	02 531	02 572	02 61 2	02 653	02 694	02 735	02 776	02 816	02 857	02 898	given on the preceding
	.07 .08			03 019 03 423			03 141	03 181	03 222	03 262	03 302	two pages.
	.09			03 822			03 941	03 981	03 623 04 021	04 060	03 703	
	1.10			.04 218			،04 336	.04 376	.04 415	.04 454	.04 493	38 36
Ì	.11			04 610 04 999					04 805			4 4
	.13			05 385					05 192 05 576			8 7
	.14			05 767					05 956			15 14
	1.15			.06 145					.06 333			19 18
	.16	06 446	06483	06 521 06 893	06 558	06 595	06 633	06 670	06 707	06 744	06 781	23 · 22
	.17			07 262			07 004	07 041	07 078 07 445	07 115	07 151	27 25 30 29
	.19					07 700						34 32
	1.20					.08 063			.08 171			34 33
	.21					08 422			08 529			3 3
	.22			: 08 707 : 00 061			-09 167	00 049	08 884	00 920	08 955	7 7 10 10
	.24					09 482			09 587			14 13
	1.25	.09 691	.09 726	.09 760	.09 795	.09 830	.09 864	.09 899	.09 934	.09 968	.10 003	17 17
	,26			10 106					10 278			20 20
	.27 .28					10517			10 619 10 958			24 23 27 26
	.29					11 193			11 294			31 30
	1.30					.11 528			.11 628			32 31
	.31					11860			11 959			.3 3 6 6
	·32 ·33					12 189			12´287 12 613			10 9
	•34					12840			12 937			13 12
	1.35			.13 098			.13 194	.13 226	.13 258	.13 290	.13 322	16 16
	.36			13418			13513	13 545	13 577	13609	13 640	19 19 22 22
	·37			13 735					13 893 14 208			26 25
	.39			14 364					14 520			29 28
	1.40	1.14613	.14 644	.14 675	.14 706	.14 737	.14 768	.14 799	.14 829	.14 860	.14 891	30 29
ı	.4I	14 922	14953	14 983	15 014	15 045	15 076	15 106	15 137	15 168	15 198	3 3
	.42	15 229	15 259	15 290 15 594	15 320	15 351	15 685	15 412	15 442 15 746	15 475	15 806	9 9
	·43 ·44	15 836	15 866	15 897	15 927	15 957			16 047			12 12
	1.45	-		.16 197					.16 346			15 15
.00	.46	16 435	16465	16 495	16 524	16 554			16 643			18_17
.30	·47	16 732	10761	16 791 17 085	10 820	10 850			16 938 17 231			2I 20 24 23
	.48 .49	17 319	17 348	17 377	17 406	17 435					17 580	27 26
	.12	-73-7	101	, .,,	• •	,			- -			l

FIVE PLACE LOGARITHMS.

5 PL. LOGS.

										5 F	<u>'L.</u>	LO	gs.
No.	0	I	2	3	4	5	6	7	8	9		ERPO. BLES.	
1.50	.17 609	.17 63	8 .17 667	.17 696	.17 725	.17 754	.17 782	.17811	.17 840	.17 869	29	27	.00
.51	17898	1792	6 17 955	17 984	18 013	18041	18 070	18 099	18 127	18 156	3		.30
.52	18 184	. 1821	3 18 241	18 270	18 298	18 327	18 355	18 384	18412	18441	6	5	"
•53	18 469	1849	8 18 526	18 554	18 583	18611	18 639	18 667	18 696	18 724	9		1
•54	1		0 18 808		-		18921	18 949	18977	19 005	12	11	
1.55	.19 033	.19 06	1 .19 089	.19 117	.19 145		.19 201	.19 229	.19 257	.19 285	15	14	
.56	19 312	19 34	0 19 368	19 396	19 424		19 479	19 507	19 535	19 562	17	16	ı
·57 ·58	19 590	19 61	8 19 645 3°19 921	19 073	19 700		19 756	19 783	19811	19 838	20	-	
.59			3 19 921 7 20 194				20 030	20 058	20 085	20 112 20 385	23		1
		20.10	, =0 -94	. 20 222	20 249	20 2 70	20 303	20 330	20 350	20 305	26	24	1
1.60	1 :-		9 .20 466			.20 548	.20 575	.20 602	.20 629	.20 656	26	25	
.61			20 737			20 817	20 844	20871	20 898	20 925	3	3	
.62	20 952	20 97	8 21 005	21 032	21 059		21 112	21 139	21 165	21 192	5	5	l
63			5 21 272			21 352	21 378	21 405	21 431	21 458	8	8.	
.64			21 537							21 722	10	ıδ	ľ
1.65			5 .21 801							.21 985	13	13	
.66			7 22 063 3 22 324			22 141	22 167	22 194	22 220	22 246	16	15	l
.68.			7 22 <u>583</u>			22 401	22 427	22 453	22 479	22 505	18	18	
.69			1 22 840			22 017	22 042	22 712 22 968	22 737	22 703	21	20	
	/-/		,		091	9-7	22 943	22 900	22 994	20 010	23	23	
1.70			.23 096			.23 172	.23 198	.23 223	.23 249	.23 274	25	24	
.71			23 350			23 426	23 452	23 477	23 502	23 528	3	2	ľ
.72			23 603			23 679	23 704	23 729	23 754	2 3 779	5	5	
·73	23 005	23 030	23 855 24 105	23 000	23 905			23 980			8	7	
·74								24 229			10	10	
1.75			•24 353 • 24 601					-24 477			13	12	
.76 •77			24 846					24 724 24 969			15	14	
.78			25 091			25 164	25 188	25 212	25 227	25 261	20	17 19	
.79			25 334			25 406	25 431	25 455	25 479	25 503	23	22	
1.80			.25 575			.25 648					24	23	
.81 .82			25 816 26 055			25 000	25.912	25 935	25 959	25 983	2	2	
.83			26 293			26 264	26 287	26 174 26 411	26 425	26 458	5	5	
.84			26 529			26 600	26 623	26 647	26 670	26 604	. 10	7	
1.85			.26 764			.26 834							
.86			26 998					27 114			12 14	12	
.87			27 231					27 346			17	14 16	
.88			27 462					27 577			19	18	
. 89	27 646	27 669	27 692	27 715	27 738			27 807			22	20	
100						0-	00.010	.0	-00	-0 -0-		۸. ا	
1.90						.27 989	25 012 210 92	.28 035 . .28 262	.28 058 .	28 2051	22	21	
.91 .92			28 149 28 375					28 262 28 488			2	2	
.93			28 60I					28 713			4 7	4 6	
.94			28 825					28 937			9	8	
.95			.29 048			.29 115 .				. 1	11	11	
.96			29 270			29 336					13	13	.00
.97			29 491			29 557					15		.30
.98			29 710			29 776	29 798	29 820	29 842	29 863	18	17	
.99			29 929			29 994	30 016	30 038	30 060	30 081	20	19	
1													

5 PL. LOGS.

LOGS, 5 PL

LO	GS.	5 PL.										
	No.	0	1	2	3	4	5	6	7	8	9	INTP. TAB.
.30	2.00			.30 146			.30 211					21
.47	.01			30 363		-				30 492		2
	.02			30 578				30 664			30 728	4
	.03	30 750		30 792		0 05				30 920	30 942	6
	.04	30 963	30 984	31 006	31 027	31 048	31 009	31 091	31 112	31 133	31 154	8
	2.05	.31 175	.31 197	.31 218	.31 239	.31 260	.31 281	.31 302	.31 323	.31 345	.31 366	11
	.06	31 387	31 408	31 429	31 450	31 471	31 492	31 513	31 534	31 555	31 576	13
	.07	31 597	31 618	31 639	31 660	31 681	31 702	31 723	31 744	31 765	31 785	15
	.08	31 806	31 827	31 848	31 869	31 890	31 911	31 931	31 952	31 973	31 004	17
	.09	32 015		32 056			32 118	32 139	32 160	32 181	32 201	19
	2.10	.32 222	.32 243	.32 263	.32 284	.32 305	.32 325	.32 346	.32 366	.32 387	.32 408	20
	.II	32 428	32 449	32 469	32 490	32 510	32 531	32 552	32 572	32 593	32 613	2
	.12	32 634	32 654	32 675	32 695	32 715				32 797		4
	.13	32 838	32 858	32 879	32 899	32 919		32 960			33 021	6
	.14	33 041	33 062		33 102		33 143		33 183		33 224	8
	2.15			.33 284								
	.16		33 465	33 486						.33 405		IO
		33 445	:		33 506					33 606		12
	.17	33 646				•				33 806		14
	81.	33 846						33 965			34 025	16
	.19	34 044	34 004	34 084	34 104	34 124	34 143	34 163	34 183	34 203	34 223	18
	2.20	.34 242	.34 262	.34 282	.34 301	.34 321	·34 34I	.34 361	.34 380	.34 400	.34 420	19
	.21	34 439	34 459	34 479	34 498	34 518	34 537	34 557	34 577	34 596	34 616	2
•	.22	34 635	34 655	34 674	34 694	34 713	34 733	34 753	34 772	34 792	34 811	4
	.23	34 830	34 850	34 869	34 889	34 908				34 986		6
	.24	35 025	35 044	35 064	35 083	35 102	35 122	35 141	35 160	35 180	35 199	8
	2.25	.35 218	.25 228	·35 ² 57	.35 276	.35 205	.25 215	.25 224	.25 252	-35 372	25 202	10
	.26			35 449						35 564		11
	.27			35 641						35 755		
	.28			35 832						35 735 35 946		13
	1	35 984		36 021			26.028	36 097	26 116	36 135		15
	.29	•••		-						•	36 154	17
	2.30					.36 248				.36 324		18
	.31					36 436		36 474			36 530	2
	.32				36 605	36 624				36 698		4
	•33	36 736	36 754	3 ⁶ 773	36 791	36 810	36 829	36 847	36 866	36 884	36 903	5
	•34	36 922	36 940	36 959	36 977	36 996	37 014	37 °33	37 051	37 070	37 088	7
	2.35	.37 107	.37 125	.37 144	.37 162	.37 181	.37 199	.37 218	.37 236	·37 254	.37 273	9
	.36	37 291		37 328	37 346	37 365				37 43 ⁸		11
		37 475	37 493			37 548	37 566			37 621		13
	·37 .38	37 658	37 676			37 731	37 749		737 785		37 822	14.
	.39	37 840		37 876		37 912		37 949				16
į		1 .0	28 222	28 055	28 000	28 002	.38 112	28 120	28 T48	28 166	. 28 184	17
		.38 021	18 110	28 228	28 256		38 292	_		38 346		2
	.41			38 238 38 417	38 435					38 525		3
	.42		38 399				28 650	28 KKP	28 686	38 703	28 221	
	•43			38 596	38 500	28 810						5
	.44		3 ⁸ 757				-			38 881	-	7
	2.45	.38 917	.38 934	.38 952	.38 970	.38 987	.39 005					9
.30	.46	39 094		39 129						39 235		10
.47	·47	39 270	39 287	39 305	39 322	39 340				39 410		12
.7/	.48	39 445	39 463	39 480	39 498	39 515	39 533	39 550	39 568	39 585	39 602	14
	-49	39 620	39 637	39 655	39 672	39 690	39 707	39 724	39 742	39 759	39 777	15
	*+7	37	3, 01									انا

LOGS. 5 PL.

FIVE PLACE LOGARITHMS.

2. 5 PL. LOGS.

										5 PL.	
ο.	0	1	2	3	4	5	6	7	8	9	INTP. TAB.
50	-39 794	.39 811	.39 829	.39 846	.39 863	.39 881	.39 898	.39 915	.39 933	.39 950	18
51					40 037			40 088			2
52	40 140	40 157	40 175	40 192	40 209	40 226	40 243	40 261	40 278	40 295	4
53		40 329				40 398	40 415	40 432	40 449	40 466	5
54		40 500				40 569	40 586	40 603	40 620	40 637	7
55	.40 654	.40 671	.40 688	.40 705	.40 722	.40 739	.40 756	.40 773	.40 790	.40 807	9
56		40 841						40 943			ΙÍ
57		41 010						41 111			13
58		41 179						41 280			14
59		41 347				41 414	41 430	41 447	41 464	41 481	16
60	.41 497	.41 514	.41 531	.41 547	.41 564	41 581	.41 597	.41 614	.41 631	.41 647	17
61 l		41 681				41 747	41 764	41 780	4 ¹ 797	41 814	2
62	41 830	41 847	41 863	41 880	41 896	41 913	41 929	41 946	41 963	41 979	3
63		42 012				42 078	42 095	42 111	42 127	42 144	5
64	42 160	42 I 77	42 193	42 210	42 226	42 243	42 259	42 275	42 292	42 308	7
65	.42 325	.42 341	.42 357	.42 374	.42 390	.42 406	.42 423	.42 439	.42 455	.42 472	9
66		42 504						42 602			Io
67		42.667								42 797	12
68		42 830								42 959	14
69	42 975	42 991	43 008	43 024	43 040					43 120	15
70	.43 136	.43 152	.43 169	.43 185	.43 201	.43 217	.43 233	.43 249	.43 265	.43 281	16
71	43 297	43 313	43 329	43 345	43 361			43 409			2
72		43 473								43 600	3
73		43 632						43 727			* 5
74		43 791						43 886			6
75		43 949				44 012	.44 028	.44 044	.44 050	.44 075	8
76		44 107						44 201			10
77		44 264								44 389	II
78					44 467			44 514			13
79	44 560	44 576	44 592	44 607	44 623					44 700	14
80	.44 716	.44 73I	.44 747	.44 762	.44 778	44 793	.44 809	.44 824	.44 840	.44 855	15
81		44 886								45 010	2
82		45 040								45 163	3
83		45 194						45 286			5
84	45 332	45 347	45 362	45 378	45 393	45 408	45 423	45 439	45 454	45 469	6
85	.45 484	.45 500	.45 515	.45.530	.45 545	.45 561	.45 576	. 45 591	.45 606	.45 621	8
86	45 637	45 652	45 667	45 682	45 697	45 712	45 728	45 743	45 758	45 773	9
87	45 788	45 803	45 818	45 834	45 849					45 924	11
88	45 939	45 954	45 969	45 984	46 000					46 075	12
89					46 150	46 165	46 1 80	46 195	46 210	46 225	14
90	.46 240	.46 255	.46 270	.46 285	.46 300	.46 315	.46 330	.46 345	.46 359	.46 374	14
91	46 389	46 404	46 419	46 434	46 449	46 464	46 479	46 494	46 509	46 523	I
92	46 538	46 553	46 568	46 583	46 598	46 613	46 627	46 642	46 657	46 672	3
93	46 687	46 702	46 716	46 731	46 746	46 761	46 776	46 790	46 805	46 820	4
94	46 835	46 850	46 864	46 879	46 894	46 909	46 923	46 938	46 953	46 967	6
95		.46 997								.47 114	7
96	47 129	47 I44	47 159	47 173	47 188	47 202	47 217	47 232	47 240	47 261	8
97	47 276	47 290	47 305	47 319	47 334	47 349	47 363	47 378	47 392	47 407	10
98	47 422	47 436	47 45 1	47 465	47 480	47 494	47 509	47 524	47 538	47 553	11
99 l	1 47 567	47 582	47 596	47 611	47 625	47 640	47 054	47 669	47 083	47 698	13

5 PL. LOGS. 2.

	No.	0	I	2	3	4	5	6	7 .	8	9	INTP. TAB.
.47	3.00	.47 712	.47 727	.47 741	.47 7 5 6	47 770	47 784	•47 799	.47 813	.47 828	.47 842	15
.60	.01		47 871					47 943				2
	.02		48 015					48 087				3
- 1	.03		48 159				48 216	48 230	48 244	48 259	48 273	5
	.04		48 302					48 373				6
- 1	3.05		.48 444				.48 501	.48 515	.48 530	.48 544	.48 558	8
	.06		48 586				48 643	48 657	48 671	48 686	48 700	9
	.07 .08		48 728 48 869				48 026	48 799 48 940	48 813	48 827	48 841	II
	.09		49 010				49 066	49 080	49 954	49 108	48 982 49 122	12 14
	3.10	.49 136	.49 150	.49 164	.49 178	.49 192	.49 206	.49 220	.49 234	.49 248	.49 262	14
	.II		49 290					49 360				I
	.12	49 415	49 429	49 443	49 457	49 47 I	49 485	49 499	49 513	49 527	49 541	3
	.13		49 568				49 624	49 638	49 651	49 665	49 679	4
	.14	49 693				49 748		49 776				6
	3.15		.49 845					.49 914				7
	.16		49 982					50 051				8
	.17 .18		50 120 50 256					50 188	-		-	10
	.19		50 393					50 325 50 461				11
	-			-	-					_		
	3.20					.50 569		.50 596				13
	.21		50 664					50 732			J	I
	.22		50 799 50 934			50 840		50 866 51 001				3
	.24		51 068			51 108	51 121				51 175	5
	3.25		.51 202			-	-	.51 268	-	-	-	7
	.26		51 335					51 402	•			8.
	.27					51 508		51 534				9
	.28					51 640	51 654	51 667	51 680	51 693	51 706	ΙÓ
	.29	51 720	51 733	53 746	51 759	51 772	51 786	51 799	51 812	51 825	51 838	12
	3.30	.51 851	.51 865	.51 878	.51 891	.51 904	.51 917	.51 930	.51 943	.51 957	.51 970	13
	.31		51 996					52 061				I
	.32		-	-	_	52 166	-	52 192			_	3
	•33		52 257					52 323				4
	•34	1 -				52 427		52 453				5
	3.35	.52 504	.52 517	.52 530	.52 543	.52 556		.52 582				7 8
	.36	52 034	52 047	52 000	52 073	52 686		52 711 52 840				9
	·37 ·38	52703	52 776 52 905	52 709	52 002 F2 030	52013	52.056	52 969	52 082	52 004	53 007	10
	.39	53 020	53 033	53 046	53 058	53 071		53 097				12
	3.40	.53 148	.53 161	.53 173	.53 186	.53 199	.53 212	.53 224	·53 237	.53 250	.53 263	12
	.41	53 275	53 288	53 301	53 314	53 326		53 352				1
	.42	53 403	53 415	53 428	53 441	53 453		53 479				2
- 1	-43	53 529	53 542	53 555	53 567	53 580		53 605				4
	-44		53 668				-	53 732	-			5
	3.45	.53 782	-53 794	.53 807	.53 820	.53 832		.53 857				6
.47	.46	53 908	53 920	53 933	53 945	53 958		53 983 54 108				7 8
.60	·47	54 033	54 045 54 170	54 050	54 105	54 208		54 233				10
	.48	54 282	54 295	54 307	54 320	54 332	54 345	54 357	54 370	54 382	54 394	11
	.49	34 203	34 493	J+ J~/	JT J=0	JT JJ	JT JT3	JT JJ/	JT 31°	JT J	JT JJT	<u> L</u>

LOGS. 5 PL. 3.

3. 5 PL. LOGS.

	-									5 PL.	LU	33.
No.	0	I	2	3	4	5	6.	7	8	9	INTP.	
3.50	.54 407	.54 419	•54 432	.54 444	.54 456	.54 469	.54 481	•54 494	.54 506	.54 5 18	13	.47
.51	54 531	54 543	54 555	54 568	54 580	54 593	54 605	54 617	54 630	54 642	1	.60
.52	54 654	54 667	54 679	54 691	54 704	54 716	54 728	54 741	54 753	54 765	3	
•53					54 827 54 949	54 839	54 851	54 864	54 876	54 888	4	
•54	1							54 986			5	1
3.55					.55 072 55 194	.55 084	.55 096	.55 108	.55 121	.55 133	7	
.56					55 315	55 200	55 210	55 230 55 352	55 242	55 255	8	
.58					55 437			55 473			IO	Į
•59					55 558	55 570	55 582	55 594	55 606	55 618	12	
3.60	1 00 0				.55 678	.55 69 1	.55 703	.55 715	·55 727	•55 739	12	
.61					55 799			55 835			I	
.62					55 919	55 931	55 943	55 955	55 967	55 979	2	
.63 .64					56 038 -56 158			56 074 56 194			4	
1	1										5	
3.65					.56 277 56 396	.50 289	.50 301	.56 312 56 431	.50 324	.56 336	6	
.67					56 514	56 526	50419	56 549	50 443	50 455	7 8	
.68					56 632			56 667			10	
.69					56 750	56 761	56 773	56 785	56 797	56 808	11	
3.70					.56 867	.56 879	.56 891	.56 902	.56 914	.56 926	12	
.71					56 984	56 996	57 008	57 019	57 031	57 043	I	
.72		57 066						57 136			2	
.73		57 183						57 252			4	
•74		57 299	•					57 3 ⁶⁸			5	
3.75					.57 449			·57 484			6	
.76		57 530 57 646						57.600			7	
.77 .78		57 761						57 715 57 830			8 10	
.79		57 875						57 944			11	
3.80	.57 978	.57 990	.58 001	.58 013	.58 024	.58 035	.58 047	.58 058	.58 070	.58 081	11	
.81		58 104						58 172			1	
.82		58 218						58 286			2	
.83		58.331						58 399			3	
.84		58 444						58 512			4	
3.85		.58 557						.58 625			6	
.86		58 670						58 737			7	
.87 .88		58 782 58 894						58 850 58 961			8	
.89					59 040			59 073			9 10	
3.90	.50 106	.50 118	.50 120	.50 140	.50 151	.59 162	.50 173	.50 184	.50 105	.50 207	11	
.91		59 229	59 240	59 251	59 262			59 295			I	
.92		59 340						59 406			2	
.93	59 439	59 450	59 461	59 472	59 483			59 517			3	
•94	59 550	59 561	59 572	59 583	59 594		-	59 627	-	-	4	
3.95		.59 671						.59 737			6	
.96		59 780						59 846			7	.47
.97		59 890						59 956			8	.60
.98		59 999 60 108						60 065 60 173			9	
.99	00 097	00 100	00 119	00 130	00 141	00 152	00 103	00 1/3	50 104	30 195	Ю	
										S DI I		_

5 PL. LOGS.

	No.	0	I	2	3	4	5	6	7	8	9	INTP.
.60	4.00	.60 206	.60 217	.60 228	.60 239	.60 249	.60 260	.60 271	.60 282	.60 293	.60 304	11
.69	.01		60 325				60 369	60 379	60 390	60 401	60 412	1
	.02		60 433						60 498			2
	.03	•••	60 541			• • •			60 606			3
	.04		60 649		•				60 713			4
	4.05		.60 756						.60 821			6
	.06		60 863 60 970		-				60 927			7
	.07		61 077						61 034 61 140			8
	.09		61 183						61 247			9. 10
	4.10	.61 278	.61 289	.61 300	.61 3ìo	.61 321	.61 331	.61 342	.61 352	.61 363	.61 374	11
	.II	61 384	61 395	61 405	61 416	61 426	61 437	61 448	61 458	61 469	61 479	ı
	.12		61 500				61 542	61 553	61 563	61 574	61 584	2
	.13	61 595	61 606	61 616	61 627	61 637			61 669			3
	.14		61711				61 752	61 763	61 773	61 784	61 794	4
	4.15		.61 815						.61 878			6
	.16		61 920						61 982			7
	.17		62 024					•	62 086		•	8
	.18		62 128 62 232						62 190 62 294			9 10
	,		•	•	•	•	, -			• •		
	4.20		.62.335 62 439						.62 397 62 500		-	10 I
	,22		62 542						62 603	_	•	2
	.23		62 644						62 706			3
	.24	62 737	62 747	62 757	62 767	62 778	62 788	62 798	62 808	62 818	62 829	4
	4.25	.62 839	.62 849	.62 859	.62 870	.62 880	.62 890	.62 900	.62 910	.62 921	.62 931	5
	.26		62 951				-	-	63 012	-		6
	.27		63 053						63 114			7
	.28		63 155						63 215			8
	.29	63 246	63 256	63 266	63 276	63 286			63 317			9
	4.30	.63 347	.63 357	.63 367	.63 377	.63 387			.63 417			10
	.31		63 458						63 518			1
	.32					63 589			63 619			2
	•33		63 659						63 719 63 819			3
	•34		. 63 759				- •					4
	4.35		.63 859						.63 919 64 018			5
	.36	03 949	63 959 64 058	64.068	64.078	64.088			64 118			7
	·37	64 147	64 157	64 167	64 177	64 187			64 217			8
	•39	64 246	64 256	64 266	64 276	64 286			64 316			9
	4.40	.64 345	.64 355	.64 365	.64 375	.64 385	.64 395	.64 404	.64 414	.64 424	.64 434	9
	.4I	64 444	64 454	64 464	64 473	64 483			64 513	_		r
	.42	64 542	64 552	64 562	64 572	64 582			64 611			2
	43	64 640	64 650	64 660	64 670	64 680			64 709			3
1	.44		64 748						64 807			4
	4.45	.64 836	.64 846	.64 856	.64 865	.64 875	.64 885					5
.60	.46	64 933	64 943	64 953	64 963	64 972	64 982	64 992	65 002	65 011	65 021	5
.69	-47		65 040				65 079	65 089	65 099	65 108	65 118	
	.48	65 128		65 147					65 196			7 8
	•49	65 225	05 234	65 244	05 254	05 203	05 2/3	05 203	65 292	05 302	05 512	نــــــــــــــــــــــــــــــــــــــ

FIVE PLACE LOCARITHMS.

5 PL. LOGS.

										5 PL.	LU	άS.
No.	0	I	2	3	4	5	6	7	8	9	INTP. TAB.	Ì
4.50	.65 321	.65 331	.65 341	.65 350	.65 360	.65 369	.65 379	.65 380	.65 308	.65 408	10	.60
.51	65 418	65 427	65 437	65 447	65 456	65 466	65 475	65 485	65 495	65 504	I	.69
.52	65 514	65 523	65 533	65 543	65 552	65 562	65 571	65 581	65 591	65 600	2	
·53	65 610	65 619	65 629	65 639	65 648	65 658	65 667	65 677	65 686	65 696	3	
•54	65 706	65 715	65 725	65 734	65 744	65 753	65 763	65 772	65 782	65 792	4	,
4.55		.65 811						.65 868			5	
.56	65 896	65 906	65 9 1 6	65 925	65 935	65 944	65 954	65 963	65 973	65 082	6	
.57	65 992	66 001	66 oi i	66 020	66 030	66 039	66 049	66 058	66 068	66 077	7	
.58	66 087	66 096	66 10 6	66 115	66 124	66 134	66 143	66 153	66 162	66 172	8	
•59	66 181	66 191	66 200	66 210	66 219	66 229	66 238	66 247	66 257	66 266	9	
4.60	.66 276	.66 285	.66 295	.66 304	.66 314	.66 323	.66 332	.66 342	.66 351	.66 361	9	
.61	66 370	66 380	66 389	66 398	66 408	66 417	66 427	66 436	66 445	66 455	I	
.62	66 464	66 474	66 483	66 492	66 502	66 511	66 521	66 530	66 539	66 549	2	
.63		66 567				66 605	66 6 14	66 624	66 633	66 642	3	
.64	66 652	66 661	66 671	66 68o	66 689	66 699	66 708	66 717	66 727	66 736	4	
4.65	.66 745	.66 755	.66 764	.66 773	.66 783			.66 811			5	
.66	66 839	66 848	66 857	66 867	66 876	66 885	66 894	66 904	- 66 913	66 922	5	
.67					66 969	66 978	66 987	66 997	67 006	67 015	6	
.68	67 025	67 034	67 043	67 052	67 062	67 071	67 080	67 089	67 099	67 108	7	
.69	67 117	67 127	67 136	67 145	67 1 54	67 164	67 173	67 182	67 191	67 201	8	
4.70	.67 210	.67 219	.67 228	.67 237	.67 24 7	.67 256	.67 265	.67 274	.67 284	.67 293	9	
.71	67 302	67 311	67 321	67 330	67 339	67 348	67 357	67 367	67 376	67 385	1	
.72	67 394	67 403	67413	67 422	67 431	67 440	67 449	67 459	67 468	67 477	2	
.73		67 495				67 532	67 541	67 550	67 560	67 569	3	
∙74	67 578	67 587	67 596	67 605	67 614	67 624	67 633	67 642	67 651	67 660	4	
4.75		.67 679				.67 715	.67 724	.67 733	.67 742	.67 752	5	
.76	67 761	67 770	67 779	67 788	67 797	67 806	67815	67 825	67 834	67 843	5	
.77		67 861				67 897	67 906	67 916	67 925	67 934	6	
.78		67 952				67 988	67 997	68 006	68 015	68 024	7	
·79	68 034	68 043	68 052	190 89	68 070	68 07 9	68 o88	68 097	68 106	68 115	8	
4.80	.68 124	.68 133	.68 142	.68 151	.68 160	.68 169	.68 178	.68 187	68 196	.68 205	9	
18.		68 224				68 26 0	68 269	68 278	68 287	68 296	I	
.82	68 305	68 314	68 323	68 332	68 341	68 350	68 359	68 368	68 377	68 386	2	
.83		68 404						68 458			3	
.84	68 485	68 494	68 502	68 511	68 520	68 529	68 538	68 547	68 556	68 565	4	
4.85	.68 574	.68 583	.68 592	.68 6о1	.68 610	.68 619	.68 628	.68 637	.68 646	.68 655	5	
.86		68 673				68 708	68 717	68 726	68 735	68 744	5	
.87		68 762				68 797	68 806	68 815	68 824	68 833	6	
.88		68 851				68 886	68 895	68 904	68913	68 922	7	
.89	68 931	68 940	68 949	68 958	68 966	68 975	68 984	68 993	69 002	69 011	8	
4.90	.69 020	.69 028	.69 037	.69 046	.69 055	.69 064	.69 073	.69 082	.69 090	.69 099	8	
.91		69 117				69 152	69 161	69 170	69 179	69 188	1	
.92		69 205						69 258			2	
.93		69 294						69 346			2	
.94		69 381				69 417	69 425	69 434	69 443	69 452	3	
4.95		.69 469						.69 522	- 50	- 50-	4	.60
.96		69 557						69 609			5 6	.69
.97		69 644		-				69 697				
.98		69 732						69 784			6	
.99	69 810	69 819	69 827	69 836	69 845	69 854	69 862	69 871	69 88o	69 888	7	

5. FIVE PLACE LOGARITHMS. LOGS. 5 PL.

Ī	No.	5 PL.		2	3	4	5	6	7	8	9	INTP.
												TAB.
.70 .77	5.00	.69 897						.69 949				9
`''	.01		70 079	70 001	70 096	70 018		70 0 36 70 1 2 2				I
	.03			70 174				70 209				2
ı	.04	70 243		70 260			70 286				70 321	3 4
	5.05	.70 329	. •	-		•	•	.70 381				1 1
- 1	.06	70 415		70 432		70 449		70 467			70 492	5
	.07			70 5 1 8			70 544			70 569		5
	.08			70 603			70 629	70 638	70 646	70 655	70 663	7
	.09	70 672	70 680	70 689	70 697	70 706	70 714	70 723	70 731	70 740	70 749	8
	5.10	.70 757	.70 766	.70 774	.70 783	.70 791	.70 800	.უი So8	.70 817	.70 825	.70 834	8
	.II	70 842	70 851	70 859	70 868	70 876	70 885	70 893	70 902	70 910	70 919	1
	.12	70 927				70 961	7 0 969	70 978	70 986	70 9 95	71 003	2
	.13	71 012			71 037			71 063				2
	.14	1				71 130		71 147				3
	5.15					.71 214	.71 223	.71 231	.71 240	.71 248	.71 257	4
	.17	1				71 299 71 383		71 315				5 6
	.18					71 466		71 399 71 483				6
	.19					71 550		71 567				7
	5.20	.71 600	.71 609	.71 617	.71 625	.71 634	.71 642	.71 650	.71 650	.71 667	.71 675	8
	.21	1 '				71 717		71 734				1
	.22					71 800		71 817				2
	.23			71 867			-	71 900			71 925	2
	.24	71 933			71 958		7 1 975		71 991		72 008	3
	5.25	1 '			-	.72 049		.72 066				4
	.26					72 132		72 148 72 230				5 6
	.27					72 296	•	72 313				6
	.29					72 378		72 395				7
	5.30	.72 428	.72 436	.72 444	.72 452	.72 460	.72 469	.72 477	.72 485	.72 493	.72 501	8 Î
	.31					72 542	72 550	72.558	72 567	72 575	72 583	Ĩ
	.32	72 591		72 607	72 616	72 624		72 640				2
	•33	72 673		•	72 697			72 722				2
	∙34	72 754			72 779		72 795	• -	72 811	-		3
	5.35	72 835				.72 868		.72 884				4
	.36	72 916			72 941		72 957			72 981		5 6
	•37			73 014 73 094			•	73 046 73 127			73 151	ğ
	.38	73 078		73 175		73 191		73 207		,		7
						.73 272	72 280	.73 288	72 206	.73 304	.73 312	7
	5.40	73 239	73 328	73 336	73 344	73 352		73 368	_	73 384		1
	.4I		73 408	73 416	73 424	73 432		73 448				1
	.43	73 480	73 488	73 496		73 512	73 520	73 528	73 536	73 544	73 552	2
	.44	73 560	73 568			73 592		73 608				3
	5.45	.73 640	.73 648	.73 656	.73 664	.73 672		.73 687				4
.70	.46	73 719	73 727	73 735	73 743	73 75 ^I	73 759	73 767	73 775	73 783	73 791	4
.77	•47		73 807	73 815	73 823	73 830		73 846				5
	.48	73 878	73 886	73 894 73 973		73 910 73 989		73 926 74 005				6
	.49	73 957	73 965	13913	73 901	13 909	13 771	,1000	74 013	74 020	77	

LOGS. 5 PL.

FIVE PLACE LOGARITHMS.

5 PL. LOGS.

				-						PL.	INTP.	
No.	0	I	2	3	4	5	6	7	8	9	TAB.	
5.50	.74 036	.74 044	.74 052	.74 060	.74 068	.74 076	.74 084	.74 092	.74 099	.74 107	8	.70
.51				74 139			-	-	74 1 78		I	.77
.52				74 218 74 296					74 257 74 335		2 2	
·53			74 367		74 382				74 414		3	
5.55				.74 453					.74 492	• • •	4	1
.56				74 531	74 539			•	74 570		5	
.57				74 609	74 617	74 624	74 632	74 640	74 648	74 656	6	ľ
.58				74 687					74 726		6	
•59	74 741	74 749	74 757	74 764	74 772	74 780	74 788	74 790	74 803	74 811	7	
5.60	.74 819	.74 827	.74 834	.74 842	.74 850	.74 858	.74 865	.74 873	.74 881	.74 889	7	
.61				74 920					74 958		1	l
.62				74 997				. •	75 035		1	l
.63 .64	75 051			75 074 75 151				75 105 75 182	75 189	75 120 75 107	3	l
5.65				.75 228					.75 266			
.66				75 305				75 335		75 351	4 4	
.67				75 381					75 420		5	
.68				75 458					75 496		6	İ
.69	75 511	75 519	75 526	75 534	75.542	75 549	75 557	75 5 ⁶ 5	75 572	75 580	6	l
5.70	.75 587	75 595	.75 603	.75 610	.75 618	.75 626	.75 633	.75 641	.75 648	.75 656	8	ı
.71	75 664	75 671	75 679	75 686	75 694	75 702	75 709	75 717	75 724	75 73 ²	-1	
.72				75 762					75 800		2	ı
.73			75 831				75 861			75 884	2	l
.74	75 891			75 914				75 944		75 959	3	
5.75				.75 989 76 065					.76 027 76 103		4	
.76 .77				76 140					76 178		5 6	
.78				76 215					76 253		6	
•79	76 268	76 275	76 283	76 290	76 298	76 305	76 313	76 320	76 328	76 335	7	
5.80	.76 343	.76 350	.76 358	.76 365	.76 373	.76 380	.76 388	.76 395	.76 403	.76 410	7	
.81				76 440					76 477		1	
.82				76 515					76 552		I	
.83				76 589					76 626		2	
.84		•		76 664					76 701	76 708	3	
5.85 .86				.76 738 76 812		.70 753	76 824	76 842	.76 775 76 849	.70 702 26 8c6	4	
.87				76 886					76 923		4 5	
.88				76 960					76 997		6	
.89					77 041				77 070		6	
5.90	.77 085	.77 093	.77 100	.77 107	.77 115	.77 122	.77 129	.77 1 37	.77 144	.77 151	7	
.91				77 181		77 195	77 203	77 210	77 217	77 225	1	l
.92				77 254					77 291		τ	
.93				77 327				77 357			2	
•94					77 408				77 437		3	
5.95				•77 474		.77 488	.77 495	.77 503	·77 510 77 583	.77 517	4	.70
.96 .97				77 546 77 619					77 5°3 77 656		5	.77
.98				77 692					77 728		6	l,
.99				77 764		77 779	77 786	77 793	77 801	77 808	6	
						77 779	77 786	77 793	77 801	77 808		

5 PL. LOGS. 5. 6. LOG<u>S. 5 PL.</u>

	No.	0	I	2	3	4	5	6	7	8	9	INTP TAB.
.77 .84	6.00 .01 .02 .03 .04	77 887 77 960 78 032	77 895 77 967	77 974 78 046	77 909 77 981 78 053	77 916 77 988	77 924 77 996 78 068	77 931 78 003 78 075	.77 866 77 938 78 010 78 082 78 154	77 945 78 017 78 089	77 952 78 025 78 097	8 I 2 2 3
	6.05 .06 .07 .08	78 247 78 319 78 390	78 254 78 326 78 398	.78 190 78 262 78 333 78 405	.78 197 78 269 78 340 78 412		.78 211 78 283 78 355 78 426	.78 219 78 290 78 362 78 433	.78 226 78 297 78 369 78 440 78 512	.78 233 78 305 78 376 78 447	.78 240 78 312 78 383 78 455	4 5 6 6 7
	6.10 .11 .12 .13 .14 6.15 .16 .17	78 604 78 675 78 746 78 817 .78 888 78 958 79 029 79 099	78 611 78 682 78 753 78 824 .78 895 78 965 79 036 79 106	.78 547 78 618 78 689 78 760 78 831 .78 902 78 972 79 043 79 113 79 183	78 625 78 696 78 767 78 838 .78 909 78 979 79 050 79 120	78 633 78 704 78 774 78 845 .78 916 78 986 79 057 79 127	78 640 78 711 78 781 78 852 .78 923 78 993 79 064 79 134	78 647 78 718 78 789 78 859 .78 930 79 000 79 071 79 141	.78 583 78 654 78 725 78 796 78 866 .78 937 79 007 79 078 79 148 79 218	78 661 78 732 78 803 78 873 .78 944 79 014 -79 085 79 155	78 668 78 739 78 810 78 880 .78 951 79 021 79 092 79 162	7 1 2 3 4 4 5 6
	6.20 .21 .22 .23 .24 6.25 .26 .27 .28	.79 239 79 309 79 379 79 449 79 518 .79 588 79 657 79 727 79 796	.79 246 79 316 79 386 79 456 79 525 .79 595 79 664 79 734 79 803	.79 253 79 323 79 393 79 463	.79 260 79 330 79 400 79 470 79 539 .79 609 79 678 79 748 79 817	.79 267 79 337 79 407 79 477 79 546 .79 616 79 685 79 754 79 824	.79 274 79 344 79 414 79 484 79 553 .79 623 79 692 79 761 79 831	.79 281 79 351 79 421 79 491 79 560 .79 630 79 699 79 768 79 837	.79 288 79 358 79 428	.79 295 79 365 79 435 79 505 79 574 .79 644 79 713 79 782 79 851	.79 302 79 372 79 442 79 511 79 581 .79 650 79 720 79 789 79 858	7 1 2 3 4 4 5 6 6
	6.30 .31 .32 .33 .34 6.35 .36 .37 .38 .39	80 003 80 072 80 140 80 209 .80 277 80 346 80 414 80 482	80 010 80 079 80 147 80 216 .80 284 80 353 80 421 80 489	.79 948 80 017 80 085 80 154 80 223 .80 291 80 359 80 428 80 496 80 564	80 024 80 092 80 161 80 229 .80 298 80 366 80 434 80 502	80 030 80 099 80 168 80 236 .80 305 80 373 80 441 80 509	.79 969 80 037 80 106 80 175 80 243 .80 312 80 380 80 448 80 516	.79 975 80 044 80 113 80 182 80 250 .80 318 80 387 80 455 80 523	.79 982 80 051 80 120 80 188 80 257 .80 325 80 393 80 462 80 530 80 598	.79 989 80 058 80 127 80 195 80 264 .80 332 80 400 80 468 80 536	.79 996 80 065 80 134 80 202 80 271 .80 339 80 407 80 475 80 543	7 1 2 3 4 4 5 6
.77 .84	6.40 .41 .42 .43 .44 6.45 .46 .47 .48	80 754 80 821	80 693 80 760 80 828 80 895 .80 963 81 030 81 097 81 164	80 699 80 767 80 835 80 902 .80 969 81 037 81 104 81 171	80 706 80 774 80 841 80 909 .80 976 81 043 81 111 81 178	80 713 80 781 80 848 80 916 .80 983 81 050 81 117 81 184	80 855 80 922 .80 990 81 057 81 124 81 191	80 726 80 794 80 862 80 929 .80 996 81 064 81 131 81 198	80 733 80 801 80 868 80 936	80 740 80 808 80 875 80 943 .81 010 81 077 81 144 81 211	80 747 80 814 80 882 80 949 .81 017 81 084 81 151 81 218	6 1 2 2 3 4 4 5 5

LOGS. 5 PL.

FIVE PLACE LOCARITHMS.

5 PL. LOGS.

										5 PL <u>.</u>		~ • •
No.	0	I	2	3	4	5	6	7	8	9	INTP. TAB.	
6.50	.81 291	.81 298	.81 305	.81 311	.81 318	.81 325	.81 331	.81 338	.81 345	.81 351	6	.77
.51	81 358	81 365	81 371	81 378	81 385	81 391		81 405			I	.84
.52	81 425	81 431	81 438	81 445	81 451	81 458	81 465	81 471	81 478	81 485	1	
·53	81 491	81 498	81 505	81511	81 518	81 525		81 538			2	
•54	81 558	81 564	81 571	81 578	81 584	81 591	81 598	81 604	81 611	81 617	2	
6.55	.81 624	.81 631	.81 637	.81 644	.81 651	.81 657	.81 664	.81 671	.81 677	.81 684	3	
.56					81 717			81 737			4	١.
∙57					81 783			81 803			4	
.58						81 856	81 862	81 869	81 875	81 882	5	
-59	81 889	81 895	81 902	81 908	81 915	81 921	81 928	81 935	81 941	81 948	5	
6.60					.81 981		.81 994	.82 000	.82 007	.82 014	7	
.61					82 046			82 066			1	ĺ
.62					82 112	82 119	82 125	82 132	82 138	82 145	1	
.63					82 178			82 197			2	
.64		82 223	_	_			_	82 263		-	3,	
6.65		.82 289						.82 328			4	
.66		82 354						82 393			4	
.67		82 419						82 458			5	١.
.68					82 504			82 523			6	•
.69	82 543	82 549	82 556	82 562	82 569	82 575	82 582	82 588	82 595	82 6ọ1 [°]	6	
6.70		.82 614						.82 653			6	
.71					82 698			82 718			1	
.72					82 763			82 782			I	
-73					82 827			82 847			2	
·74				-	82 892	-	. •	82 911	-		2	-
6.75		.82 937						.82 975			3	
.76					83 020						4	
.77					83 085			83 104			4	
.78	83 123	83 129	83 136	83 142	83 149			83 168			5	
·79	03 107	03 193	83 200	83 200	83 213	83 219	83 225	83 232	83 238	83 245	5	l.
6.80		.83 257						.83 296			7	
.81		83 321						83 359			I	
.82	83,378	83 385	83 391	83 398	83 404	83 410	83417	83 423	83 429	83 436	1	
.83		83 448						83 487			2	
.84		83 512						83 550		_	3	
6.85		.83 575						.83 613			4	
.86	83 632	83 639	83 645	83 651	83 658			83 677			5	
.87		83 702				83 727	83 734	83 740	83 746	83 753		
.88 .89	82 822	82 828	82 82	83 770	83 784 83 847	83 790	83 797	83 803	83 809	83 816	6	
.09		-			,	03 053	03 000	83 866	03 072	03 079	6	
6.90		.83 891						.83 929			6	
.91		83 954				83 979	83 985	83 992	83 998	84 004	I	
.92		84 017						84 055			I	
.93		84 080 84 142						84 117 84 180			2 -	
.94							. , .	•	•			
6.95		.84 205				.04 230	.04 230 84 20°	.84 242	84 277	.04 255	3	нн
.96		84 267 84 330						84 305 84 367			4	.77 .84
·97		84 392						84 429			4	.04
.99		84 454						84 491			5	
.22	~ + ++~	~+ 434	54 40 0	3 7 400	~ + +/3	~ 4/9	~ + 4~3	~T 471	~+ 49/	J4 304	د ا	

(23)

LOGS, 5 PL

LC	GS.	5 PL.										
	No.	0	I	2	3	4	5	6	7	8	9	INTP. TAB.
.84	7.00 .01 .02 .03 .04 7.05 .06 .07 .08 .09 7.10 .11	84 572 84 634 84 696 84 757 .84 819 84 880 84 942 85 003 85 065 .85 126 85 187	.84 825 84 887 84 948 85 009 85 071 .85 132 85 193	84 584 84 646 84 708 84 770 .84 831 84 893 84 954 85 016 85 077 .85 138 85 199	.84 528 84 590 84 652 84 714 84 776 .84 837 84 899 84 960 85 022 85 083 .85 144 85 205	84 597 84 658 84 720 84 782 .84 844 84 905 84 967 85 028 85 089 .85 150 85 211	.84 541 84 603 84 665 84 726 84 788 .84 850 84 911 84 973 85 034 85 095 .85 156 85 217	84 609 84 671 84 733 84 794 .84 856 84 917 84 979 85 040 85 101 .85 163 85 224	.84 553 84 615 84 677 84 739 84 800 .84 862 84 924 84 985 85 046 85 107 .85 169 85 230	84 621 84 683 84 745 84 807 .84 868 84 930 85 052 85 114 .85 175 85 236	84 628 84 689 84 751 84 813 .84 874 84 936 84 997 85 058 85 120 .85 181 85 242	7 1 2 3 4 4 5 6 6
	.12 .13 .14 7.15 .16 .17 .18	85 309 85 370 .85 431 85 491 85 552 85 612	85 254 85 315 85 376 .85 437 85 497 85 558 85 618 85 679	85 321 85 382 .85 443 85 503 85 564 85 625	85 327 85 388 .85 449 85 509 85 570 85 631	85 333 85 394 .85 455 85 516 85 576 85 637	85 339 85 400 .85 461 85 522 85 582 85 643	85 345 85 406 .85 467 85 528 85 588 85 649	85 291 85 352 85 412 .85 473 85 534 85 594 85 655 85 715	85 358 85 418 .85 479 85 540 85 600 85 661	85 364 85 425 .85 485 85 546 85 606 85 667	1 2 2 3 4 4 5 5 5
	7.20 .21 .22 .23 .24 7.25 .26 .27 .28	85 794 85 854 85 914 85 974 .86 034 86 094 86 153 86 213	.85 739 85 800 85 860 85 920 85 980 .86 040 86 100 86 159 86 219 86 279	85 806 85 866 85 926 85 986 .86 046 86 106 86 165 86 225	85 812 85 872 85 932 85 992 .86 052 86 112 86 171 86 231	85 818 85 878 85 938 85 998 .86 058 86 118 86 177 86 237	85 824 85 884 85 944 86 004 .86 064 86 124 86 183 86 243	85 830 85 890 85 950 86 010 .86 070 86 130 86 189 86 249	.85 775 85 836 85 896 85 956 86 016 .86 076 86 136 86 195 86 255 86 314	85 842 85 902 85 962 86 022 .86 082 86 141 86 201 86 261	85 848 85 908 85 968 86 028 .86 088 86 147 86 207 86 267	6 1 2 2 3 4 4 5 5
	7.30 .31 .32 .33 .34 7.35 .36 .37 .38 .39	86 392 86 451 86 510 86 570 .86 629 86 688 86 747 86 806	86 812	86 404 86 463 86 522 86 581 .86 641 86 700 86 759 86 817	86 410 86 469 86 528 86 587 .86 646 86 705 86 764 86 823	86 415 86 475 86 534 86 593 .86 652 86 711 86 770	86 421 86 481 86 540 86 599 .86 658 86 717 86 776 86 835	86 427 86 487 86 546 86 605 .86 664 86 723 86 782 86 841	.86 374 86 433 86 493 86 552 86 611 .86 670 86 729 86 788 86 847 86 906	86 439 86 499 86 558 86 617 .86 676 86 735 86 794 86 853	86 445 86 504 86 564 86 623 .86 682 86 741 86 800 86 859	6 1 2 2 3 4 4 5 5
.84 .90	7.40 .41 .42 .43 .44 7.45 .46 .47 .48 .49	86 982 87 040 87 099 87 157 .87 216 87 274 87 332 87 390	.86 929 86 988 87 046 87 105 87 163 .87 221 87 280 87 338 87 396 87 454	86 994 87 052 87 111 87 169 .87 227 87 286 87 344 87 402	86 999 87 058 87 116 87 175 .87 233 87 291 87 349 87 408	87 064 87 122 87 181 .87 239 .87 297 87 355 87 413	87 011 87 070 87 128 87 186 .87 245 87 303 87 361 87 419	87 017 87 075 87 134 87 192 .87 251 87 309 87 367 87 425	.86 964 87 023 87 081 87 140 87 198 .87 256 87 315 87 373 87 431 87 489	87 029 87 087 87 146 87 204 .87 262 87 320 · 87 379 87 437	87 035 87 093 87 151 87 210 .87 268 87 326 87 384 87 442	5 1 2 2 3 3 4 4 5

LOGS. 5 PL. 7.

FIVE PLACE LOGARITHMS.

5 PL. LOGS.

		_									LUC	i .
No.	0	I	2	3	4	5	6	7	8	9	TAB.	
7.50	.87 506	.87 512	.87 518	.87 523	.87 529	.87 535	.87 541	.87 547	.87 552	.87 558	6	.84
.51	87 564	87 570	87 576	87 581	87 587	87 593	87 599	87 604	87 610	87 616	I	.90
.52				87 639					87 668		I	
•53				87 697		87 708	87714	87 720	87 726		2	
•54				87 754				87 777		,,,	2	
7.55				.87 812		.87 823	.87 829	.87 835	.87 841	.87 846	3	
.56				87 869		87 881	87 887	87 892	87 898	87 904	4	
•57				87 927					87 955		4	
.58	87 907	o7 973	07 970	87 984 88 041	88 045				88 013 88 070		5	
•59	00 024	00 U3U	00 030	00 041	33 047	00 053	00 050	00 004	88 070	88 070	5	
7.60					.88 104	.88 110	.88 116	.88 121	.88 127	.88 133	5	
.61				88 156					88 184		I	
.62					88 218				88 241		I	
.63				88 270					88 298		2	
.64				88 326					88 355		2	
7.65				.88 383					.88 412		3	
.66				88 440					88 468		3	
.67				88 497					88 525		4	
.68				88 553 88 610		88 621	88 627	88 622	88 581 88 638	88 642	4	
.69	00 593	00 590	00 004	88 010	00 015	00 021	00 027	00 032	00 030	00-043	5	
7.70				.88 666		.88 677	.88 683	.88 689	.88 694	.88 700	6	
.71				88 722					88 750		I	
.72	88 762	88 767	88 773	88 779	88 784				88 807		r	
·73				88 835					88 863		2	
·74	, .	88 880	•	-	88 897	88 902	88 908	88 913	88 919	88 925	2	
7.75				.88 947					.88 975		3	
.76				89 003					89 031		4	
.77					89 064				89 087		4	
.78				89 115 89 170					89 143 89 198		5	
•79	39 154	09 159	og 105	89 170	39 170	09 102	oy 107	09 193	09 190	og 204	5	
7.80	.89 209	.89 215	.89 221	.89 226	.89 232	.89 237	.89 243	.89 248	.89 254	.89 260	5	
.81				89 282		89 293	89 298	89 304	89 310	89 315	I	
.82				89 337					89 365		I	
.83				89 393		89 404			89 421		2	
.84				89 448		_	_	-	89 476		2	
7.85				.89 504					.89 531		3	
.86				89 559		89 570	89 575		89 586		3	
.87				89 614		89 625			89 642		4	
.88				89 669					89 697		4	
.89	09 700	09 713	09 719	09 724	89 730	89 735	09 741	09 740	89 752	og 757	5	
7.90	.89 763	.89 768	.89 774	.89 779	.89 785	.89 790	.89 796	.89 801	.89 807	.89 812	6	
.91	89 818	89 823	89 829	89 834	89 840				89 862		I	
.92				89 889					89 916		I	
•93				89 944					89 97 1		2	
•94	89 982	89 988	89 993	89 998	90 004	90 009	90015	90 020	90 026	90 031	2	
7.95				.90 053		.90 064	.90 069	.90 075	.90 080	.90 086	3	
.96				90 108					90 135		4	.84
-97				90 162		, ,,			90 189		4	.90
.98				90 217					90 244		5	
.99	90 255	90 260	90 266	90 27 1	90 276	90 282	90 287	90 293	90 298	90 304	5	

5 PL. LOGS.

FIVE PLACE LOCARITHMS.

LOGS, 5 PL

LO	GS.	5 PL.										l.s.===1
	No.	0	I	2	3	4	5	6	7	<u> </u>	9	TAB.
.90	8.00	.90 309	.90 314	.90 320	.90 325	.90 331	.90 336	.90 342	.90 347	.90 352	.90 358	5
.95	.01			90 374						90 407		I
	.02			90 428				90 450			90 466	1
1	.03 .04		9º 477 9º 531		90 488					90 515	. •	2
		•		_	-	90 547				90 569		2
i	8.05 .06			.90 590						.90 623		3
1	.07			90 644 90 698						90 677 90 730		3
	.08		_	90 752						90 784		4
	.09			90 806		90 816		90 827		90 838	90 843	4 5
	8.10	.90 849	.90 854	.90 859	.90 865	.90 870	.90 875	.90 881	.90 886	.90 891	.90 897	6
1	.II	90 902	90 907	90 913	90 918	90 924				90 945		I
	.12	90 956	90 961	90 966	90 972	90 977	90 982	90 988	90 993	90 998	91 004	1
	.13			91 020			91 036	91 041	91 046	91 052	91 057	2
	.14	1		91 073						91 105		2
	8.15	91 116	.91 121	.91 126	.91 132	.91 137	.91 142	.91 148	.91 153	.91 158	.91 164	3
	.16			91 180						91 212		4
	.17			91 233						91 265		4
	81.			91 286	-					91 318		5
	.19			91 339			91 355	91 300	91 305	91 371	91 370	5
	8.20			.91 392						.91 424		5
	.21			91 445						91 477	- 1	I
	.22			91 498						91 529		I
	.23	1		91 551 91 603						91 582 91 635		2
		91 593	-									2
	8.25			.91 656					-	.91 687	, ,,	3
	.26 .27			91 709 91 761						91 740 91 793		3 4
	.28			91 814						91 845		4
	.29			91 866						91 897		5
	8.30	.91 908	.91 913	.91 918	.91 924	.91 929	.91 934	.91 939	.91 944	.91 950	.91 955	6
	.31	91 960	91 965	91 971	91 976	91 981	91 986	91 991	91 997	92 002	92 007	1
	.32	92 012	92018	92 023	92 028	92 033				92 054		1
	•33			92 075		-		92 096	-	-	-	2
	•34		-	92 127		-	92 143	92 148	92.153	92 158	92 103	2
	8.35			.92 179						.92 210		3
	36			92 231		92 241				92 262		4
ĺ	•37			92 283						92 314		4
	.38			92 335 92 387				92 355 92 407		92 366 92 418		5 5
		' ''				•						1
	8.40					.92 449				.92 469		5 I
	.4I			92 490 92 542		92 500				92 521 92 572		I
	.42 ·43	92 531	92 588	92 593	92 598	92 603				92 572		2
	.44			92 645						92 675		2
	8.45			.92 696	_					.92 727		3.
.90	.46	92 737	92 742	92 747	92 752	92 758			-	92 778		3
.95	.47		92 793	92 799	92 804	92 809				92 829		4
	.48	92 840	92 845	92 850	92 855	92 860	92 865	92 870	92 875	92 881	9 2 886	4
	•49	92 891	92 896	92 901	92 906	92911	92.916	92 921	92 927	92 932	92 937	5

LOGS. 5 PL.

FIVE PLACE LOGARITHMS.

8. 5 PL. LOGS.

										O PL.		
lo.	0	I	2	3	4	5	6	7	8	. 9	INTP. TAB.	
.50	.92 942	.92 947	.92 952	.92 957	.92 962	.92 967	.92 973	.92 978	.92 983	.92 988	6	. (
51			93 003					93 029			1	. 9
.52	93 044	93 049	93 054	93 059	93 064	93 069	93 075	93 080	.93 085	93 090	1	
.53			93 105					93 131			2	ı
•54	93 146	93 151	93 156	93 161	93 166	93 171	93 176	93 181	93 186	93 192	2	l
.55	.93 197	.93 202	.93 207	.93 212	.93 217	.93 222	.93 227	.93 232	.93 237	.93 242	3	ı
.56	93 247	93 252	93 258	93 263	93 268	93 273	93 278	93 283	93 288	93 293	4	ı
.57	93 298	93 303	93 308	93 313	93 318	93 323	93 328	93 334	93 339	93 344	4	l
.58			93 359			93 374	93 379	93 3 ⁸ 4	93 389	93 394	5	l
•59	93 399	93 404	9 3 40 9	93 414	93 420	93 425	93 430	93 435	93 440	93 445	5	l
.60			.93 460					.93 485			5	l
.61			93 510					93 536			I	
.62			93 561					93 586			I	l
.63			93611					93 636			2	l
.64			93 661					93 687			2	l
.65			.93 712					.93 737			3	l
.66			93 762					93 7 ⁸ 7			3	ı
.67			93 812					93 837			4	l
.68			93 862					93 887			4	ı
.69	93 902	93 907	93912	93 917	93 922	93 927	93 932	93 937	93 942	93 947	5	l
.70			.93 962					·93 987			4	ĺ
71			94 012					94 037			0	l
72			94 062					94 086			I	l
.73			94 III 94 I6I					94 136 94 186			I	l
•74											2	l
75			.94 211					.94 236			2	l
.76			94 260					94 285			2	ı
·77 .78			94 310 94 359		-			94 335 94 384			3	l
.79 .79			94 409					94 433			3 4	l
.80	04.448	04.452	.94 458	.04.462	04.468	.04.472	04 478	.94 483	04.488	04.402	5	l
.81			94 507					94 532			I	l
.82			94 557					94 581			ī	l
.83			94 606					94 630	-		2	ı
84			94 655					94 680			2	l
.85	.94 694	.94 699	.94 704	.94 709	.94 714	.94 719	.94 724	.94 729	.94 734	.94 738	3	l
86			94 753			94 768	94 773	94 778	94 783	94 7.87	3	l
87			94 802					94 827			4	l
.88					94 861	94 866	94 871	94 876	94 88 o	94 885	4	
89	94 890	94 895	94 900	94 905	94 9 To	94 915	94 919	94 924	94 929	94 934	5	l
90			.94 949			.94 963					4	l
.91			94 998					95 022			0	ı
.92			95 046	- 5	- 0			95 071		-	I	ı
93			95 095					95 119			1	ı
94			95 143					95 168			2	
95			.95 192					.95 216			2	
96			95 240					95 265			2	٠
97			95 289					95 313	- 0 0		3	ŀ
98			95 337					95 361			3	ı
99	95 376	95 38I	95 386	95 390	95 395	95 400	95 405	95 410	95 415	95 419	141	ı

	No.	.0	I	2	3	4	5	6	7	8	9	INTP.
.95				.95 434				_	.95 458			5
.99	.01			95 482					95 506			1
	.02	95 521		95 530 95 578					95 554			I
	.04	95 509		95 626		- 0 0	95 593	05 646	95 602 95 650	95 007	95 660	2 2
	9.05	1		.95 674								
	.06			95 722					.95 698 95 746			3
	.07	05 761	95 766	95 770	95 775	95 780			95 794			3
	.o8			95 818			95 832	95 837	95 842	95 199	95 852	4
	.09			-95 866				95 885	95 890	95 895	95 899	5
	9.10	-		.95 914			.95 928	95 933	.95 938	.95 942	.95 947	4
	II.		95 957			95 971	95 976	95 980	95 985	95 990	95 995	0
	.12	95 999		96 009			96 023	96 028	96 033	96 038	96 042	I
	.13	96 047 96 095		- 0.			90 071	96 076	96 080 96 128	96 085	96 090	I
												2
	9.15			.96 152			.96 166	.96,171	.96 175	.96 180	.96 185	2
	.16	96 237	-	96 199 96 246			90 213	90 218	96 223	96 227	96 232	2
	.18			96 2 94			06 208	90 205	96 270 96 317	96 275	96 280	3
	.19			96 341			96 355	96 360	96 365	96 369	96 374	3
	9.20	.96 379	.96 3 84	.96 388	.96 393	.96 398	.96 402	.96 407	.96 412	.96 417	.96 421	5
	.21			96 435		96 445	96 450	96 454	96 459	96 464	96 468	I
	.22			96 483			96 497	96 501	96 506	96 511	96 515	1
`	.23		96 525						96 553			2
	.24	1		96 577					96 6 00	-	-	2
- 1	9.25			.96 624			.96 638	.96 642	.96 647	.96 652	.96 656	3
	.26			96 670			96 685	96 689	96 694	96 699	96 703	3
ł	.27			96 717			96 731	96 736	96 741	96 745	96 750	4
	.28	96 755	96 759 96 806	96 764 96 811	96 816	96 774 96 8 20	96 778 96 825	96 830	96 788 96 8 3 4	96 839	90 797 96 844	4 5
	9.30	.06 848	.06 853	.96 858	.06 862	.96 867			.96 881			4
	.31			96 904					96 928			o
	.32			96 951					96 974			I
	•33	96 988	96 993	96 997	97 002	97 007	97 01 1	97 016	97 021	97 025	97 030	I
	•34	97 °35	9 7 039	97 044	97 049	97 °53	97 058	97 063	97 067	97 072	97 °77	2
	9.35	.97 081	.97 086	.97 090	.97 095	.97 100	.97 104	.97 109	.97 114	.97 118	.97 123	2
	.36			97 137			97 151	97 ¹ 55	97 160	97 165	97 169	2
ı	•37			97 183					97 206			3
	.38			97 230			97 2 43		97 253			3
	.39	97 267	97 271	97 276	97 280	97 285	97 290	9 7 2 94	97 299	97 304	97 308	4
	9.40			.97 322			.97 336		·97 345 97 391			5
	.41 .42			97 368 97 414			-		97 437			I
ı	.43			97 460					97 483			2
	.44			97 506					97 529			2
	9.45			.97 552			.97 566					3
.95	.46	97 589	97 594	97 598	97 603	97 607			97 621			3
.99	.47	97 635	97°640	97 644	97 649	97 653			97 667			4
1	.48			97 690					97713			4
	∙49	97 727	97 73 1	97 736	97 740	97 745	97 7 49	97 754	97 759	97 763	97 768	5

FIVE PLACE LOGARITHMS.

5 PL. LOGS.

										O PL.	LU	, J
No.	0	I	2	3	4	5	6	7	8	9	INTP. TAB.	
9.50	.97 772	-97 777	.97 782	.97 786	.97 791	.97 795	.97 800	.97 804	.97 809	.97 813	4	.95
.51				97 832					97 ⁸ 55		0	.99
.52				97 877			-, -	-, -	97 900		I	
·53				97 923					97 946		1	i
∙54	1		-	97 968					97 991		2	
9.55				.98 014					.98 037		2	i
.56				98 059 98 105					98 0 82 98 127		2	i
·57 ·58			-	98 150					98 173	_	3	i
.59				98 195					98 218		4	i
.39	_								-	-	1	i
9.60				.98 241					.98 263		5	i
.61				98 286					98 308		I	i
.62				98 331 98 376					98 3 5 4 98 399		1 2	ĺ
.63 .64	1			98 421					98 444		2	
	1 ' '			.98 466					.98 489			
9.65 .66				98 511					98 534		3	ı
.67				98 556					98 579		3 4	i
.68				98 601					98 623		4	ı
.69				98 646		-		-	98 668	-	5	İ
9.70	.98 677	.98 682	.98 686	.98 691	.98 695	.98 700	.98 704	.98 709	.98 713	.98 717	4	İ
.71				98 735					98 758		0	
.72				98 780					98 802		1	
·73				98 825					98 847		I	
·74				98 869	-				98 892		2	
9.75				.98 914					.98 936		2	
.76				98 958					98 981		2	ĺ
.77				99 003 99 047					99 025 99 069		3	i
.78 .79				99 047		-			99 114		3 4	İ
9.80	İ			.99 136						.99 162	5	
.81				99 180					99 202		I	
.82				99 224	0				99 247		ī	
.83				99 269					99 291		2	Í
.84	99 300	99 304	99 308	99 313	99 317	99 322	99 3 2 6	99 330	99 335	99 339	2	ĺ
9.85	-99 344	.99 348	99 352	.99 357	.99 361	.99 366	.99 370	.99 374	.99 379	.99 383	3	İ
.86				99 401					99 423		3	
.87				99 445					99 467		4	
.88	99 476	. 99 480	99 484	99 489	99 493				99 511		4	İ
.89	99 520	99 52 4	99 528	99 533	99 537	99 542	99 546	99 550	99 555	99 559	5	
9.90				-99 577					.99 599		4	
.91				99 621					99 642		0	
.92				99 664					99 686		I	
·93				99 708					99 730	_	I	
•94		99 743			99 756		99 765			99 778	2	
9.95				.99 795					.99 817		2	
.96				99 839					99 86 1 99 904		2	.95
·97 .98				99 883 99 926					99 904		3	.99
.99				99 920					99 948 99 99 1		3 4	
99	22 Y3/	77 7 ⁰¹	77 7°5	77 7 /º	JJ 9/4	99910	77 9°3	77 YU/	77 77ª	23 39 ⁰	4	ı

5 PL. LOGS

SQUARE ROOTS AND SQUARES.

Note. The table gives roots directly, squares by inverse interpolation.

No.	0	I	2	3	4	5	6	7	8	9	Interp	oola. sandths.
1.0	1.000	1.005	010.1	1.015	1.020	1.025	1.030	1.034	1.039	1.044	5	4
.ı	1.049	1.054	1.058	1.063	1.068	1.072	1.077	1.082	1.086	1.091	1	О
.2	1.095	1.100	1.105	1.109			I.I22	1.127	1.131	1.136	1	I
∙3		1.145		1.153	1.158	1.162	1.166	1.170	1.175	1.179	2	1
٠4	1.183	1.187	1.192	1.196	1.200	1.204	1.208	1,212	1.217	1.221	2	2
1.5	1.225	1.229	1.233	1.237	1.241	1.245	1.249	1.253	1.257	1.261	3	2
.6		1.269		1.277	1.281	1.285	1.288	1.292	1.296	1.300	3	2
.7	- '	-	1.311	1.315	1.319	1.323	٠.	1.330	1.334	1.338	4	3
.8		1.345		1.353	1.356	1.360	1.364	1.367	1.371	1.375	4	3
.9	1.378	1.382	1.386	1.389	1.393	1.396	1.400	1.404	1.407	1.411	5	4
2.0	1.414	1.418	1.421	1.425	1.428	1.432	1.435	1.439	1.442	1.446	4	3
.1	1.449	1.453		1.459	1.463	1.466	1.470	1.473	1.476		0	0
.2	1.483	1.487	1.490	1.493	1.497	1.500	1.503	1.507	1.510		1	1
-3	1.517	1.520	1.523	1.526	1.530	1.533		1.539	1.543	1.546	1	I
-4	1.549	1.552	1.556	1.559	1.562	1.565	1.568	1.572	1.575	1.578	2	I
2.5	1.581	1.584	1.587	1.591	1.594	1.597	1.600	1.603	1.606	1.600	2	2
.6	1.612	1.616	1.619	1.622	1.625	1.628	1.631	1.634	1.637	1,640	2	2
.7	1.643	1.646	1.649	1.652	1.655	1.658		1.664	٠.		3	2
.8	1.673	1.676	1.679	1.682	1.685	1.688	1.691	1.694	1.697	1.700	3	2
.9	1.703	1.706	1.709	1.712	1.715	1.718	1.720	1.723	1.726	1.729	4	3
3.0	1 722	1.735	1.738	1.741	1.744	1.746	1 740	1.752	1 766	1.758	3	2
1.	, , -	1.764		1.769	,	1.775		1.780		• •	0	0
.2	• -	1.792		1.797		1.803		1.808		1.814	ī	0
•3		1.819		1.825	1.828	J	1.833		1.838	1.841	1	I
•4		1.847		1.852	1.855	1.857		1.863		1.868	1	r
3.5	1 871	1.873		1.879	1.881	1 884	1.887	T 880	1.892	1 80E	2	I
.6		1.900	•	1.905	1.908			1.916		1.921	2	1
.7	1.924		1.929	1,931	1.934		1.939		I.944	-	2	I
.8		-	1.954	1.957	1.960	1.962	1.965	1.967		1.972	2	2
.9	1.975	1.977	1.980	1.982	1.985	1.987	1.990	1.992		1.997	3	2
140	2.000	2.002	2.00	2 00	2010	2.012	2011	2017	2 020	2 022	3	2
4.0	2.025		2.005			2.012		•	2.020	2.022	Ö	0
.2	2.025		•	2.057	05	2.062			2.069		ĭ	0
-3	2.074	•	2.078			2.086	2.088		2.003	•	ī	ī
·4	2.098	•	2.102	2.105	2.107	2.110	2.112	2.114	2.117		ī	I
4.5	2.121		2.126	2.128	2.131	2.133	2.135	•	2.140	2.142	2	Ţ
.6	2.121	•	2.149		•		2.135	_	2.140		2	ï
.7	2.145			2.175	2.177	2.179	-		2.186		2	I
.8	2.191	,		2.198		2.202			2.209	_	2	2
.9	2.214		2.218	-		2.225		•	2.232		3	2
٠,۶					3				3-	JT		

SQUARE ROOTS AND SQUARES. 1.-10. SQ. RTS. & SQRS.

<u> </u>	1									Q. KI		361
No.	0	I	2	3	4	5	6	7	8	9		ola, for andths.
5.0	2.236	2.238	2.241	2,243	2.245	.2.247	2.249	2.252	2.254	2.256	3	2
.1	2.258	2.261	2.263	2.265	2.267	2.269	2.272	2.274	2.276	2.278	0	0
.2					2.2 89	2.291	2.293	2.296	2.298	2.300	1	0
•3	2.302	2.304	2.307	2.309	2.311	2.313	2.315	2.317	2.319	2.322	I	I
•4	2.324	2.326	2.328	2.330	2.332	2.335	2.337	2.339	2.341	2.343	I	I
5.5	2.345	2.347	2.349	2.352	2.354	2.356	2.358	2.360	2.362	2.364	2	Ţ
.6	2.366	2.3 69	2.371	2.373	2.375	2.377	2.379	2.381	2.383	2.385	2	I
-7	2.387	2.390	2.392	2.394	2.396	2.398	2.400	2.402	2.404	2.406	2	I
.8					2.417		2.421				2	2
.9	2,429	2.431	2.433	2.435	2.437	2.439	2.44I	2.443	2.445	2.447	3	2
6.0				2.456			2.462				3	2
I.				2.476		2.480	2.482	2.484	2.486	2.488	0	О
.2					2,498		2.502		•		1	0
•3	-	-	-	2.516	-	_	2.522	-	-		I	I
•4	_	-	_	2.536	2.538	2.540	2.542	2.544	2.546	-	I	1
6.5	2.550	2.551	2.553	2.555	2.557		2.561			2.567	2	I
.6	2.569	2.571	2.573	2.575	2.577		2.581				2	I
•7					2.596		2.600				2	I
٠8					2.615		2.619				2	2
.9	2.627	2.629	2.631	2.632	2.634	2.636	2.638	2.640	2.642	2.644	3	2
7.0	2.646	2.648	2.650	2.651	2.653	2.655	2.657	2.659	2.661	2.663	2	1
I.				2.670		2.674	2.676	2.678	2.680	2.681	0	О
.2	2.683	2.685	2.687	2.689	2.691	2.693	2.694	2.696	2.698	2.700	0	0
٠3				2,707	2.709	2.711	2.713	2.715	2.717	2.718	1	0
•4	2.720	2.722	2.724	2.726	2.728	2.729	2.731	2.733	2.735	2.737	1	0
7.5	2.739	2.740	2.742	2.744	2.746	2.748	2.750	2.751	2.753	2.755	1	1
.6	2.757	2.759	2.760	2.762	2.764		2.768				1	I
.7	2.775	2.777	2.778	2.780	2.782	2.784	2.786	2.787	2.789	2.791	1	I
.8	2.793	2.795	• •	2.798		2.802	2.804	2.805	2.807	2.809	2	I
.9	2.811	2.812	2.814	2.816	2.818	2.820	2.821	2.823	2.825	2.827	2	I
8.0	2.828	2.830	2.832	2.834	2.835	2.837	2.839	2.841	2.843	2.844	2	1
ı.				2.851		2.855	2.857	2.858	2.860	2.862	0	О
.2				2.869			2.874				0	0
•3				2.886	2.888	2.890	2 .891	2.893	2.895	2.897	I	0
•4	2.898	2.900	2.902	2.903	2.905	2.907	2.909				I	О
8.5	2.915	2.917	2.919	2.921	2.922	2.924	2.926	2.927	2,929	2.931	1	I
.6				2.938	2. 939	2.941			2.946	_	1	I
.7	2.950	2.951	2.953	2.955	2.956		2. 960	2.961	2.963	2.965	1	I ·
.8	2.966	2.968	2.970	2.972	2.973	2.975			2. 980		2	1
•9	2.983	2.985	2.987	2.988	2.990	2.992	2.993	2.995	2.997	2.998	2	I
9.0	3.000	3.002	3.003	3.005	3.007	3.008	3.010	3.012	3.013	3.015	2	1
.ı				3.022		3.025	3.027	3.028	3.030	3.032	0	0
.2				3.038			3.043				0	0
-3				3.055		3.058	3.059	3.061	3.063	3.064	I	0
•4	3.066	3.068	3. 069	3.071	3.072	3.074	3.076	3.077	3.079	3.081	1	0
9.5				3.087		3.090	3.092	3.094	3.095	3.097	I	1
.6	3.098	3.100	3.102	3.103	3.105		3.108				I	I
.7	3.114	3.116	3.118	3.119	3.121		3.124				I	1
.8	3.130	3.132	3.134	3.135	3.137		3.140				2	I
.9	3.146	3.148	3.150	3.151	3.153	3.154	3.156	3.158	3.159	3.161	2	1
											•	

SQUARE ROOTS AND SQUARES.

No.	0	I	2	3	4	5	6	7	8	9		rpola, ndredths.
10.	3.162	3.178	3.194	3.209	3.225	3.240	3.256	3.271	3.286	3.302	16	14
11.	3.317		3.347	3.362	3.376	3.391	3.406	3.421	3.435	3.450	2	1
I 2.	3.464		3.493	3.507	3.521	3.536	3.550	3.564	3.578	3.592	3	3
13.	3.606	3.619	3.633	3.647	3.661	3.674		3.701	3.715	3.728	5	4
14.	3.742	3-755	3.768	3.782	3.795	3.808	3.821	3.834	3.847	3.860	6	6
15.	3.873	3.886	3.899	3.912	3.924	3.937	3.950	3.962	3.975	3.987	8	7
16.	4.000		4.025	4.037	4.050	4.062	4.074		4.099		10	8
17.	4.123	4.135	4.147	4.159	4.171	4.183	4.195		4.219		11	10
18.	4.243		4.266		4.290	4.301	4.313	4.324	4.336	4.347	13	11
19.	4.359	4.370	4.382	4.393	4.405	4.416	4.427	4.438	4.450	4.461	14	13
20.	4.472	4.483	4.494	4.506	4.517	4.528	4.539	4.550	4.561	4.572	12	10
21.		4.593		4.615		4.637		4.658			ı	1
22.			4.712		-	4.743			4.775		2	2
23.	4.796	4.806	4.817	4.827	4.837	4.848	4.858	4.868	4.879	4.889	-4	3
24.	4.899	4.909	4.919	4.930	4.940	4.950	4.960	4.970	4.980	4.990	5	4
25.	5.000	5.010	5.020	5.030	5.040	5.050	5.060	5.070	5.079	5.089	6	5 .
26.	5.099	5.109	5.119	5.128				5.167	5.177		7	6
27.	5.196	5.206	5.215	5.225	5.235	5.244		5.263		5.282	. 8	7
28.	5.292	5.301	5.310	5.320	5.329	5.339		5-357	5.367	5.376	10	8
29.	5.385	5.394	5.404	5.413	5.422	5.431	5.441	5.450	5.459	5.468	11	9
30.	5.477	5.486	5.495	5.505	5.514	5.523	5.532	5.541	5.550	5.559	9	8
31.	5.568		5.586	5.595				5.630			I	I
32.	5.657	5.666		5.683	5.692	5.701		5.718			2	2
33.	5.745	5.753		5.771	5.779		5.797	5.805	5.814	5.822	3	2
34.	5.831		5.848	5.857	5.865	5.874	5.882	5.891	5.899	5.908	4	3
35.	5.916	5.925	5.933	5.941	5.950	5.958	5.967	5.975	5.983		5	4
36.			6.017			6.042	6.050	6.058	6.066	6.075	5 6	5
37•					6.116		6.132	6.140	6.148	6.156		6
38.	6.164	6.173	6.181	6.189	6.197	6.205	6.213	6.221	6.229	6.237	7	6
39.	6.245	6.253	6.261	6.269	6.277	6.285	6.293	6.301	6.309	6.317	8	7
40.	6.325	6.332	6.340	6.348	6.356			6.380			8	7
41.	6.403	6.411	6.419	6.427	6.434			6.458			I	I
42.	6.481	6.488	6.496	6.504	6.512			6.535			2	I
43.	6.557	6.565	6.573	6.580	6.588	6.595		6.611			2	2
44.			6.648			-		6.686	_		3	3
45.	6.708	6.716	6.723	6.731	6.738	6.745		6.760			4	4
46.	6.782	6.790	6.797	6.804	6.812			6.834			5	4
47.	6.856	6.863	6.870	6.877	6.885			6.907			6	5
48.			6.943					6.979			6	6
49.	7.000	7.007	7.014	7.021	7.029	7.036	7.043	7.050	7.057	7.064	7	6

SQ. RTS. & SQRS. 10.-100.

SQUARE ROOTS AND SQUARES. 10.-100. SQ. RTS. & SQRS.

50. 7.071 7.078 7.085 7.092 7.099 7.106 7.113 7.120 7.127 7.134 7.16 51. 7.141 7.148 7.155 7.162 7.169 7.176 7.183 7.190 7.197 7.204 52. 7.211 7.225 7.232 7.239 7.246 7.253 7.259 7.266 7.273 53. 7.285 7.287 7.294 7.301 7.305 7.314 7.21 7.328 7.329 7.266 7.273 53. 7.285 7.287 7.294 7.301 7.305 7.314 7.321 7.328 7.335 7.342 2 2 2 53. 7.285 7.287 7.294 7.301 7.305 7.314 7.312 7.328 7.335 7.342 2 2 54. 7.348 7.355 7.362 7.369 7.376 7.352 7.389 7.396 7.403 7.409 3 2 55. 7.416 7.423 7.430 7.436 7.443 7.450 7.457 7.533 7.530 7.537 7.543 4 4 56. 7.483 7.490 7.497 7.503 7.510 7.516 7.583 7.590 7.596 7.603 7.609 58. 7.616 7.622 7.629 7.635 7.642 7.649 7.655 7.656 7.665 7.657 6 58. 7.616 7.622 7.629 7.635 7.642 7.649 7.655 7.656 7.665 7.675 6 58. 7.616 7.622 7.629 7.635 7.642 7.649 7.655 7.656 7.665 7.675 6 59. 7.681 7.688 7.694 7.701 7.707 7.714 7.720 7.727 7.733 7.740 6 50. 7.316 7.817 7.832 7.839 7.839 7.387 7.844 7.980 7.887 7.893 7.899 7.396 7.912 7.918 7.925 7.931 1 1 61. 7.816 7.817 7.832 7.839 7.899 7.396 7.912 7.918 7.925 7.931 1 1 62. 7.874 7.880 7.887 7.893 7.899 7.396 7.912 7.918 7.925 7.991 1 1 63. 7.937 7.944 7.950 7.956 7.962 7.969 7.912 7.918 7.925 7.991 1 1 64. 8.000 8.006 8.012 8.019 8.025 8.031 8.319 8.198 8.294 8.210 8.128 8.214 8.130 8.136 8.142 8.149 8.155 8.161 8.167 8.173 8.179 64. 8.000 8.006 8.018 8.087 65. 8.246 8.252 8.258 8.264 8.270 8.276 8.238 8.289 8.295 8.301 6 65. 8.246 8.252 8.258 8.264 8.270 8.276 8.283 8.289 8.295 8.301 6 6 6 6 7.746 7.755 8.751 8.756 8.792 8.798 8.793 8.794 8.799 7.916 8.292 8.918 8.909 8.313 8.319 8.389 8.389 8.390 8.330 8.340 8.355 8.361 8.697 8.606 8.666 8.672 8.678 8.683 8.693 8.693 8.15 8.820 8.201 8.217 8.228 8.238 8.829 8.839 8.394 8.394 8.395 8.995 8.911 8.916 8.922 8.927 8.933 8.939 70. 8.486 8.491 8.497 8.503 8.509 8.313 8.340 8.343 8.349 8.859 8.859 8.910 9.006 9.011 9.017 9.022 9.028 9.032 9.033 9.044 9.099 9.105 1 1 1 1 2 2 3 3 3 3 3 3 3	No.	0	I	2	3	4	5	6	7	8	9	Interpo	la. for edths.
1	50	7.071	7.078	7.081	7.002	7 000	7 106	7 112	# 140	2.102	H T24		
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•4	7143	7092	7042	6993	6944	6897	6849	6803	6757	6711	18 14		9
1.5			0.6579	0.6536		0.6452				0.6289	23 18	13	ΙΙ
.6	6250	6211	6173	6135	6098	6061	6024	5988	5952	5917	27 21	-	-
.7	5882	5848	5814	5780	5747	5714	5682	5650	5618	5587	32 25		
.8	5556	5525	5495	5464	5435	5405	5376	5348	5319	5291	36 28		
•9	5263	5236	-	5181	5155	5128	5102	5076	5051	5025	41 32	23	20
2.0	1 -		0.4950	•••	•••	0.4878			0.4808		-18-16	-14-	12
.I	4762	4739		4695	4673	4651	4630	4608	4587	4566	2 2	1	1
.2	4545	4525	4505	4484	4464	4444	4425	4405	4386	4367	4 3	3	2
•3	4348	4329		4292	4274	4255	4237	4219	•	4184	5 5		4
٠4	4167	4149		4115	4098	4082	4065	4049	4032	4016	7 6	6	5
2.5			0.3968	0.3953		0.3922	0.3906	0.3891	0.3876	0.3861	9 8	7	6
.6	3846		3817	3802	3788	3774	3759	3745	3731	3717	11 10	8	7
.7	3704		٠.,	3663	3650	3636	3623	3610	3597	3584	13 11	10	8
.8	3571	3559	3546	3534	3521	3509	3497	3484	3472	3460	14 13		
.9	3448			3413	3401	3390	3378	3367	3356	3344	16 14	13	11
3.0	0.3333	0.3322	0.3311	0.3300	0.3289	0.3279	0.3268	0.3257	0.3247	0.3236	-11 -9	-8	-7
Ι.	3226	3215	3205	3195	3185	3175	3165	3155	3145	3135	1 1	I	1
.2	3125	3115	3106	3096	3086	3077	3067	3058	304 9	3040	2 2	2	I
.3	3030	3021	3012	3003	2994	2985	2976	2967	2959	2950	3 3	2	2
٠4	2941	2933	2924	2915	2907	2899	2890	2882	2874	2865	4 4	3	3
3.5	0.2857	0.2849	0.2841	0.2833	0.2825	0.2817	0.2809	0.2801	0.2793	0.2786	6 5	4	4
.6	2778	2770	2762	2755	2747	2740	2732	2725	2717	2710	7 5	5	4
7	2703	2695	2688	2681	2674	2667	2660	2653	2646	2639	8 6	_	5
.8	2632	2625	2618	261 I	2604	2597	2591	2584	2577	2571	9 7		6
•9	2564	2558	2551	2545	2538	2532	2525	2519	2513	2506	10 8	7	6
4.0	0.2500					0.2469					-6 -5		
.1	2439	2433	2427	2421	2415	2410	2404	2398	2392	2387	I I		
.2	2381	2375	2370	2364	2358	2353	2347	2342	2336	2331	II		
.3	2326	2320	2315	2309	2304	2299	2294	2288	2283	2278	2 2		
.4	2273	2268	2262	2257	2252	2247	2242	2237	2232		2 2		
4.5	0.2222					0.2198			_		3 3		
.6	2274	2169	2165	2160	2155	2151	2146		2137	2132	4 3		
.7	2128	2123	2119	2114	2110	2105	2101	2096	2092	2088	4 4	_	
.8	2083	2079	2075	2070	2066	2062	2058	2053	2049	2045	5 4		
۰9	2041	2037	2033	2028	2024	2020	2016	2012	2008	2004	5 5	4	

RECIP.

No.	0	I	2	3	4	5	6	7.	8	9		POLATION THOUS.
5.0	0.2000	0.1996	0.1992	0.1988	0.1984	0.1980	0.1976	0.1972	0.1969	0.1965	-4	-3
J.U	1961	1957	1953	1949	1946	1942	1938	1934	1931	1927	0	0
.2	1923	1919	1916	1912	1908	1905	1901	1898	1894	1890	1	I
•3	1887	1883	1880	1876	1873	1869	1866	1862	1859	1855	1	I
•4	1852	1848	1845	1842	1838	1835	1832	1828	1825	1821	2	1
5.5	0.1818		0.1812		0.1805	0.1802		0.1795		0.1789	2	2
.6	1786	1783	1779	1776	1773	1770	1767	1764	1761	1757	2	2
•7	1754	1751	1748	1745	1742	1739	1736	1733	1730	1727	3	2
.8	1724	1721	1718 1689	1715 1686	1712 1684	1709 1681	1706	1704	1701	1698 1669	3	2
•9	1695	1692	1009	1000	1004	- 1001 -	1678	1675	1672	1009	4	3
6.0	0.1667	0.1664	0.1661	0.1658	0.1656	0.1653	0.1650	0.1647	0.1645	0.1642	3	-2
.I	1639	1637	1634	1631	1629	1626	1623	1621	1618	1616	0	0
.2	1613	1610	1608	1605	1603	1600	1597	1595	1592	1590	1	0
•3	1587	1585	1582	1580	1577	¹ 575	1572	1570	1567	1565	I	I
•4	1563	1560	1558	1555	1553	1550	1548	1546	1543	1541	1	I
6.5	0.1538	0.1536	0.1534		- ·	0.1527	0.1524	0.1522	0,1520	0.1517	2	1
.6	1515	1513	1511	1508	1506	1504	1502	1499	1497	1495	2	1
•7	1493	1490	1488	1486	1484	1481	1479	1477	1475	1473	2	I
.8	1471	1468	1466	1464	1462	1460	1458	1456	1453	1451	2	2
•9	1449	1447	1445	1443	1441	1439	1437	1435	1433	1431	3	2
7.0	0.1429	0.1427	0.1425	0.1422	0.1420	0.1418	0.1416	0,1414	0.1412	0.1410	-2	-1
1,	1408	1406	1404	1403	1401	1399	1397	1395	1393	1391	О	0
.2	1389	1387	1 385	1383	1381	1379	1377	1376	1374	1372	0	0
•3	1370	1368	1 366	1 364	1362	1361	1359	1357	1355	1353	1	0
٠4	1351	1350	1348	1346	I 344	1342	1340	1339	1337	1335	1	0
7.5	0.1333	0.1332	0.1330	0.1 328 (0.1326	0.1325	0.1 323 0	0.1321	0.1319	0.1318	1	1
.6	1316	1314	1312	1311	1 309	1 307	1 305	1304	1302	1300	1	1
.7	1299	1297	1295	1294	1292	1290	1289	1287	1285	1284	1	1
.8	1282	1280	1279	1277	1276	1274	1272	1271	1269	1267	2	I
.9	1266	1264	1263	1261	1259	1258	1256	1255	1253	1252	2	1
8.0	0.1250	0.1248	0.1247	0.1245	0.1244	0.1242	0.1241	0.1239	0.1238	0.1236	-2	-1
.I	1235	1233	1232	1230	1229	1227	1225	1224	1222	1221	0	0
.2	1220	1218	1217	1215	1214	1212	1211	1209	1208	1206	0	0
•3	1205	1203	1202	1200	1199	1198	1196	1195	1193	1192	I	0
•4	1190	1189	1188	1186	1185	1183	1182	1181	1179	1178	I	0
8.5	0.1176	0.1175	0.1174	0.1172	0.1171	0.1170	o.1168 c	0.1167	0.1166	0.1164	1	I
.6	1163	1161	1160	1159	1157	1156	1155	1153	1152	1151	1	I
•7	1149	1148	1147	1145	1144	1143	1142	1140	1139	1138	1	1
.8	1136	1135	1134	1133	1131	1130	1129	1127	1126	1125	2	I
.9	1124	1122	1121	1120	1119	1117	1116	1115	1114	1112	2	ľ.
9.0	011110	0.1110	0.1109	0.1107	0.1106	0.1105	0.1104	0,1103	0.1101	0,1100	-2	-1
.I	1099	1098	1096	1095	1094	1093	1092	1091	1089	1088	0	0
.2	1087	1086	1085	1083	1082	1801	1080	1079	1078	1076	0	0
•3	1075	1074	1073	1072	1071	1070	1068	1067	1066	1065	1	0
•4	1064	1063	1062	1060	1059	1058	1057	1056	1055	1054	I	0
9.5	0.1053		0.1050		0.1048	0.1047	0.1046		0,1044	0.1043	I	1
.6	1042	1041	1040	1038	1037	1036	1035	1034	1033	1032	1	I
.7	1031	1030	1029	1028	1027	1026	1025	1024	1022	1021	I	I
.8	1020	1019	1018	1017	1016	1015	1014	1013	1012	1011	2	I
.9	1010	1009	1008	1007	1006	1005	1004	1003	1002	1001	2	1

(35) RECIP.

SLIDE-WIRE RATIOS.

S. W. RATIOS.

cm.	Omm.	ımm.	2 ^{mm} ·	3 ^{mm} ·	4 ^{mm} ·	5 ^{mm.}	6 _{шш} .	7 ^{mm} .	8mm.	9 ^{mm} .
0	0.0000	0,0010	0,0020	0.0030	0,0040	0.0050	0,0060	0.0071	1800,0	0.0091
I	0101	OIII	0122	0132	0142	0152	0163	0173	0183	0194
2	0204	0215	0225	0235	0246	0256	0267	0278	0288	0299
3	0309	0320	0331	0341	0352	0363	0373	0384	0395	0406
4	0417	0428	0438	0449	0460	0471	0482	0493	0504	0515
5	0.0526	0.0537	0.0549	0.0560	0.0571	0.0582	0.0593	0.0605	0.0616	0.0627
6	0638	0650	0661	0672	0684	0695	0707	0718	0730	0741
7	0753	0764	0776	0788	0799	0811	0823	0834	0846	0858
8	0870	0881	0893	0905	0917	0929	0941	0953	0965	0977
9	0989	1001	1013	1025	1038	1050	1062	1074	1087	1099
10	0.1111	0.1124	0.1136	0.1148		0.1173	0.1186	0.1198	0,1211	0.1223
11	1236	1249	1261	1274	1287	1299	1312	1325	1338	1351
12	1364	1377	1390	1403	1416	1429	1442	1455	1468	1481
13	1494	1508		1534	1547	1561	1574	1588	1601	1614
14	1628	1641	1655	1669	1682	1696	1710	1723	1737	1751
15	0.1765	0.1779	0.1793	0.1806	0.1820	0.1834	0.1848	0.1862	0.1877	0.1891
16	1905	1919	1933	1947	1962	1976	1990	2005	2019	2034
17	2048	2063	2077	2092	2107	2121	2136	2151	2166	2180
18	2195	2210	2225	2240	2255	2270	2285	2300	2315	2331
19	2346	2361	2376	2392	2407	2422	2438	2453	2469	2484
20	0.2500	0.2516	0.2531	0.2547	0.2563	0.2579	0.2595	0.2610	0.2626	0.2642
21	2658	2674	2 690	2707	2723	2739	2755	2771	2788	2804
22	2821	2837	2854	2870	2887	2903	2920	2937	2953	2970
23	2987	3004	3021	3038	3055	3072	30 89	3106	3123	3141
24	3158	3175	3193	3210	3228	3245	3263	3280	3298	3316
25	0.3333	0.3351	0.3369			0.3423		0.3459	0.3477	0.3495
26	3514	3532	3550	3569		3605	3624	3643	3661	368o
27	3699	3717	3736	3755	3774	3793	3812	3831	3850	3870
28	3889	3908	3928	3947	3967	3986	4006	4025	4045	4065
29	4085	4104	4124	4144	4164	4184	4205	4225	4245	4265
30	0.4286	0.4306	0.4327	0.4347	0.4368	0.4389	0.4409	0.4430	0.4451	0.4472
31	4493	4514	4535	4556	4577	4599	4620	464 I	4663	4684
32	4706	4728	4749	4771	4793	4815	4837	4859	4881	4903
33	4925	4948	4970	4993	5015	5038	5060	5083	5106	5129
34	5152	5175	5198	5221	5244	5267	5291	5314	5337	5361
35	0.5385		0.5432			0.5504	0.5528	0.5552		0.5601
36	5625	5650	5674	5699	5723	5748	5773	5798	5823	5848
37	5873	5898	5924	5949	5974	6000	6026	6051	6077	6103
38	6129	6155	6181	6208	6234	6260	6287	6313	6340	6367
39	6393	6420	6447	6475	6502	6529	6556	6584	6611	6639
40	0.6667	0.6695	-				0.6835		0.6892	
41	6949	6978	7007	7036	7065		7123			
42	7241	7271	7301	7331	7361 7668	7391	7422	7452	7483	7513
43	7544	7575	7606	7637	7668 7086	7699 8018	7731	7762 8082	7794 8116	7825 8149
44	7857	7889	7921	7953	7986		8051	8083	8116	
45		0.8215		0.8282		0.8349	_			0,8484
46	8519	8553	8587	8622	8657	8692	8727	8762	8797	8832
47	8868	8904	8939	8975	9011	9048	9084	9121	9157	9194
48	9231	9268	9305	9342	9380 0762	9418 9802	9455	9493	9531	9570 0060
49	9608	9646	9685	9724	9763	9002	9841	9881	9920	9960

SLIDE-WIRE RATIOS.

S. W. RATIOS.

cm.	Omm.	Imm.	2 ^{mm} .	3 _{mm} .	4 ^{mm} .	5 ^{mm} ·	6 ^{mm} .	7 ^{mm} ·	8mm.	9 ^{mm} .
50	1.000	1.004	1.008	1.012	1,016	1.020	1.024	1.028	1.033	1.037
51	1.041	1.045	1.049	1.053	1.058	1.062	1.066	1.070	1.075	1.079
52	1.083	1.088	1.092	1.096	1.101	1,105	1.110	1.114	1.119	1.123
53	1.128	1.132	1.137	1.141	1.146	1.151	1.155	1.160	1.165	1.169
54	1.174	1.179	1.183	1.188	1.193	1.198	1.203	1.208	1.212	1.217
55	1.222	1.227	1.232	1.237	1.242	1.247	1.252	1.257	1.262	1.268
56	1.273	1.278	1.283	1.288	1.294	1.299	1.304	1.309	1.315	1.320
57	1.326	1.331	1.336	1.342	1.347	1.353	1.358	1.364	1.370	1.375
58	1.381	1.387	1.392	1.398	1.404	1,410	1.415	1,421	1.427	1.433
59	1.439	1.445	1.451	1.457	1.463	1.469	1.475	1.481	1.488	1.494
60	1.500	1.506	1.513	1.519	1.525	1.532	1.538	1.545	1.551	1.558
61	1.564	1.571	1.577	1.584	1.591	1.597	1.604	1.611	1.618	1.625
62	1.632	1.639	1.646	1.653	1.660	1.667	1.674	1.681	1.688	1.695
63	1.703	1.710	1.717	1.725	1.732	1.740	1.747	1.755	1.762	1.770
64	1.778	1.786	1.793	1.801	1.809	1.817	1.825	1.833	1.841	1.849
65	1.857	1.865	1.874	1.882	1.890	1.899	1.907	1.915	1.924	1.933
66	1.941	1.950	1.959	1.967	1.976	1.985	1.994	2.003	2.012	2.021
67	2.030	2.040	2.049	2.058	2.067	2.077	2.086	2.096	2.106	2.115
68	2.125	2.135	2.145	2.155	2.165	2.175	2.185	2.195	2.205	2.215
69	2.226	2.236	2.247	2.257	2.268	2.279	2.289	2.300	2.311	2.322
70	2.333	2.344	2.356	2.367	2.378	2.390	2.401	2.413	2.425	2.436
7I	2.448	2.460	2.472	2.484	2.497	2.509	2.521	2.534	2.546	2.559
72	2.571	2.584	2.597	2.610	2.623	2.636	2.650	2.663	2.676	2.690
73	2.704	2.717	2.731	2.745	2.759	2.774	2.788	2.802	2.817	2.831
74	2.846	2.861	2.876	2.891	2. 906	2.922	2.937	2.953	2.968	2.984
75	3.000	3.016	3.032	3.049	3.065	3.082	3.098	3.115	3.132	3.149
76	3.167	3.184	3.202	3.219	3.237	3.255	3.274	3.292	3.310	3.329
77	3.348	3.367	3.386	3.405	3.425	3.444	3.464	3.484	3.505	3.525
78	3.545	3.566	3.5 87	3.608	3.6 <i>3</i> 0	3.651	3.673	3.695	3.717	3.739
79	3.762	3.785	3.808	3.831	3.854	3.878	3.902	3.926	3.950	3.975
80	4.000	4.025	4.051	4.076	4.102	4.128	4.155	4.181	4.208	4.236
81	4.263	4.291	4.319	4.348	4.376	4.405	4.435	4.465	4.495	4.525
82	4.556	4.587	4.618	4.650	4.682	4.714	4.747	4.780	4.814	4.848
83	4.882	4.917	4.952	4.988	5.024	5.061	5.098	5.135	5.173	5.211
84	5.250	5.289	5.329	5.369	5.410	5.452	5.494	5.536	5.579	5.623
85	5.667	5.711	5.757	5.803	5.849	5.897	5.944	5.993	6.042	6.092
86	6.143	6.194	6.246	6.299	6.353	6.407	6.463	6.519	6.576	6.634
87	6.692	6.752	6.813	6.874	6.937	7.000	7.065	7.130	7.197	7.264
88	7.333	7.403	7.475	7.547	7.621	7.696	7.772	7.850	7.929	8.009
89	8.091	8.174	8.259	8.346	8.434	8.524	8.615	8.709	8.804	8.901
90	9.000	9.101	9.204	9.309	9.417	9.526	9.638	9.753	9.870	9.989
91	10.11	10.33	10.36	10.49	10.63	10.77	10.90	11.05	11.20	11.35
92	11.50	11.66	11.82	11.99	12.16	12.33	12.51	12.70	12.89	13.08
93	13.29	13.49	13.71	13.93	14.15	14.38	14.63	14.87	15.13	15.39
94	15.67	15.95	16.24	16.54	16.86	17.18	17.52	17.87	18.23	18.61
95	19.00	19.41	19.83	20.28	20.74	21.22	21.73	22.26	22.81	23.39
96	24.00	24.64	25.32	26.03	26.78	27.57	28.41	29.30	30.25	31.26 46.62
97 98	32.33	33.48 51.6	34.71 54.6	36.04 57.8	37.46 61.5	39.00 65.7	40.67 7 0. 4	42.48 75.9	44.45 82.3	89.9
98	49.00 99.0	110.	124.	142.	166.	199.	249.	73·9 332.	499.	999•
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NATURAL SINES AND COSINES

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FOUR PLACES.

Note. For cosines use right-hand column of degrees and lower line of tenths.

Deg.	٠.٥	٠. I	ຶ.2	∵ 3	°.4	°.5	°.6	°.7	°.8	°.9			pola. 'dths
0°	0.0000	0.0017	0.0035	0.0052	0.0070	0.0087	0.0105	0.0122	0,0140	0.0157	89	18	17
I	0175	0192	0209	0227	0244	0262	0279	0297	0314	0332	88	2	2
2	0349	0366	0384	0401	0419	0436	0454	0471	0488	0506	87	4	3
3	0523	0541	0558	0576	0593	0610	0628	0645	0663	0680	86	5	5
4	0698	0715	0732	0750	0767	0785	0802	0819	0837	0854	85	- 7	7
5	0.0872	0.0889		0.0924	0.0941	0.0958	0.0976	0.0993	0.1011	0.1028	84	9	9
6	1045	1063	1080	1097	1115	1132	1149	1167	1184	1201	83	11	IO
7	1219	1236	1253	1271	1288	1 305	1323	I 340	1357	I 374	82	13	12
8	1392	1409	1426	1444	1461	1478	1495	1513	1530	I 547	81	14	14
9	1564	1582	1599	1616	1633	1650	1668	1685	1702	1719	80°	16	15
10°	0.1736	0.1754	0.1771	0.1788	0.1805	0.1822	0.1840	0.1857	0.1874	0.1891	79	17	16
11	1908	1925	1942	1959	1977	1994	2011	2028	2045	2062	78	2	2
12	2079	2096	2113	2130	2147	2164	2181	2198	2215	2232	77	3	3
13	2250	2267	2284	2300	2317	2334	2351	2368	2385	2402	76	5	5
14	2419	2436	2453	2470	2487	2504	2521	2538	2554	2571	75	7	6
15	0.2588	0.2605	0,2622	0.2639	0.2656	0.2672	0.2689	0.2706	0.2723	0.2740	74	9	8
16	2756	2773	2790	2807	2823	2840	2857	2874	2890	2907	73	IO	10
17	2924	2940	2957	2974	2990	3007	3024	3040	3057	3074	72	12	ΙI
18	3090	3107	3123	3140	3156	3173	3190	3206	3223	3239	71	14	13
19	3256	3272	3289	3305	3322	3338	3355	3371	3387	3404	70°	15	14
20°	0,3420	0.3437	0.3453	0.3460	0.3486	0.3502	0.3518	0.3535	0.3551	0.3567	69	16	15
21	3584	3600	3616	3633	3649	3665	3681		3714	3730	68	2	2
22	3746	3762	3778	3795	3811	3827	3843		3875	3891	67	3	3
23	3907	3923	3939	3955	3971	3987	4003			4051	66	5	5
24	4067	4083	4099	4115	4131	4147	4163		4195	4210	65	6	6
25	0.4226	0.4242	0.4258	0.4274	0.4289	0.4305	0.4321	0.4337	0.4352	0.4368	64	8	8
26	4384	4399	4415	443I	4446	4462	4478		4509	4524	63	10	9
27	4540	4555	4571	4586	4602	4617	4633	4648	4664	4679	62	11	11
28	4695	4710	4726	4741	4756	4772	4787	4802	4818	4833	61	13	12
29	4848	4863	4879	4894	4909	4924	4939	4955	4970	4985	60°	14	14
30°	0.5000	ח גטוג	0.5030	0.5045	0.5060	0.5075	0.5000	0.5105	0.5120	0.5135	59	14	13
31	5150	5165	5180	5195	5210	5225	5240		5270	5284	58	I	1
32	5299	5314	5329	5344	5358	5373	5388	5402		5432	57	3	3
	5446	5461	5476	5490	5505	5519	5534	5548			56	4	4
33 34	5592	5606	5621	5635	5650	5664	5678	5693	5707	5721	55	6	5
	0.5736	-				0.5807	0.5821	0.5835	0.5850	0.5864	54	7	7
35 36	5878	5892	5906	5920	5934	5948	5962	5976	5990	6004	53	8	8
-	6018	6032	6046	6060	6074	6088	6101	6115	6129	6143	52	10	9
37 38	6157	6170	6184	6198	6211	6225	6239	6252	6266	6280	5 r	11	10
30 39	6293	6307	6320	6334	6347	6361	6374	6388	6401	6414	50°	13	12
	1°.0		°.8	°.7	°.6	°.5	°.4	°-3	°.2	°. I	Deg.		rpola. h'dths

NATURAL SINES AND COSINES. 4 PL. NAT. SIN.

Deg.	°.0	°.I	°.2	്-3	°.4	ຶ∙5	°.6	°.7	°.8	,°.9		Inter for h	pola. 'dths
40°	0.6428	0.6441	0.6455	0,6468	0.6481	0.6494	0.6508	0.6521	0.6534	0.6547	49	13	12
41	6561	6574	6587	6600	6613	6626	6639	6652	6665	6678	48	1	1
42	6691	6704	6717	6730	6743	6756	6769	6782	6794	6807	47	3	2
43	6820	6833	6845	6858	6871	6884	6896	6909	6921	6934	46	4	4
44	6947	6959	6972	6984	6997	7009	7022	7034	7 046	7059	~ 45	5	5
45	0.7071		0.7096	0.7108	0.7120	0.7133					44	7	6
46	7193	7206	7218	7230	7242	7254	7266		.7290	7302	43	8	7
47	7314	7325	7337	7349	7361	7373	7385	7396	7408	7420	42	9	8
48	743I	7443	7455	7466 7581	7478	7490 7604	7501 7615	7513 7627	7524 7638	7536 7649	41 40°	10	10
49	7547	7559	7570		7593	•					40		
50°	0.7660					0.7716				* = -	39	11	9
51	7771	7782	7793	7804	7815	7826	7837	7848	7859	7869	38	I	1
52	7880	7891	7902	7912 8018	7923 8028	7934	7944 8049	7955 8059	7965 8070	7976 8080	37	2	2
53	7986 8090	7997 8100	8007 8111	8121	8131	8039 8141	8151	8161	8171	8181	36 35	3 4	3 4
54												6	
55 56	0.8192 (8290	300 8300 8300	0.8211 0 8310	83 2 0	8329	0,824 1 0 8339	8348	8358	8368	8377	34	l	5
56	8387	8396	8406	8415	8425	8434	8443	8453	8462	8471	33	8	5
57 58	8480	8490	8499	8508	8517	8526	8536	8545	8554	8563	31	9	7
59	8572	8581	8590	8599	8607	8616	8625	8634	8643	8652	300	Io	8
1		-	•-	•	•	0.8704				-		8	7
60°	0.8660	8755 8	3.8078 (8763	3,8080 (877 1	8780	8788	8796	8805	8813	0.0730 8821	29 28	ľ	1
62	8746 8829	8838	8846	8854	8862	8870	8878	8886	8894	8902	27	2	1
63	8910	8918	8926	8934	8942	8949	8957	8965	8973	8980	26	2	2
64	8988	8996	9003	9011	9018	9026	9033	9041	9048	9056	25	3	3
65	0.9063			•	-	0.9100			- •		24	4	4
66	9135	9143	9150	9157	9164	9171	9178	9184	9191	9198	23	5	4
67	9205	9212	9219	9225	9232	9239	9245	9252	9259	9265	22	6	5
68	9272	9278	9285	9291	9298	9304	.9311	9317	9323	9330	21	6	6
69	9336	9342	9348	9354	9361	9367	9373	9379	9385	9391	20°	7	6
70°	0.9397	0.0403	0.9409	0.9415	0.9421	0.9426	0.0432	0.0438	0.0444	0.0440	19	6	4
71	9455	9461	9466	9472	9478	9483	9489	9494	9500	9505	18	1	0
72	9511	9516	9521	9527	9532	9537	9542	9548	9553	9558	17	I	1
73	9563	9568	9573	9578	9583	9588	9593	9598	9603	9608	16	2	I
74	9613	9617	9622	9627	9632	9636	964 1	9646	9650	9655	15	2	2
75	0.9659	0.9664	o.9668 d	0.9673	0.9677	0.9681			0.9694	0.9699	14	3	2
76	9703	9707	9711	9715	9720	9724	9728	9732	9736	9740	13	4	2
77	9744	9748	9751	9755	9759	9763	9767	9770	9774	9778	12	4	3
78	9781	9785	9789	9792	9796	9799	9803	9806	9810	9813	11	5	3
7 9	9816	9820	9823	9826	9829	9833	9836	9839	9842	9845	10°	5	4
80°	0.9848	0.9851	0.9854			0.9863				0.9874	9	3	2
8r	9877	9880	9882	9885	9888	9890	9893	9895	9898	9900	8	0	0
82	9903	9905	9907	9910	9912	9914	9917	9919	9921	9923	7	1	0
83	9925	9928	9930	9932	9934	9936	9938	9940	9942	9943	6	I	r
84	9945	9947	9949	9951	9952	9954	9956	9957	9959	9960	5	1	I
85	0.9962					0.9969					4	2	1
86	9976	9977	9978	9979	9980	9981	9982	9983	9984	9985	3	2	I
87	9986	9987	9988	9989	9990	9990	9991	9992	9993	9993	2	2 2	1 2
88 89	9994 9998	9995 9999	9995 9999	9996 9999	9996 9999	999 7 1.000	9997 1.000	9997 1.000	9998 1.000	9998	0°	3	2
	7990	7777	7777	7777	7777	1.000				1.500		_ '	
	1°.0	و.٥	°.8	°.7	°.6	°.5	°.4	°-3	°.2	°. I	Deg.		rpola. h'dths

NATURAL TANGENTS AND COTANGENTS

TO FOUR PLACES.

Note. For cotangents use right-hand column of degrees and lower line of tenths

Deg.	°.0	°.1	٠ .2	°·3	°.4	°∙5	°.6	°.7	°.8	°.9			erpola h'dth
0°	0,0000	0.0017	0.0035	0.0052	0.0070	0.0087	0.0105	0.0122	0.0140	0.0157	89	17	18
1	0175	0192	0209	0227	0244	0262			0314		88	2	
2	0349	0367	0384	0402	0419	0437			٠.		87	3	
3	0524	0542	0559	0577	0594	0612	0629		0664	<i>.</i>	86	5	
4	0699	0717	0734	0752	0769	0787	0805		0840	0857	85	7	_
5	0.0875	0.0892	0.0910	0.0928	0.0945	0.0963	0.0981	0.0998	0.1016		84	9	•
6	1051	1069	1086	1104	1122	1139	1157		1192		83	10	-
7	1228	1246	1263	1281	1299	1317	1334		1370	1388	82	12	
8	1405	1423	1441	1459	1477	1495			1548	1566	81	14	-
9	1584	1602	1620	1638	1655	1673	1691	1709	1727		80°	15	
10°	0.1763	0.1781	0.1790	0.1817	0.1835	0.1853	0.1871	0.1800	o too8	0.1026	1	19	20
11	1944		1980	1998	2016	2035	2053		2089	2107	79 78	2	
12	2126	-	2162	2180	2199	2217	2235	2254	2272	2290			
13	2309		2345	2364	2382	2401	2419	• •	2456	2475	77 76	4 6	4 6
14	2493	2512	2530	2549	2568	2586	2605		2642	2661	75	8	8
15	0.2670	0.2698				0.2773	-				1	-	- 1
16	2867	2886	2905	2924	2943	2962	2981	3000	•	'-	74	to	10
17	3057	3076	3096	3135	3134	3153	3172	3191	3019 3211	ე038	73	11	12
18	3249	3269	3288	3307	3327	3°53 3346	3365	3385	3404	3230	72	13	14
19	3443	3463	3482	3502	3522	3541	3561	3581	3600	3424 3620	71 70°	15	16 18
			•			_			-	•		1	
20°	0.3640					0.3739					69	22	24
22	3839	3859 4061	3879 4081	3899	3919	3939	3959	3979	4000	4020	68	2	2
23	4245	4265	4286	4101	4122	4142	4163	4183	4204	4224	67	4	5
23 24	4452	4473	4494	4307	4327 4536	4348	4369 4578	4390	4411 4621	4431	66	7	7
				4515		4557		4599		4642	65	9	10
25	0.4663					0.4770					64	II	12
26	4877	4899	4921	4942	4964	4986	5008	5029	5051	5073	63	13	14
27 28	5095	5117	5139	5161	5184	5206	5228	5250	5272	5295	62	15	17
29	5317	5340 5566	5362 5589	5384 5612	5407	5430	5452 5681	5475	5498	5520	60°	20	19 22
	5543	••		-	5635	5658	•	5704	57 2 7	5750	00	20	22
30 °	0.5774					0.5890					59	26	28
31	6009	6032	6056	6080	6104	6128	6152	6176	6200	6224	58	3	3
32	6249	6273	6297	6322	6346	6371	6395	6420	6445	6469	57	6	6
33	6494	6519	6544	6569	6594	6619	6644	6669	6694	6720	56	8	8
34	6745	6771	6796	6822	6847	6873	6899	6924	6950	6976	55	10	11
35	0.7002	0.7028	.7054 c	.7080 c	.7107	0.7133	0.7159	0.7186		0.7239	54	13	14
36	7265	7292	7319	7346	7373	7400	7427	7454	7481	7508	53	16	17
37	7536	7563	7590	7618	7646	7673	7701	7729	7757	7785	52	18	20
38	7813	7841	7869	7898	7926	7954	7983	8012	8040	8069	51	21	22
39	8098	8127	8156	8185	8214	8243	8273	8302	8332	8361	50 °	23	25
	ı°.o	°.9	°.8	°.7	°.6	~ 5	°.4	°.3	ి.2	°.1	Deg.	Inter for h	

NATURAL TANCENTS AND COTANGENTS. 4 PL. NAT. TAN.

Deg.	°.o	~. I	°.2	°·3	°.4	°-5	°.6	°.7	°.8	°.9		Interpola. for h'dths
40°	0.8391	0.8421	0.8451	0.8481	0.8511	0.8541	0.8571	0.8601	0.8632	0.8662	49	30 40
41	8693					8847					48	3 4
42	9004					9163	, , ,	-	-		47	6 8
43	9325					9490					46	9 12
44	9657					9827	-	9896	,,,		45	1
45 46	0355		1.0070			0538		0612	0649		44	15 20 18 24
47	0724				-	0913		0990			43	21 28
48	1106	•	, , , ,			1303					41	24 32
49	1504	1544	. 1585	1626	1667	1708	1750	1792	1833	1875	40°	27 36
50°	1.1918	1.1960	1,2002	1.2045	1.2088	1.2131	1.2174	1,2218	1,2261	1.2305	39	50 60
51	2349			_		2572			_		38	5 6
52	2799	2846				3032	3079			_	37	10 12
53	3270					3514					36	15 18
54	3764			3916		4019		4124		-	35	20 24
55			1.4388					1,4659	1.4715		34	25 30
56	4826 5399					5108 5697				5340 5941	33 32	30 36 35 42
57 58	6003				6255	6319		6447	-		31	40 48
59	6643				6909	6977		7113		7251	30°	45 54
60°			1.7461			1 2625		T 7820	1.7893	1 7066	29	70 80
61		8115		8265		8418			8650	8728	28	7 8
62	8807				٠.	9210				9542	27	14 16
63	1.9626	1.9711	1.9797			2.0057				2.0413	26	21 24
64	2.0503	2.0594	. 2 . 0686	2.0778	2.0872	2.0965	2.1060	2.1155	2.1251	2.1 348	25	28 32
65	2.1445		2.1642					2.2148	2.2251	2.2355	24	35 40
66	2460				2889	2998		3220			23	42 48
67	3559		-, -			4142				4627	22	49 56
68 69	4751 6051		-		5257 6605	5386 6746	5517 6889	5649 7034		5916 7326	21 20°	56 64 63 72
	ĺ	•			-		-					- ,
70°			2.7776			2.8239					19	90
7I 72			2.9375 3.1146			2.9887	-		3.2305		18	9 18
73	2709				3544	3759	-	-			17 16	27
74	4874		-		5816	6059	6305	6554		7062	15	36
75	3.7321	3.7583	3.7848		3.8391				3.9520	3.9812	14	45
76			4.0713			4.1653					13	54
77			4.4015			4.5107				-	12	63
78			4.7867						5.0504		11	72
79	5.1446	5.1929	5.2422	5.2924	5.3435	5.3955	5.4486	5.5026	5·5578	5.0140	10°	81
80°			5.7894			5.9758					9	
81			6.4596							7.0264	8	
82			7.3002						7.9158		7	
83 84			8.3863 9.845			8.7769			10.99		6	
85			11.91				-		13.62		3	
86	14.30	14.67	15.06	15.46	15.80				17.89		3	
87	19.08	19.74	20.45	21.20	22.02				26.03		2	
88	28.64	30.14	31.82	33.69	35.80	38.19	40.92	44.07	47.74	52.08	1	
89			71.62			114.6	143.2	191.0	286.5	573.0	0 °	
	ı°.o	٠.9	°.8	°.7	°.6	°∙5	°.4	്.3	°.2	°.1	Deg.	Interpola. for h'dths

LOCARITHMS OF SINES AND COSINES

TO

FOUR PLACES.

Note. For log. cos. use right-hand column of degrees and lower line of tenths.

Deg.	°.0	٠.٦	٠.2	°.3	°.4	°.5	°.6	°.7	°.8	°.9			rpola. h'dths
0°		3 .2419	3.5429	3.7190	3 .8439	3.9408	2.0200	2.0870	2,1450	2.1061	89	35	25
I	2.2419	2.2832	2.3210	2.3558	2.388o	2.4179					88	4	3
2			2.5842			2.6397	2.6567	2.6731	2.6889	2.7041	87	7	5
3	2.7188	2 .7330	2.7468	2.7602	2.7731	$\frac{2.7857}{2}$	2.7979	2.8098	2.8213	2.8326	86	ıί	8
4	2.8436	2.8543	2.8647	2.8749	2 .8849	2.8946	2.9042	2.9135	2.9226	2.9315	85	14	10
5	2.9403	2.9489	2.9573	2.9655	2.9736	2.9816	2.9894	2.9970	ī.0046	Ī.0120	84	18	13
6	1.0192	1.0264	ī.0334	1.0403	Ī.0472	T.0539	T.0605	1.0670	ī.0734	I.0707	83	21	15
7	1.0859	ī.0920	ī.0981	1.1040	1.1099	ī.1157	ī.1214	1.1271	1.1326	1.1381	82	25	18
8	ī.1436	ī.1489	Ī.1542	1.1594	1.1646	1.1697	Ī.1747	1.1797	T.1847	7.1895	81	28	20
9	1.1943	ī.1991	ī.2038	ī.2085	1.2131	1.2176	ī,222 I	1.2266	ī.2310	ī.2353	80°	32	23
10°	T.2307	T.2430	ī.2482	T.2524	7 2565	ī.2606						21	
11	2806	2845	2883	2921	2959	2997	3034				79		18
12	3179	3214		3284	3319	3353	3387	3421	3455	3143 3488	78	2	2
13	3521	3554		3618	3650	3682	3713		3775	3806	77	4 6	4
14	3837	3867		3927	3957	3986	4015	4044	3773 4073	4102	75	8	5
15		٠,	ī.4186							•	1		7
16	4403	4430		4482	4508	Ĩ.4269		4584			74	11	9
17	4659	4684		4733		4533 4781	4559 4805	45°4 4829	4609	4634	73	13	II
18	4900	4923		4969	4757 4992	5015	5037	5060	4853 5082	4876	72	15	13
19	5126	5148		5192	5213	5235	5256	5278	5299	5104 5320	71 70°	17	14 16
1	1		٠.	•				٠.	•		70"	_	
20°			T.5382			ī.5443					69	15	13
21	5543	5563		5602	5621	5641	5660	5679	5698	5717	68	2	I
22	5736	5754		5792	5810	5828	5847	5865	5883	5901	67	3	3
23	5919	5937		5972	5990	6007	6024	•	6059	6076	66	5	4
24	6093	6110	•	6144	6161	6177	6194	6210	6227	6243	65	6	5
25			1.6292			ī.6340					64	8	7
26	6418	6434		6465	6480	6495	6510	6526	6541	6556	63	9	8
27	6570	6585	6600	6615	6629	6644	6659	6673	6687	6702	62	11	9
28	6716	6730		6759	6773	6787	6801	6814	6828	6842	61	12	10
2 9	6856	6869	6883	6896	6910	6923	6937	6950	6963	6977	60°	14	12
30°	ī.6990	1.7003	ī.7016	1.7029	1.7042	1.7055	7.7068	ī.7080	7.7093	7.7106	59	11	9
31	7118	7131	7144	7156	7168	7181	7193	7205	7218	7230	58	I	1
32	7242	7254	7266	7278	7290	7302	7314	7326	7338	7349	57	2	2
33	7361	7373	7384	7396	7407	7419	7430	7442	7453	7464	56	3	3
34	7476	7487	7498	7509	7520	7531	7542	7553	7564	7575	55	4	4
35	7.7586	Ī.7597	ī.7607	7.7618	ī.7629	ī.7640	ī.7650	ī.7661	ī.7671	ī.7682	54	6	5
36	7692	7703	7713	7723	7734	7744	7754	7764	7774	7785	53	7	
37	7795	7805	7815	7825	7835	7844	7854	7864	7874	7884	52	8	5 6
38	7893	7903	7913	7922	7932	7941	7951	7960	7970	7979	51	9	7
39	7989	7998	8007	8017	8026	8035	8044	8053	8063	8072	50°	10	8
	I°.0	°.9	°.8	°.7	°.6	°-5	°.4	°.3	°.2	°.1	Deg.		rpola.
	1.0	.9	.0	٠,		.3	. **	٠.5		••	Dog.	for t	ı'dthe

LOGARITHMS OF SINES AND COSINES.

4 PL. LOG. SIN.

Deg.	°.o	°.1	°.2	°·3	°.4	~.5	°.6	°.7	°.8	°.9		interpola. tables.
40°	ī.8081	ī.8090	T.8000	ī.8108	ī.8117	T.8125	T.8134	ī.8143	T.8152	7.8161	49	987
41	8169		8187	8195	8204	8213	8221		8238	8247	48	111
42	8255	8264	8272	8280	8289	8297	8305		8322	8330	47	2 2 I
43	8338	8346	8354	8362	8370	8378	8386	8394	8402	8410	46	3 2 2
44	8418	8426	8433	8441	8449	8457	8464	8472	8480	8487	45	4 3 3
45	1.8495	ī.8502	ī.8510	ī.8517		1.8532	ī.8540	1.8547		ī.8562	44	5 4 4
46	8569	8577	8584	8591	8598	8606	8613		8627	8634	43	5 5 4
47	8641	8648	8655	8662	8669	8676	8683		8697	8704	42	665
48	8711	8718	8724	8731	8738	8745 8810	8751 8817	8758 8823	8765	8771 8836	41 40°	7 6 6 8 7 6
49	8778	•	8791	8797	8804		•	-	8830	•	40	
50 °		7.8849						ī.8887		_	39	654
51	8905	8911	8917	8923	8929	8935	8941	8947	8953	8959	38	IIO
52	8965	8971	8977	8983	8989	8995	9000	-	9012	9018	37	2 2 I
53	9023		9035	904 1 9096	9046 9101	9052	9057 9112	9063 9118	9069 9123	9074 9128	36 35	.2 2 2
54	9080	-	9091			9107						3 3 2
55 56	1.9134 9186	1.9139 9191	9144	9201	9206	9211	9216	9221	9226	9231	34 33	4 3 2
57	9236		9246	9251	9255	9260	9265	9270	9275	9231	33	4 4 3
58	9230	9289	9294	9298	9303	9308	9312	9317	9322	9326	31	5 4 3
59	9331	9335	9340	9344	9349	9353	9358		9367	9371	3ั0∘	5 5 4
60°					_			_				432
61	9418	1.9380 9422	9427				9443	1.9406			29 28	000
62	9418	9463	9427	9431 9471	9435 9475	9439 9479	9443	9447 9487	9451 9491	9455 9495	27	110
63	9439	9503	9506	9510	9514	9518	9522	9525	9529	9533	26	111
64	9537	9540	9544	9548	9551	9555	9558		9566	9569	25	2 I I
65		ī.9576	-	-				1.9597			24	2 2 I
66	9607	9611	9614	9617	9621	9624	9627	9631	9634	9637	23	2 2 I
67	9640	-	9647	9650	9653	9656	9659	9662	9666	9669	22	3 2 I
68	9672	9675	9678	968r	9684	9687	9690	9693	9696	9699	21	3 2 2
69	9702	9704	9707	9710	9713	9716	9719	9722	9724	9727	20°	4 3 2
70°	1.9730	ī.9733	0735	ī.0738	ī.074I	Ī.0743	ī.0746	ī.9749	1.0751	T.0754	19	3 2 1
71	9757	9759	9762	9764	9767	9770	9772	9775	9777	9780	18	000
72	9782	9785	9787	9789	9792	9794	9797	9799	9801	9804	17	100
7 3	9806	9808	9811	9813	9815	9817	9820	9822	9824	9826	16	110
74	9828	9831	9833	9835	9837	9839	9841	9843	9845	9847	15	110
75	ī.9849	ī.9851	ī.9853	ī.9855	ī.9857	ī.9859	ī.9861	ī.9863	7.9865		14	2 1 1
76	9869	-	9873	9875	9876	9878	9880	9882	9884	9885	13	2 1 1
77	9887	9889	9891	9892	9894	9896	9897	9899	9901	9902	12	2 I I
78	9904	9906	9907	9909	9910	9912	9913	9915	9916	9918	11	2 2 I
79	9919	9921	9922	9924	9925	9927	9928	9929	9931	9932	10°	321
80°	1.9934	1.9935	ī.9936	ī.9937	ī.9939	1.9940	ī.994 1	ī.9943	1.9944	1.9945	9	2 1
81	9946	9947	9949	9950	9951	9952	9953	9954	9955	9956	8	00
82	9958	9959	9960	996 1	9962	9963	9964	9965	9966	9967	7	00
83	9968	9968	9969	9970	9971	9972	9973	9974	9975	9975	6	10
84	9976	9977	9978	9978	9979	9980	9981	9981	9982	9983	5	10
85		ī.9984						ī.9988			4	II
86	9989	9990	9990	9991	999 1	9992	9992	9993	9993	9994	3	II
8 ₇ 88	9994	9994	9995 9998	9995 9998	9996	9996	9996		9997	9997	2	II
88 ' 89	9997 9999	9998 9999	9998 zero	9998 zero	9998 zero	9999 zero	9999 zero	9999 zero	9999 zero	9999 zero	. 0°	2 I 2 I
	7779	7777	2010	2010	2010	2010		_			<u>_</u> _	
	1°.0	°.9	°.8.	°.7	°.6	°∙5	°.4	்.3	ຶ.2	٥.٦	Deg.	Interpola. for h'dths
		_								4 D		

LOCARITHMS OF TANCENTS AND COTANGENTS

TO FOUR PLACES.

Note. For log. cot. use right-hand column of degrees and lower line of tenth

Deg.	°.0	°.1	ိ.2	°.3	°.4	°∙5	°.6	°.7	°.8	°.9			erpola h'dth
0°				3.7190		3.9409	2.0200	2.0870	2.1450	2.1962	89	35	27
I				2.3559		2.4181	2.4461	2.4725	$\overline{2.4973}$	2.5208	88	4	-
2				2.6038		2.6401	2.6571	2.6736	2,6894	2.7046	87	7	•
3				2.7609		2.7865	2.7988	2.8107	2.8223	2.8336	86	ΙÍ	_
4	· 2 .8446	2.8554	2.8659	2.8762	2.8862	2.8960	2.9056	2.9150	2.9241	2.9331	85	14	II
5				2.9674		2.9836	2.9915	2.9992	ī.0068	ī.0143	84	18	14
6				1.0430		ī.0567	ī.0633	ī.0699	1.0764	1.0828	83	21	16
7	1.0891	1.0954	1.1015	1.1076	1.1135	1.1194	Ī.1252	ī.1310	ī.1367	1.1423	82	25	19
- 8				<u>1</u> .1640		1.1745	Ī.1797	1.1848	<u>1.1898</u>	1.1948	81	28	22
9	1.1997	1.2046	1.2094	1.2142	1.2189	1.2236	ī.2282	1.2328	1.2374	1.2419	80°	32	24
10°	ī.2463	1.2507	1.2551	1.2594	ī.2637	ī.2680	ī.2722	ī.2764	ī.2805	ī.2846	79	25	23
11	2887	2927	2967	3006	3046	3085			3200	3237	78	3	2
12	3275	3312	3349	3385	3422	3458	3493	3529	3564		77	5	5
13	3634	3668	3702		3770	3804	3 ⁸ 37	3870	3903	3935	76	8	7
14	3968	4000			4095	4127	4158	4189	4220	4250	75	10	9
15	1.4281	ī.4311	ī.4341	ī.4371	ī.4400	ī.4430	ī.4459	ī.4488	1.4517	ī.4546	74	13	Ι2
16	4575	4603	4632	4660	4688	4716	4744	477I	4799	4826	73	15	14
17	4853	4880	4907	4934	4961	4987	5014	5040	5066	5092	72	18	16
18	5118	5143	5169	5195	5220	5245	5270	5295	5320	5345	71	20	18
19	5370	5394	5419	5443	54 ⁶ 7	5491	5516	5539	5563	5587	70°	23	21
20°	ī.5611	ī.5634	ī.5658	ī.5681	T.5704	Ī.5727	ī.5750	Ī.5773	ī.5796	ī.5810	69	21	19
21	5842	5864	5887	5909	5932	5954	5976	5998	6020	6042	68	2	2
22	6064	6086	6108	6129	6151	6172	6194	6215	6236	6257	67	4	4
23	6279	6300	6321	6341	6362	6383	6404	6424	6445	6465	66	6	6
24	6486	6506	6527	6547	6567	6587	6607	6627	6647	6667	65	8	8
25	7.6687	ī.6706	ī.6726	ī.6746	1.6765	ī.6785	ī.6804	ī.6824	ī.6843	ī.6863	64	11	10
26	6882	6901	6920	6939	6958	6977	6996	7015	7034	7053	63	13	11
27	7072	7090	7109	7128	7146	7165	7183	7202	7220	7238	62	15	13
28	7257	7275	7293	7311	7330	7348	7366	7384	7402	7420	61	17	15
29	7438	7455	7473	749 I	7509	7526	7544	7562	7579	7597	60°	19	17
30°	ī.7614	T.7632	T.7640	1.7667	ī.7684	ī.770I	T.7710	T.7736	T.7753	_ [.777]	59	17	15
31	7788	7805	7822	7839	7856	7873	7890	7907	7924	7941	58	2	2
32	7958	7975	7992	8008	8025	8042	8059	8075	8092	8109	57	3	3
33	8125	8142	8158	8175	8191	8208	8224	8241	8257	8274	56	5	5
34	8290	8306	8323	8339	8355	8371	8388	8404	8420	8436	55	7	6
35	1.8452	ī.8468	1.8484	1.8501	ī.8517	ī.8533	ī.8540	1.8565	ī.8 5 81	1.8597	54	9	8
36	8613	8629	8644	866o	8676	8692	8708	8724	8740	8755	53	IO	9
37	8771	8787	8803	8818	8834	8850	8865	8881	8897	8912	52	12	11
38	8928	8944	8959	8975	8990	9006	9022	9037	9053	9068	51	14	12
39	9084	9099	9115	9130	9146	9161	9176	9192	9207	9223	50°	15	14
	ı°.o	°.9	°.8	°-7	°.6	".5	°.4	∵ 3	ိ.2	°. I	Deg.		rpola.

LOCARITHMS OF TANGENTS AND COTANGENTS. 4 PL. LOG. TAN.

Deg.	°.0	°.1	°.2	3.3	°.4	°.5	°.6	°.7	°.8	°.9		Interpola. for h'dths
40°	ī.9238	ī.9254	ī.9269	ī.9284	ī.9300	1.9315	ī.9330	ī.9346	ī.9361	ī.9376	49	15 16
4I			Ī.9422					1.9499			48	2 2
42			<u>1</u> .9575					1.9651			47	3 3
43			Ī.9727					ī.9803			46	5 5 6
44			1.9879					1.9955			45	
45	L		0.0030				_	0.0106		= = =	44	9 10
46 47	0152			0197 0349	0212 0364	0228 0379	0243 0395		0273 0425	0288 0440	43 42	9 10
47 48	0303	-			0517	0532					41	12 13
49 •	0608		- 1			0685			٠.	0746	40 °	14 14
50°	0.0762	0.0777	0.0793	0.0808	0.0824	0.0839	0.0854	0.0870	0.0885	0.0901	39	17 18
51	0916			0963		0994		-	1041	1056	38	2 2
52	1072	1088	1103	1119	1135	1150	1166	1182	1197	1213	37	3 4
53	1229		1260	1276	-	1 308				1371	36	5 5
54	1387			1435	1451	1467	1483		1516	1532	35	7 7
55	1 .		0.1580	• •		-		0.1661			34	9 9
56	1710	•		1759	1776	1792		-	1842	1858	33	to II
57	1875	-		1925	1941	1958			2008	2025	32	12 13
58 59	2042	• .	-	2093 2264	_	2127 2299	- :		2178 2351	2195 2368	31 30°	14 14 15 16
]						-			•	1	
60°			0.2421					0.2509			29 28	21 23
62	2562 2743			2616 2798		2652 2835		-	2707 2891	2725 2910	27	2 2
63	2928			2985	3004	3023			3080	3099	26	4 5 6 7
64	3118		-	3176		3215	3235	3254	3274	3294	25	8 9
65			0.3353					0.3453			24	11 12
66	3514		3555	3576		3617	3638		3679	3700	23	13 14
67	3721	3743		3785	3806	3828	3849	3871	3892	3914	22	15 16
68	3936	3958	3980	4002	4024	4046	4068	4091	4113	4136	21	17 18
69	4158	4181	4204	4227	4250	4273	4296	4319	4342	4366	20°	19 21
70°	0.4389	0.4413	0.4437	0.4461	0.4484	0.4509	0.4533	0.4557	0.4581	0.4606	19	25 27
71	4630	4655	4680	4705	4730	4755			4831	4857	18	3 3
72	4882	4908	4934	4960	4986	5013	5039	5066	5093	5120	17	5 5 8 8
73	5147	5174	5201	5229	5256	5284	5312		5368	5397	16	
74	5425	5454	5483	5512	5541	5570	-		5659	5689	15	10 11
75			0.5780					0.5936			14	13 14
76	6032	6065	6097	6130	6163	6196	6230	6264	6298	6332	43	15 16
7 7 78	6366 6725	6401 6763	6436 6800	6471 6838	6507 6877	6542 6915	6578	6615 6994	6651	6688	12 11	18 19
79	7113	7154	7195	7236	7278	7320	6954 7363	7406	7 0 33 7449	7073 7493	10°	20 22 23 24
80°	• -							•			i .	
81			0.7626			0.7764		0.7858			9	35 45
82			0.8633					0.8924			7	4 5 7 9
83			0.9236				-	0.9570			6	11 14
84	0.9784	0.9857	0.9932	8000.1	1.0085			1.0326			5	14 18
85			1.0759					1.1238			4	18 23
86			1.1777					1.2391			3	21 27
87			1.3106					1.3962			2	25 32
88			1.5027					1.6441			1	28 36
89	1.7581	1.8038	1.8550	1.9130	1.9800	2.0591	2.1561	2.2810	2.4571	2.7581	0 °	32 41
	I°.0	۰٬9	°.8	°-7	°.6	°∙5	°.4	°∙3	ి.2	°.I	Deg.	Interpola. for h'dths
				-		(G CC

LOCARITHMS OF TRICONOMETRIC FUNCTIONS

то

FIVE PLACES.

Note. The table gives the log of the natural value of the function, and hence the characteristic is negative when that value is fractional. The common practice of adding 10. to avoid the negative characteristic is not recommended.

0°	log cos		0°	log oos	
0'-16' -17'-28' 29'-36' 37'-43'	0,00 000 1.99 999 1.99 998 1.99 997	44'-60' 32'-43' 24'-31' 17'-23'	44'-49' 50'-54' 55'-59' 60'	ī.99 996 ī.99 995 ī.99 994 ī.99 993	11'-16' 6'-10' 1'-5' 0'
	log sin	89°		log sin	89°

0°

,	log sin	log tan	log cot		,	log sin	log tan	log oot	
0' 1 2 3 4	—————————————————————————————————————	—————————————————————————————————————	3.53 627 3.23 524 3.05 915 2.93 421	60 ′ 59 58 57 56	30' 31 32 33 34	3.94 084 95 508 96 887 98 223 3.99 520	3.94 086 95 510 96 889 - 98 225 3.99 522	2.05 914 04 490 03 111 01 775 2.00 478	30' 29 28 27 26
5 6 7 8 9	3.16 270 24 188 30 882 36 682 41 797	3.16 270 24 188 30 822 36 682 41 797	2.83 730 75 812 69 118 63 318 58 203	55 54 53 52 51	35 36 37 38 39	2.00 779 02 002 03 192 04 350 05 478	2.00 781 02 004 03 194 04 353 05 481	1.99 219 97 996 96 806 95 647 94 519	25 24 23 22 21
10 11 12 13 14	3.46 373 50 512 54 291 57 767 60 985	3.46 373 50 512 54 291 57 767 60 986	2.53 627 49 488 45 709 42 233 39 014	50 49 48 47 46	40 41 42 43 44	2.06 578 07 650 08 696 09 718 10 717	2.06 581 07 653 08 700 09 722 10 720	92 347 91 300 90 278 89 280	20 19 18 17 16
15 16 17 18 19	3.63 982 66 784 69 417 71 900 74 248	3.63 982 66 785 69 418 71 900 74 248	2.36 018 33 215 30 582 28 100 25 752	45 44 43 42 41	45 46 47 48 49	2,11 693 12 647 13 581 14 495 15 391	2.11 696 12 651 13 585 14 500 15 395	1.88 304 87 349 86 415 85 500 84 605	15 14 13 12
20 21 22 23 24	3.76 475 78 594 80 615 82 545 84 393	3.76 476 78 595 80 615 82 546 84 394	2.23 524 21 405 19 385 17 454 15 606	40 39 38 37 36	50 51 52 53 54	2.16 268 17 128 17 971 18 798 19 610	2.16 273 17 133 17 976 18 804 19 616	1.83 727 82 867 82 024 81 196 80 384	10 9 8 7 6
25 26 27 28 29	3.86 166 87 870 89 509 91 088 92 612	3.86 167 87 871 89 510 91 089 92 613	2.13 833 12 129 10 490 08 911 07 387	35 34 33 32 31	55 56 57 58 59	2.20 407 21 189 21 958 22 713 23 456	2.20 413 21 195 21 964 22 720 23 462	1.79 587 78 805 78 036 77 280 76 538	5 4 3 2 1
30′	3.94 084 log cos	3.94 086 log oot	2.05 914 log tan	30′	60′	2.24 186 log oos	2.24 192 log cot	1.75 808 log tan	<u>0'</u>

89°

(47)

89° LOG SIN, etc.

89°

2 25 609 25 616 74 384 99 993 73 688 99 993 55 354 55 382 44 618 99 995 57 05 5705 55 734 44 266 99 73 004 99 992 75 05 05 05 05 05 05 05 05 05 05 05 05 05	
1	
2	
3	973 59 973 58
10 2.30 879 2.30 888 7.69 112 7.99 992 7.084 7.714 42.866 99	
5 \$\bar{2}.27 \text{ 66}\$ \bar{1}.22 \text{ 36}\$ \text{ 69}\$ \bar{1}.72 \text{ 331}\$ \bar{1}.99 \text{ 992}\$ \bar{2}\$ \bar{2} \bar{2} \text{ 56}\$ \text{ 60}\$ \bar{2}\$ \bar{2}	
6 28 324 28 332 71 668 99 992 56 400 56 429 43 571 99 7 28 977 28 986 71 014 99 992 56 743 56 773 43 227 99 9 30 255 30 263 69 737 99 991 57 784 57 114 42 886 99 10 2 30 879 2 30 888 7.69 112 7.99 991 2.57 757 2.57 788 7.42 212 7.99 11 31 495 31 505 68 495 99 990 58 419 59 99 58 419 59 99 58 419 58 419 59 99 58 419 59 915 59 975 59 10	. , .
7 28 977 28 986 71 014 99 992 56 743 56 773 43 227 99 9 30 255 30 263 69 737 99 991 57 784 57 114 42 886 99 10 2 30 879 2 30 888 1.69 112 1.99 991 57 421 57 757 2.57 788 1.42 212 1.99 11 31 495 31 505 68 495 99 990 13 32 702 32 711 67 888 99 990 58 449 58 451 41 879 99 13 32 702 32 711 67 888 99 990 58 449 58 451 41 879 99 14 33 292 33 302 66 698 99 990 58 747 58 79 40 895 99 16 34 450 34 461 65 539 99 989 59 715 59 749 40 251 99 17 35 018 35 578 35 590 64 410 99 989 60 632 63 349 60 384 39 616 99 20	97 ¹ 55
10	970 53
10	970 52
11	969 51
12	
13	968 49
14	_
15 2.33 875 2.33 886 1.66 114 1.99 990 7.59 395 2.59 428 1.40 572 1.99 199 1.99 17 35 518 35 5209 64 971 99 989 60 33 60 683 39 932 99 989 60 603 60 608 39 932 99 989 60 603 60 608 39 932 99 989 60 602 60 608 39 932 99 989 60 602 60 608 39 9302 99 99 99 99 60 602 60 608 39 9302 99 99 99 60 602 60 608 39 9302 99 99 99 60 602 60 608 39 9302 99 99 60 602 60 608 39 9302 99 99 99 60 602 60 608 39 9302 99 99 99 60 602 60 608 39 9302 99 99 99 60 602 60 602 60 608 39 9302 99 99 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 60 602 </td <td></td>	
16	
17	' .'. '/
20	966 43
20	965 42
21	964 41
22	
23	963 39
24	
25	
26	
27	
29	_ 1 0 1
30	60 32
31	
32 42 746 42 762 57 238 99 984 64 543 64 585 35 415 99 984 33 43 216 43 232 56 768 99 984 64 827 64 870 35 130 99 98 35 2.44 139 2.44 156 1.55 844 1.99 983 2.65 391 2.65 391 2.65 313 34 285 99 983 37 45 044 45 061 54 939 99 983 65 670 65 715 34 285 99 38 45 489 45 507 54 493 99 982 65 947 65 993 34 007 99 39 45 930 45 948 54 052 99 982 66 497 65 543 33 731 99 40 2.46 366 2.46 385 1.53 615 7.99 982 2.66 769 2.66 816 1.33 184 7.99 41 46 799 46 817 53 183 99 981 67 039 67 087 32 913 99 42 47 226 47 245 52 755 99 981 67 308 67 356 32 644 99 43 47 650 47 669 52 331 <td></td>	
33 43 216 43 232 56 768 99 984 64 827 64 870 35 130 99 984 34 43 680 43 696 56 304 99 984 65 110 65 154 34 846 99 98 35 2.44 139 2.44 156 7.55 844 7.99 983 7.65 391 7.65 435 7.34 565 7.99 7.98 36 44 594 44 611 55 389 99 983 65 670 65 715 34 285 99 983 37 45 044 45 661 54 939 99 983 65 947 65 993 34 007 99 983 39 45 930 45 948 54 052 99 982 66 223 66 269 33 731 99 99 40 2.46 366 2.46 385 7.53 615 7.99 982 7.66 769 7.66 816 7.33 184 7.99 99 41 46 799 46 817 53 183 99 981 67 039 67 087 32 913 99 99 42 47 226 47 245 52 755 99 981 67 308 67 356 32 644 99 99 43 47 650 47 669 52 331 </td <td></td>	
34 43 680 43 696 56 304 99 984 65 110 65 154 34 846 99 983 35 2.44 139 2.44 156 1.55 844 1.99 983 2.65 391 2.65 435 1.34 565 1.99 983 36 44 594 44 611 55 389 99 983 65 670 65 715 34 285 99 98 37 45 044 45 061 54 939 99 982 65 947 65 993 34 007 99 98 38 45 489 45 507 54 493 99 982 66 223 66 269 33 731 99 99 39 45 930 45 948 54 052 99 982 66 497 66 543 33 457 99 99 40 2.46 366 2.46 385 1.53 615 1.99 982 2.66 769 2.66 816 1.33 184 1.99 98 41 46 799 46 817 53 183 99 981 67 039 67 087 32 913 99 98 42 47 226 47 245 52 755 99 981 67 308 67 356 32 644 99 98 43 47 650 47 669 52 331	- 1
35	
36	- 1
37 45 044 45 061 54 939 99 983 65 947 65 993 34 007 99 983 38 45 489 45 507 54 493 99 982 66 223 66 269 33 731 99 982 39 45 930 45 948 54 948 54 952 99 982 66 497 66 543 33 457 99 982 40 2.46 366 2.46 385 1.53 615 1.99 982 2.66 769 2.66 816 1.33 184 1.99 981 41 46 799 46 817 53 183 99 981 67 039 67 087 32 913 99 981 42 47 226 47 245 52 755 99 981 67 308 67 356 32 644 99 981 43 47 650 47 669 52 331 99 981 67 575 67 624 32 376 99 981	
39 45 930 45 948 54 052 99 982 66 497 66 543 33 457 99 99 40 \$\bar{2}\$.46 366 \$\bar{2}\$.46 385 \$\bar{1}\$.53 615 \$\bar{1}\$.99 982 \$\bar{2}\$.66 769 \$\bar{2}\$.66 816 \$\bar{1}\$.33 184 \$\bar{1}\$.99 981 67 039 67 087 32 913 99 981 67 308 67 356 32 644 99 981 67 575 67 624 32 376 99 981 67 575 67 624 32 376 99 981 67 575 67 624 32 376 99 981 67 575 67 624 32 376 99 981 67 575 67 624 32 376 99 981 67 575 67 624 32 376 99 981 67 575 67 624 32 376 99 981 67 67 67 67 67 624 32 376 99 981 67 67 67 67 67 624 32 376 99 981 67 67 67 67 67 624 32 376 99 981 67 67 67 67 67 624 32 376 99 981 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67 67	55 23
40 \bar{2}.46 366 \bar{2}.46 385 \bar{1}.53 615 \bar{1}.99 982 \bar{2}.66 769 \bar{2}.66 816 \bar{1}.33 184 \bar{1}.99 \bar{2} \bar{2}.66 769 \bar{2}.66 816 \bar{1}.33 184 \bar{1}.99 \bar{2} \bar{2}.66 769 \bar{2}.66 816 \bar{1}.33 184 \bar{1}.99 \bar{2}.91	
41 46 799 46 817 53 183 99 981 67 039 67 087 32 913 99 981 42 47 226 47 245 52 755 99 981 67 308 67 356 32 644 99 981 43 47 650 47 669 52 331 99 981 67 575 67 624 32 376 99 981	-
42 47 226	
43 47 650 47 669 52 331 99 981 67 575 67 624 32 376 99	
	- 1
	- 1 -
45 \[\bar{2}.48 485 \[\bar{2}.48 505 \[\bar{1}.51 495 \[\bar{1}.99 980 \] \[\bar{2}.68 104 \[\bar{2}.68 154 \[\bar{1}.31 846 \[\bar{1}.99 980 \]	٠ ١
46 48 896 48 917 51 083 99 979 68 367 68 417 31 583 99 97	-
47 49 304 49 325 50 675 99 979 68 627 68 678 31 322 99 9	49 13
48 49 708 49 729 50 271 99 979 68 886 68 938 31 062 99 9	
49 50 108 50 130 49 870 99 978 69 144 69 196 30 804 99 9	-
50 $\overline{2}$.50 504 $\overline{2}$.50 527 $\overline{1}$.49 473 $\overline{1}$.99 978 $\overline{2}$.69 400 $\overline{2}$.69 453 $\overline{1}$.30 547 $\overline{1}$.99 9	
51 50 897 50 920 49 080 99 977 69 654 69 708 30 292 99 9	
52 51 287 51 310 48 690 99 977 69 962 30 038 99 9 53 51 673 51 696 48 304 99 977 70 159 70 214 29 786 99 9	
53 51 673 51 696 48 304 99 977	. >
55 2.52 434 2.52 459 T.47 541 T.99 976 2.70 658 2.70 714 T.29 286 T.99 9	
56 52 810 52 835 47 165 99 975 70 905 70 962 29 038 99 9	
57 53 183 53 208 46 792 99 975 71 151 71 208 28 792 99 9	42° 3
57 53 183 53 208 46 792 99 975 71 151 71 208 28 792 99 95 58 53 552 53 578 46 422 99 974 71 395 71 453 28 547 99 99	42 2
 59	
log oos log cot log tan log sin log oos log cot log tan log	in ,

LOG SIN, etc. 85°-88°

88°

(48)

87°

4° LOG SIN, etc.

		<u> </u>					<u> </u>	LUG 3	111, 6
	log sin	log tan	log oot	log cos	log sin	log tan	log cot	log cos	
0	2.71 880	2.71 940	1.28 060	ī,99 940	2.84 358	2.84 464	1.15 536	ī.99 894	60
I	72 120	72 181	27 819	99 940	84 539	84 646	15 354	99 893	59 58
3	72 359 72 597	72 420 72 659	27 580 27 34 I	99 939 99 938	84 718 84 897	84 826 85 006	15 174 14 994	99 892 99 891	58 57
4	72 834	72 896	27 104	99 938	85 075	85 185	14 815	99 891	56
5	2.73 069	2.73 I32	1.26 868	ī.99 937	2.85 252	2.85 363	1.14 637	ī.99 890	55
	73 303	73 366	26 634	99 936	85 429	85 540	14 460	99 889	54
7 8	73 535	73 600	26 400 26 168	99 936	85 605	85 717	14 283	99 888	53
9	73 7 ⁶ 7 73 997	73 832 74 063	26 168 25 937	99 935 99 934	85 780 85 955	85 893 86 069	14 107 13 93 I	99 887 99 886	52 51
10	73 997 2.74 226	2.74 292	1.25 708	1.99 934	2.86 128	2.86 243	1.13 757	ī.99 885	50
II	74 454	74 521	25 479	99 934	86 301	86 417	13 583	99 884	49
12	74 680	74 748	25 252	99 932	86 474	86 591	13 409	99 883	48
13	74 906	74 974	25 026	99 932	86 645	86 763	13 237	99 882	47
14	75 130	75 199	24 801	99 931	86 816	86 935	13 065	99 881	46
15 16	2.75 353	2.75 423 75 645	1.24 577	99 930	2.86 987 87 156	2.87 106 87 277	1.12 894	7.99 880 99 879	45 44
17	75 575 75 795	75 867	24 355 24 133	99 929 99 9 2 9	87 325	87 447	12 553	99 879	43
18	76 015	76 087	23913	99 928	87 494	87616	12 384	99 878	42
19	76 234	76 306	23 694	99 927	87 661	87 785	12 215	99 877	4 I
20	2.76 451	2.76 525	1.23 475	1.99 926	2.87 829	2.87 953	1.12 047	ī.99 876	40
21	76 667	76 742	23 258 23 042	99 926	87 995	88 120	11 880	99 875	39 38
22	76 883 77 097	76 958 77 1 73	23 042	99 9 25 99 924	88 161 88 326	88 287 88 453	11 713	99 874 99 873	
23 24	77 310	77 387	22 613	99 923	88 490	88 618	11 347	99 873	37 36
25	2.77 522	2.77 600	1.22 400	ī.99 923	2.88 654	2.88 783	1.11 217		35
26	77 733	77 811	22 189	99 922	88 817	88 948	11052	99 870	34
27	77 943	78 022	21 978	99 921	88 980	89 111	10 889	99 869	33
2 8	78 152 78 360	78 232 78 441	21 768 21 559	99 9 20 99 9 20	89 142	89 274	10 726	99 868	32
29					89 304	89 437	, 10 563	99 867	31
30 31	2.78 568 78 774	2.78 649 78 855	21 145	919 919	2.89 464 89 625	2.89 598 89 760	1.10 402 10 240	ī.99 866 99 865	30
31 32	78 979	79 061	20 939	99 917	89 784	89 920	10 080	99 864	29 28
33	79 183	79 266	20 734	99 917	89 943	90 080	09 920	99 863	27
34	79 386	_ 79 470	20 530	_ 99 916	90 102	90 240	09 760	99 862	26
35	2.79 588	2.79 673	1.20 327	1.99 915	2.90 260		1.09 601		25
36 37	79 789 79 990	79 875 80 076	20 125 19 924	99 914 99 913	90 417 90 574	90 557 90 715	09 443 09 285	99 860 99 859	24 23
37 38	80 189	80 277	19 723	99 913	90 574	90 713	09 205	99 858	23
39	80 388	80 476	19 524	99 912	90 885	91 029	08 971	99 857	21
40	2.80 585	2.80 674	1.19 326	1.99 911	2.91 040	2.91 185	1.08815	1.99 856	20
4I	80 782	80 872	19 128	99 910	91 195	91 340	o8 66o	99 855	19
42	80 978	81 068	18932	99 909	91 349	91 495	08 505	99 854	18
43 44	81 173 81 367	81 264 81 459	18 736 18 541	99 909 99 908	91 502 91 655	91 650 91 803	08 350 08 197	99 853 99 852	17 16
45	2.81 560	2.81 653	1.18 347		2.91 807	2.91 957	1.08 043	1.99 851	15
46	81 752	81 846	18 154	99 906	91 959	92 110	07 890	99 850	14
47	81 944	82 038	17 962	99 905	92 110	92 262	07 738	99 848	13
48	82 134	82 230	17 770	99 904	92 261	92414	07 586	99 847	12
49	82 324	82 420	17 580	99 904	92411	92 565	07 435	99 846 7.99 845	10
50 51	2.82 513 82 701	2.82 610 82 799	1.17 390	1.99 903 99 902	2.92 561 92 710	2.92 716 92 866	07 134	99 844	10
52	82 888	82 799 82 987	17 013	99 902 99 901	92 710	93 016	06 984	99 843	9 8
53	83 075	83 175	16 825	99 900	93 007	93 165	06 835	99 842	7 6
54	83 261	83 361	16 639	99 899	93 154	93 313	06 687	99 841	
55 56	2.83,446	2.83 547	1.16 453	T.99 898	2.93 301	2.93 462	1.06 538	1.99 840 99 839	5 4
50	-83 630 83 813	83 732 83 916	16 268 16 084	99 898 99 897	93 448 93 594	93 609 93 756	06 391 06 244	99 838	3
57 58	83 996	84 100	15 900	99 896	93 740	93 903	06 097	99 837	2
59 60	84.177	84 282	15718	_ 99 895	_ 93 885	_94 049	05 951	_99 836	I
60	2.84 358	2.84 464	1.15 536	ī.99 894	2.94 030	2.94 195	1.05 805	1.99 834	0
	log cos	log cot	log tan	log sin	log cos	log cot	log tan	log sin	_ ′

85° LOG SIN, etc.

	14, 610.								
	log sin	log tan	log cot	log oos	log sin .	log tan	log oot	log cos	
0'	2.94 030	2.94 195	1.05 805	1.99 834	ī.01 923	1.02 162	1.97 838	ī.99 761	60'
I	94 174	94 340	05 660	99 833	02 043	02 283	97 717	99 760	59 58
2	94 317	94 485	05 515	99 832	02 163	02 404	97 596	99 759	
3	94 461	94 630	05 370	99 831	02 283	02 525	97 475	99 757	57
4	94 603	94 773	05 227	99 830	02 402	02 645	97 355	_ 99 756	56
5 6	2.94 746 94 887	2.94 917 95 060	1.05 083	1.99 829 99 828	1.02 520	1.02 766	1.97 234	· ī.99 755	55
7	95 029	95 202	04 940 04 798	99 827	02 639 02 757	02 885	97 115	99 753	54
7 8	95 170	95 344	04 656	99 825	02 874	03 124	96 995 96 876	99 752	53
9	95 310	95 486	04 514	99 824	02 992	03 242	96 758	99 751 · 99 749	52
10	2.95 450	2.95 627	1.04 373	1.99 823	1.03 109		1.96 639		51
II	95 589	95 767	04 233	99 822	03 226	1.03 361		1.99 748	50
12	95 728	95 908	04 092	99 821	03 342	93 479 93 597	96 521 96 403	99 747	49
13	95 867	96 047	03 953	99 820	03 458	03 714	96 286	99 745 99 744	
14	96 005	96 187	03 813	99 819	03 574	03 832	96 168	99 7 44 99 742	47 46
15	2.96 143	2.96 325	1.03 675	1.99 817		1.03 948	1.96 052	1.99 741	45
16	96 280	96 464	03 536	99 816	03 805	04 065	95 935	99 740	44
17	96 417	96 602	03 398	99 815	03 920	04 181	95 819	99 738	43
18	96 553	96 739	03 261	99814	04 034	04 297	95 703	99 737	42
19	96 689	96 877	03 123	99 813	04 149	04 413	95 587	99 736	41
20	2.96 825	2.97 013	1.02 987	1.99 812	ī.04 262	ī.04 528	1.95 472	ī.99 734	40
21	96 960	97 150	02 850	99 810	04 376	04 643	95 357	99 733	30
22	97 095	97 285	02 715	99 809	04 490	04 758	95 242	99 731	38
23	97 229	97 421	217	99 808	04 603	04 873	95 127	99 730	37
24	97 363	_ 97 556		99 807	_ 04 715	_ 04 987	95 013	99 728	36
25	2.97 496	2.97 691	1.02 309	7.99 806		ī.05 101	1.94 899	1.99 727	35
26	97 629	97 825	02 175	99 804	04 940	05 214	94 786	99 726	34
27 28	97 762	97 959		99 803 99 802	05 052	05 328	94 672	99 724	33
29	98 026	98 092 98 225	-		05 164	05 441	94 559	99 723	32
	1 -			99 801	05 275	05 553	94 447	99 721	31
30	2.98 157	2.98 358		1.99 800		ī.05 666	1.94 334	1.99 720	30
31	98 288	98 490		99 798	05 497	05 778	94 222	99 718	29
32	98 419	98 622 98 753	0,	99 797	05 607	05 890	94 110	99 717	28
33 34	98 679	98 884 98 884		99 796	05 717	06 002 06 113	93 998 93 887	99 716	27
35	2.98 808	2.99 015	1.00 985	99 795	ī.05 937	ī.06 224		99 714	26
35 36	98 937	99 145	00 855 00 855	1.99 793 99 792	06 046	06 335	1.93 776 93 665	1.99 713 99 711	25
37	99 066	99 275	00 725	99 79 2 99 79 1	06 155	06 445	93 555	99 710	24
38	99 194	99 405	00 595	99 790	06 264	06 556	93 444	99 708	22
39	99 322	99 534		99 788	06 372	06 666	93 334	99 707	21
40	2.99 450		-	ī.99 787		ī.06 775	1.93 225	ī.99 705	20
41	2.99 577	2.99 791	1.00 209	99 786	06 589	06 885	93 115	99 704	19
42	2.99 704			99 785	06 696	06 994	93 006	99 702	18
43	2.99 830	1.00 046		99 783	06 804	07 103	92 897	99 701	17
44	2.99 956	ī.00 174		99 782	06 911	07 211	92 789	99 699	16
45	1.00 082	1.00 301	0.99 699	1.99 781	7.07 018	ī.07 320	1.92 680	7.99 698	15
46	00 207	00 427	99 573	99 780	07 124	07 428	92 572	99 696	14
47	00 332	00 553	99 447	99 778	07 231	07 536	92 464	99 69 5	13
48	00 456	00 679	99 321	99 777	07 337	07 643	92 357	99 693	12
49	00 581	_ 00 805	99 195	_ 99 776	07 442	07 751	92 249	99 692	II
50	ī.00 704		0.99 070	ī.99 775	ī.07 <u>5</u> 48	ī.07 8 <u>5</u> 8	1.92 142	1.99 690	10
51	00 828	01 055	98 945	99 773	07 653	07 964	92 036	99 689	9
52	00 951	01 179	98 821	99 772	07 758 07 863	08 071	91 929	99 687	8
53	01 074	01 303	98 697	99 771		08 177 08 283	91 823	99 686 99 684	7 6
54	01 196	01 427	98 573	99 769	07 968		91 717	7.99 683	1
55	01 440	01 673	0.98 450 98 327	1.99 768	1.08 072 08 176	ī.08 389 08 495	91 505	99 681	5 4
56	01 561	01 796	98 204	99 767 99 765	08 170	08 600	91 400	99 680	4
57 58	01 682	01 918	98 082	99 764	08 383	08 705	91 295	99 678	3 2
59	01 803	02 040	97 960	99 763	08 486	08 810	91 190	99 677	ī
59 60 ′	ī.01 923		0.97 838	7.99 761	1.08 589	ī.08 914	1.91 086	T.99 675	0'
	log cos	log cot	log tan	log sin	log 008	log cot	log tan	log sin	
	3	J .	J	J	3	<u> </u>	J		1

LOG SIN, etc. 81°-84° **84**°

(50)

83°

			<u> </u>				0	LOGS	יש, פוויי
'	log sin	log tan	log cot	log cos	log sin	log tan	log cot	log cos	
0'	ī.08 <u>5</u> 89	1.08 914	0.91 086	ī.99 675	ī.14 356	ī.14 780	0.85 220	ī.99 575	60′
I	08 692	09 019	90 981	99 674	14 445	14 872	85 128	99 574	59 58
2	08 795 08 897	09 123 09 227	90 877 90 773	99 672	14 535	14 963	85 037	99 572	58
3 4	o8 999	09 330	90 773	99 6 70 99 669	14 624 14 714	15 054 15 145	84 946 84 855	99 570 99 568	57 56
	1.09 101	1.09 434		1.99 667	1.14 803	ī.15 236		1.99 566	55
5 6	09 202	09 537	90 463	99 666	14 891	15 327	84 673	99 565	54
7 8	09 304	. 09 640	90 360	99 664	14 980	15417	84 583	99 563	53
	09 405	09 742	90 258	99 663	15 069	15 508	84 492	99 561	52
9	09 506	_ 09 845	90 155	99 661	- 15 157	15 598	84 402	_ 99 559	51
10	-	1.09 947	0.90 053 89 95 I	ī.99 659 99 658	1.15 245 15 333			1.99 557	50
11 12	09 707	10 049	89 850	99 656	15 421	15 777 15 867	84 223 84 133	99 556 99 554	49 48
13	09 907	10 252	89 748	99 655	15 508	15 956	84 044	99 552	47
14	10 006	10 353	89 647	99 653	15 596	16 046	83 954	99 550	46
15	ī.10 106	ī.10 454		1.99 651	7.15 683		0.83 865	ī.99 548	45
16	10 205	10 555	89 445	99 650	15 770	16/224	83 776	99 546	44
17 18	10 304	10 656 10 756	89 344 89 244	99 648 99 647	15 857 15 944	16 312 16 401	83 688 83 599	99 545	43
19	10 501	10 856	89 144	99 645	16 030	16 489	83 511	99 543 99 541	42 41
20	ī.10 599	ī.10 956		T.99 643	T.16 116			1.99 539	40
2U 2I	10 697	11 056	88 944	99 642	16 203	16 665	83 335	99 537	39
22	10 795	11 155	88 845	99 640	16 289	16 753	83 247	99 535	38
23	10 893	11 254	88 746	99 638	16 374	16 841	83 159	99 533	37
24	10 990	_ 11 353	88 647	99 637	16 460	16 928	83072	99 532	36
25	1.11 087	1.11 452	0.88 548 88 449	7.99 635 99 633	1.16 545 16 631	1.17 010	0.82 984 82 897		35
26 27	11 281	11 551 11 649	88 351	99 632	16 716	17 190	82 810	99 528 99 526	34
2 8	11 377	11 747	88 253	99 630	16 801	17 277	82 723	99 524	32
29	11 474	11 845	88 155	99 629	16 886	17 363	82 637	99 522	31
30	ī.11 570	1.11 943	0.88 057	ī.99 627	ī.16 970	ī.17 450		1.99 520	30
31	11 666	12040	87 960	99 625	17055	17 536	82 464	99 5 18	29
32	11 761	12 138	87 862 87 765	99 624 99 622	17 139	17 622	82 378 82 292	99 517	28
33 34	11 857	. 12 235 12 332	87 668	99 620	17 223 17 307	17 708 17 794	82 292 82 206	99 515 99 513	27 26
35	1.12 047	ī.12 428	•	ī.99 618	ī.17 391		0.82 120	1.00 511	25
36 36	12 142	12 525	87 475	99 617	17 474	17 965	82 035	99 509	24
37`	12 236	12 621	87 379	99 615	17 558	18051	81 949	99 507	23
38	12 331	12 717	87 283	99 613	17 641	18 136	81 864	99 505	22
39	12 425	- 12 813	87 187	99 612	17 724	18 221	81 779	_ 99 503	21
40	1.12 519	1.12 909		1.99 610 99 608	1.17 807 17 890	18 306	0.81 694	7.99 501	20
41 42	12 706	13004	86 996 86 901	99 607	17 973	18 391 18 475	81 609 81 525	99 499 99 497	19
43	12 799	13 194	86 806	99 605	18 055	18 560	81 440	99 497	17
44	12892	13 289	86 711	99 603	18 137	18 644	81 356	99 494	16
45	1.12 985	1.13 384		1.99 601		1.18 728		ī.99 492	15
46	13078	13478	86 522	99 600	18 302	18 812	81 188	99 490	14
47 48	13 171	13 573 13 667	86 427 86 333	99 598 99 596	18 383 18 465	18 896 18 9 7 9	81 104 81 021	99 488 99 486	13 12
40 49	13 355	13 761	86 239	99 595	18 547	19 063	80 937	99 484	11
50			0.86 146				0.80 854		10
51	13 539	13 948	86 052	99 591	18 709	19 229	80 771.	99 480	
52	13 630	14 041	85 959	99 589	18 790	19 312	8o 688	99 478	9 8
53	13 722	14 134	85 866	99 588	18871	19 395	80 605	99 476	7 6
54	13813	14 227	85 773	99 586	18952	19 478	80 522 0.80 439	99 474 1.99 472	
55 56	13 904	14 412	0.85 680 85 588	1.99 584 99 582	1.19 033	19 561	80 357	99 472	5 4
57	14 085	14 504	85 496	99 581	19 193	19 725	80 275	99 468	3
57 58	14 175	14 597	85 403	99 579	19 273	19 807	80 193	99 466	2
59	14 266	_ 14 688	85 312	_ 99 577	_ 19 353	19 889	80 111	99 464	1,
60′	1.14 356	1.14 780	0.85 220	1.99 575	1.19 433	1.19 971	0.80 029	1.99 462	0'
1	log cos	log cot	log_tan	log sin	log ocs	log cot	log tan	log sin	1

81° LOG SIN, etc. 81°-84°

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u	1

	iv, etc.							140
	log sin		oot log oos	log sin	log tan	log oot	log cos	
0′	1.19 433	ī.19 971 o.80		1.23 967	ī.24 632	0.75 368	ī.99 335	60'
I	19513		947 99 460	24 039	24 706	75 294	99 333	59 58
2	19 592		866 99 458	24 1 10	24 779	75 221	99 331	
3	19 672 19 751		784 99 456 703 99 454	24 181	24 853	75 147	99 328	57
4		ī.20 378 0.79		24 253 1.24 324	24 926 1.25 000	75 074	99 326	56
5 6	19 909		541 99 450	24 395	25 073	0.75 000 74 927	1.99 324 99 322	55
	19 988		460 99 448	24 466	25 146	74 854	99 322	54 53
7 8	20 067		379 99 446	24 536	25 219	74 781	99 317	52
9	20 145		299 99 444	24 607	25 292	74 708	99 315	51
10	Ī.20 223	ī.20 782 0.79	218 7.99 442	ī.24 677	ī.25 365	0.74 635	ī.99 313	50
11	20 302	20 862 79	138 99 440	24 748	25 437	74 563	99 310	49
12	20 380	20 942 79	058 99 438	24 818	25 510	74 490	99 308	48
13	20 458		978 99 436	24 888	25 582	74 418	99 30 6	47
14	20 535		898 99 434	24 958	25 655	74 345	_ 99 304	46
15 16	20 691	1.21 182 0.78 21 261 78	818 1.99 432	1.25 028	1.25 727	0.74 273	1.99 301	45
17	20 768	21 341 78	739 99 429 659 99 427	25 098 25 168	25 799	74 201	99 299	44
18	20 845		659 99 427 580 99 425	25 237	25 871 25 943	74 129 74 057	99 297	43
19	20 922	21 499 78	501 99 423	25 307	25 943 26 015	73 985	99 294 99 292	42 41
20	1.20 999	_	422 <u>1</u> .99 421	1.25 376		-		
21	21 076		343 99 419	25 445	26 158	0.73 914 73 842	1.99 290 99 288	40
22	21 153	21 736 78	264 99417	25 514		73 771	99 285	39 38
23	21 229	21 814 78	186 99415	25 583		73 699	99 283	37
24	21 306		107 _ 99 413	25 652	26 372	73 628	99 281	36
25	1.21 382		029 <u>1</u> .99411	1.25 721		0.73 557	ī.99 278	35
26	21 458		951 99 409	25 790		73 486	99 276	34
27	21 534		873 99 407	25 858		73415	99 274	33
28 29	21 610	~	795 99404	25 927		73 345	99 271	32
	1_		717 99 402	25 995			99 269	31
30	1.21 761		639 1.99 400	1.26 063			Ī.99 267	30
31 32	21 836		7 562 99 398 7 484 99 396	26 131 26 199		73 133 73 063	99 264 99 262	29 28
33	21 987		7 484 99 396 7 407 99 394	26 267		72 992		20
34	22 062	9	330 99 392	26 335		72 992	99 257	26
35	Ī.22 137		253 1.99 390	ī.26 403				25
36	22 211		176 99 388	26 470		72 782	99 252	24
37	22 286		099 99 385	26 538	27 288	72 712	99 250	23
38	22 361		023 99 383	26 605		72 643	99 248	22
39	22 435		946 99 381	26 672		7 ² 573	99 245	21
40	Ī.22 509		870 T.99 379	ī.26 739			1.99 2 43	20
41	22 583		794 99 377	26 806	27 566		99 241	19
42	22 657		99 375	26 873		72 365	99 238	18
43	22 731		641 99 372	26 940		72 296 72 227	99 236 99 233	17
44	22 805		565 99 370 490 1.99 368	27 007			799 233 1.99 231	15
45	1.22 878		490 1 .99 368 414 99 366	1.27 073 27 140		72 089	99 229	14
46 47	23 025		339 99 364	27 206			99 226	13
47 48	23 098		263 99 362	27 273			99 224	12
49	23 171		188 99 359	27 339	0		99 221	II
50	1.23 244	ī.23 887 0.76		1.27 405		0.71 814	ī.99 219	10
51	23 317		038 99 355	27 471	28 254	71 746	99 217	
52	23 390	24 037 75	963 99 353	27 537	28 323	71 677	99 214	9 8
53	23 462	24 112 75	888 99 351	27 602	28 391	71 609	99 212	7
54	23 535	24 186 75	814 _ 99 348	27 668		71 541	99 209	
55	1.23 607	1.24 261 0.75		1.27 734	ī.28 527		1.99 207	5 4 3 2
56	23 679		665 99 344	27 799	28 595	71 405	99 204	4
57 58	23 752		590 99 342	27 864	28 662 28 730	71 338 71 270	99 202 99 200	2
50	23 823		516 99 340 442 99 337	27,930 27,995	28 730	71 202	99 197	l I
59 60 ′	1.23 967	1.24 632 0.75		I.28 060		0.71 135	1.99 195	0'_
1-00	log cos		tan log sin	log oos	log oot	log tan	log sin	,
	1 -05 000		,		6 550	6		

LOG SIN, etc. 77°-80°

80°

(52)

79°

,	11°	1	2° Log sii	<u>n,</u>
0'	log sin log tan log oot log oos 1.28 060 1.28 865 0.71 135 1.99 195		og cot log oos	
ĭ	1.28 060 1.28 865 0.71 135 1.99 195 28 125 28 933 71 067 99 192	1.31 788 1.32 747 0.0 31 847 32 810	67 253 T.99 040	60
2	28 190 29 000 71 000 99 190		67 190 99 038 67 128 99 035	59 58
3	28 254 29 067 70 933 99 187	31 966 32 933	67 067 99 032	57
4	28 319 29 134 70 866 99 185 1.28 384 1.29 201 0.70 700 1.00 182		67 005 99 030	56
5 6	28 448 29 268 70 732 99 180		56 943 1.99 027 56 881 99 024	55
7 8	28 512 29 335 70 665 99 177	32 202 33 180 6	56 881 99 024 56 8 2 0 99 022	54 53
	28 577 29 402 70 598 99 175 28 641 29 468 70 532 99 172		6 758 99 019	52
9 10				51
11	1.28 705 1.29 535 0.70 465 1.99 170 28 769 29 601 70 399 99 167			50
12	28 833 29 668 70 332 99 165		66 574 99 011 66 513 99 008	49 48
13	28 896 29 734 70 266 99 162	32 553 33 548 6	6452 99 005	47
14	28 960 29 800 70 200 99 160	32 612 33 609 6	6 391 99 002	46
15 16	1.29 024 1.29 866 0.70 134 1.99 157 29 087 29 932 70 068 99 155			45
17	29 150 29 998 70 002 99 152	32 728 33 731 6 32 786 33 792 6		44 43
18	29 214 30 064 69 936 99 150	32 844 33 853 6	6147 98991].	42
19	29 277 30 130 69 870 99 147	32 902 33 913 6		41
20	1.29 340 1.30 195 0.69 805 1.99 145			40
2I 22	29 403 30 261 69 739 99 142 29 466 30 326 69 674 99 140		5 966 98 983 5 905 98 980	39 38
23	29 529 30 391 69 609 99 137	33 133 34 155 6	5 845 98 978	37
24	29 591 30 457 69 543 99 135	33 190 34 215 6	5 785 98 975	36
25 26	1.29 654 1.30 522 0.69 478 1.99 132		5 724 Ī.98 972	35
27	29 716 30 587 69 413 99 130 29 779 30 652 69 348 99 127			34
28	29 841 30 717 69 283 99 124			33 32
29	29 903 30 782 69 218 99 122			31
30	1.29 966 1.30 846 0.69 154 1.99 119	1.33 534 1.34 576 0.6	5 424 T.98 958 3	30
31 32	30 028 30 911 69 089 99 117 30 090 30 975 69 025 99 114	33 591 34 635 6	5 365 98 955 2	29
33	30 090 30 975 69 025 99 114 30 151 31 040 68 960 99 112			28
34	30 213 31 104 68 896 99 109	33 761 34 814 6		27 26
35	1.30 275 1.31 168 0.68 832 1.99 106		5 1 2 6 1 . 9 8 9 4 4 2	25
36 37	30 336 31 233 68 767 99 104 30 398 31 297 68 703 99 101		- 0 0 0	24
38	30 459 31 361 68 639 99 099			23 22
39	30 521 31 425 68 575 99 096			21
4 0	ī.30 <u>5</u> 82 ī.31 489 0.68 511 ī.99 093			20
41 42	30 643 31 552 68 448 99 091	34 156 35 229 64	1771 98 927 I	19
43	30 704 31 616 68 384 99 088 30 765 31 679 68 321 99 086			18
44	30 826 31 743 68 257 99 083			17 16
45	1.30 887 1.31 806 0.68 194 1.99 080	ī.34 380 ī.35 464 0.64	536 T.98 916 I	15
46 47	30 947 31 870 68 130 99 078 31 008 31 933 68 067 99 075	34 436 35 523 64	1477 98 913 1	14
47 48	31 008			13 12
49	31 129 32 059 67 941 99 070			11
50	1.31 189 1.32 122 0.67 878 1.99 067	1.34 658 1.35 757 0.64		LO
51	31 250 32 185 67 815 99 064	34 713 35 815 64	185 98 898	9
52 53	31 310 32 248 67 752 99 062 31 370 32 311 67 689 99 059		127 98 896 8 069 98 893	8
54	31 430 32 373 67 627 99 056		. 069 98 893 7 . 011 98 890 6	7
55	Ī.31 490	1.34 934 1.36 047 0.63	953 7.98 887	5
56	31 549 32 498 67 502 99 051		3 8 9 5 9 8 8 8 4 1 4 4 1 4 1 4 1 4 1 4 1 4 1 4 1	4
57 58	31 609		8 8 3 7 9 8 8 8 1 1 3 8 8 7 9 8 8 7 8 1 3	3
59	31 728 32 685 67 315 99 043	35 154 36 279 63	; 721 98875 1	I
59 60 ′	1.31 788 1.32 747 0.67 253 1.99 040	ī.35 209 ī.36 336 o.63	664 7.98 872	<u>0′</u>
	log cos log cot log tan log sin	log cos log cot log	tan log sin	7

(53)

OG S	IN, etc.	19					14		
,	log sin	log tan	log cot	log cos	log sin	log tan	log cot	log oos	
0′	1.35 209				ī.38 368	1.39 677	0,60 323	ī.98 690	60'
I 2	35 263 35 318	36 394 36 452	63 606 63 5 48	98 869 98 867	38 418 38 469	39 731 39 785	60 269	98 687	59 58
3	35 373	36 509	63 491	98 864	38 519	39 705	60 21 5 60 162	98 684 98 681	
4	35 427	_ 36 566	63 434	98 861	38 570	39 892	60 108	98 678	57 56
5 6	1.35 481			1.98 858	ī.38 620	1.39 945	0.60 055	ī.98 675	55
	35 536 35 590		63 319 63 262	98 855 98 852	38 670 38 721	39 999	60 001	98 671	54
7 8	35 644	36 795	63 205	98 849	38 771	40 052 40 106	59 948 59 894	98 668 98 665	53
9	35 698	36852	63 148	98 846	38 821	40 159	59 841	98 662	52 51
10	1.35 752	ī.36 909			ī.38 871	Ī.40 212		ī.98 659	50
11 12	35 806 35 860	36 966	,0 0.	98 840	38 921	40 266	59 734	98 656	49
13	35 914		62 977 62 920	98 837 98 834	38 971 39 021	40 319	59-68r		48
14	35 968	37 137	62 863		39 021	40 372 40 425	59 628 59 575	98.64 <u>9</u> 98.646	47 46
15	Ī.36 022	ī.37 193		ī.98 828	1.39 121	ī.40 478	0.59 522		45
16	36 075		62 750	98 825	39 170	40 531	59 469	98 640	44
17 18	36 129 36 182			98 822 98 819	39 220	40 584	59 416		43
19	36 236		62 581	98 816	39 270 39 319	40 636 40 689	59 364 59 311	98 633 98 630	42
20	7.36 289		-	-	ī.39 369	T.40 742		7.98 627	41
21	36 342	37 532	62 468	98 810	39 418	40 795	59 205	98 623	40 39
22	36 395		62 412	98 807	39 467	40 847	59 153	98 620	38
23 24	36 449 36 502				39 517	40 900	59 100	98 617	37
25	ī.36 555	1.37 756			39 566 7.39 615	40 952 7.41 005	59 048 0.58 995	98 614 7.98 610	36
26	36 608	37 812	62 188	98 795	39 664	41 057	58 943	98 607	35 34
27 28	36 660		62 132	98 792	39 713	41 109	58 8g I	98 604	33
28 29	36 713 36 766		62 076 62 020		39 762	41 161	58 839	98 60i	32
30	T.36 819				39 811	41 214	58 786	98 597	31
31	36 871	38 091	0.61 965 61 909		ī.39 860 39 909	1.41 266 41 318	0.58 734 58 682	ī.98 594	30
32	36 924	38 147	61 853	98 777	39 909	41 370	58 630	98 591 98 588	29 28
33	36 976		61 798	98 774	40 006	41 422	58 578	98 584	27
34	37 028	_ 38 257	61 743	98 77 i	_ 40 055	41 474	58 526	98 581	26
35 36	37 133	ī.38 313 38 368	0.61 687 61 632			1.41 526	0.58 474	1.98 578	25
37	37 185	38 423	61 577	98 765 98 762	40 152 40 200	41 578 41 629	58 422 58 371	98 574 98 571	24 23
37 38	37 237	38 479	61 521	98 759	40 249	41 681	58 319	98 568	22
39	37 289	38 534	61 466		40 297	41 733	58 267	98 565	21
40	ī.37 341	ī.38 <u>5</u> 89	0.61 411	T.98 753	ī.40 346		0.58 216	7.98 561	20
4I	37 393	38 644 38 699	61 356 _61 301	98 750	40 394	41 836	58 164	98 558	19
42 43	37 445 37 497	38 754	61 246	98 746 98 743	40 442 40 490	41 887 41 939	58 113 58 061	98 555 98 551	18 17
44	37 549	38 808	61 192	98 740	40 538	41 990	58 010	98 548	16
45	ī.37 600	7.38 863	0.61 137	ī.98 737		Ĩ.42 041	0.57 959	ī.98 545	15
46	37 652	38 918	61 082	98 734	40 634	42 093	57 907	98 541	14
47 48	37 7°3 37 755	38 972 39 027	61 028 60 973	98 731 98 728	40 682 40 730	42 I44 42 I95	57 856 57 805	98 538 98 535	13 12
49	37 806	39 082	60 918	98 725	40 778	42 246	57 754	98 531	11
50	ī.37 858		0.60 864	1.98 722	1.40 825	ī.42 297		ī.98 528	10
51	37 909	39 190	60 810	98 719	40 873	42 348	57 652	98 525	9
52	37 960	39 245	60 755	98 715	40 921	42 399	57 601	98 521	8
53 54	38 of 1 38 of 2	39 299 39 353	60 701 60 647	98 712 98 709	40 968 41 016	42 450 42 501	57 550 57 499	98 518 98 515	9 8 7 6
54	ī.38 113	1.39 407	0.60 593	1.98 706	1.41 063	T.42 552	0.57 448	7.98 511	
55 56	38 164	39 461	60 539	98 703	41 111	42 603	57 397	98 508	4
57	38 215	39 515	60 485	98 700	41 158	42 653	57 347	98 505	5 4 3 2
58	38 266 38 317	39 569 _ 39 623	60 431 60 377	98 697 98 694	41 205 41 252	42 704 _ 42 755	57 296 57 245	98 501 98 498	2
57 58 59 60	ī.38 368	1.39 677	0.60 323	7.98 690	1.41 300	T.42 805	0.57 195	1.98 494	Ô'
	log cos	log cot	log tan	log sin	log oos	log cot	log tan	log sin	

LOG SIN, etc. 73°-76°

76°

(54)

75°

 16° LOG SIN, etc.

_							16°	LOG	3IN, e
0'	log sin	log tan	log oot	log oos	log sin	log tan	log oot	log oos	
U'	41 347		0.57 195 57 I44		1.44 034				60′
2	41 394	. 42 906	57 094	98 488	44 078 44 122	45 845	54 203 54 155		59 58
3	41 441		57 043	98 4 84	44 166	45 892	54 108	98 273	57
4 5	1.41 535				44 210 T 44 252		54 060	98 270	56
5 6	41 582	43 108	56 892	98 474	1.44 253 44 297			7.98 266 98 262	55 54
7 8	41 628	43 158	56 842	98 471	44 341	46 082	53918	98 259	54 53
8	41 675				44 385 44 428	46 130 46 177	53870	98 255	52
10	1.41 768	ī.43 308		ī.98 460	744 420 1.44 472			98 251 1.98 248	51 50
II	41815	43 358	56 642	98 457	44 516	46 271	53 729	98 244	49
12	41 861 41 908	43 408	56 592 56 542	98 453	44 559 44 602	46 319 46 366	53 681	98 240	48
13	41 908		56 542 56 492	98 450 98 447	44 646	46 413	53 634 53 587	98 2 37 98 2 33	47 46
15	1.42 001	ī.43 558	0.56 442	ī.98 443	ī.44 689	ī.46 460	0.53 540	1.98 229	45
16	42 047	43 607	56 393	98 440	44 733	46 507	53 493	98 226	44
17 18	42 093 42 I40	43 657 43 707	56 343 56 293	98 436 98 433	44 776 44 819	46 554 46 601	53 446 53 399	98 222 98 218	43
19	42 186	43 756	56 244	98 433 98 42 9	44 862	46 648	53 359	98 21 5	42 41
20	ī.42 232	ī.43 806	0.56 194	1.98 426	1.44 905	ī.46 694	0.53 306	1.98 211	40
21	42 278	43 855	56 145	98 422	44 948	46 741	53 259	98 207	39 38
22 23	42 324 42 370	43 905 43 954	56 095 56 046	98 419 98 415	44 992 45 035	46 788 46 835	53 212 53 165	98 204 98 200	38
24	42416	43 954	55 996	98412	_ 45 °77	46 881	53 105	98 196	37 36
25	1.42 461	ī.44 053	0.55 947	ī.98 409	ī.45 120	ī.46 928	0.53 072	ī.98 192	35
26 27	42 507 42 553	44 102 44 151	55 898 55 849	98 405 98 402	45 163 45 206	46 975 47 021	53 025 52 979	98 189 98 185	34
28	42 599	44 151 44 201	55 849 55 799	98 398	45 200 45 249	47 068	52 932	98 181	33 32
29	42 644	44 250	55 750	98 395	45 292	47 114	52 886	98 177	31
30	1.42 690	1.44 299	0.55 701	ī.98 391	1.45 334		0.52 840	ī.98 174	30
31 32	42 735	44 348 44 397	55 652 55 603	98 388	45 377 45 419	47 207	52 793	98 170 98 166	29
33	42 826	44 397 44 446	55 603 55 554	98 384 98 381	45 462	47 253 47 299	52 747 52 701	98 162	28 27
34	42 872	44 495	55 505	98 377	_ 45 504	47 346	52 654	98 159	26
35 36	1.42917 42962	1.44 544	0.55 456	ī.98 373	1.45 547	1.47 392	0.52 608	7.98 155	25
37	42 902	44 592 44 641	55 408 55 359	98 370 98 366	45 589 45 632	47 438 47 484	52 562 52 516	98 151 98 147	24 23
37 38	43 053	44 690	55 310	98 363	45 674	47 530	52 470	98 144	23 22
39	43 098	44 738	55 262	98 359	45 716	47 576	52 424	98 140	21
40 41	1.43 143 43 188	ī.44 787 44 836	0.55 213	1.98 356	ī.45 758 45 801	1.47 622	0.52 378		20
41 42	43 188	44 836 44 884	55 164 55 116	98 352 98 349	45 843	47 668 47 714	52 332 52 286	98 132 98 129	19 18
43	43 278	44 933	55 067	98 345	45 885	47 760	52 240	98 125	17
44 45	43 323	44 981	55 019	98 342	45 927	47 806	52 194	98 121	ΙĞ
45 46	1.43 367 43 412	1.45 029 45 078	0.54 97 I 54 922	ī.98 338 98 334	ī.45 969 46 01 1	1.47 852 47 897	0.52 148 52 103	1.98 117 98 113	15
47 48	43 457	45 126	54 874	98 331	46 053	47 943	52 057	98 110	14 13
	43 502	45 174	54 826	98 327	46 095	47 989	52011	98 106	12
49 50	43 546 1.43 591		54 778	98 324 T 08 220	46 136 7 46 138	48 035 T 48 080	51 965	98 102	11
51	43 635	1.45 271 45 319	54 681	ī.98 320 98 317	ī.46 178 46 220	1.48 080 48 126	0.51 920 51 874	ī.98 098 98 094	10
52	43 680	45 367	54 633	98 313	46 262	48 171	51829	98 o go	9 8
53 54	43 724 43 769	45 415 45 463	54 585 ·	98 309	46 303	48 217	51 783	98 087	7
54 55		45 463 1.45 511	54 537 0.54 489	98 306 1.98 302	46 345 7.46 386	48 262 7.48 307	51 738 0.51 693	98 083 1.98 079	
56	43 857	45 559	54 441	98 299	46 428	48 353	51 647	98 075	5 4
57 58	43 901	45 606	54 394	98 295	46 469	48 398	51 602	98 071	3 2
50 59	43 946 43 990	45 654 45 702	54 346 54 298	98 291 98 288	46 511 46 552	48 443 48 489	51 557 51 511	98 067 98 063	2 I
59 60 ′	ī.44 034	ī.45 750	0.54 250	1.98 284	ī.46 594	1.48 534	0.51 466	ī.98 o6o	<u>0′</u>
	log cos	log oot	log tan	log sin	log oos	log oot	log tan	log sin	,

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73°

LOG SIN, etc. 73°-76°

18°

.Q	G 31	N, etc.	1.0			10				
Ì	,	log sin	log tan	log oot	log oos	log sin	log tan	log cot	log cos	
-	0′	1.46 594	1.48 534	0.51 466	1.98 060	ī.48 998		0.48 822	ī.97 821	60'
	I 2	46 635 46 676	48 579 48 624	51 421	98 056 98 052	49 037	51 221	48 779	97 817	59 58
1	3	46 717	48 669	51 376 51 331	98 048	49 076 49 115	51 264 51 306	48 736 48 694	97 812 97 808	
-	4	46 758	48 714	51 286	98 044	49 153	51 349	48 651	97 804	57 56
1	5 6	ī.46 800	ī.48 759	0.51 241	7.98 040	1.49 192	ī.51 392		1.97 800	55
		46 841 46 882	48 804	51 196	98 0 36	49 231	51 435	48 565	97 796	54
	7 8	46 923	48 849 48 894	51 151 51 106	98 032 98 029	49 269	51 478	48 522	97 792	53
	9	46 964	48 939	51 061	98 025	49 308 49 347	51 520 51 563	48 480 48 437	97 788 97 784	52
	10	ī 47 005		0.51 016			ī.51 606	0.48 394	ī.97 779	51 50
Ì	ΙI	47 045	49 029		-98 017	49 424	51 648	48 352	97 775	
	12	47 086	49 073	50 927		49 462	51 691	48 309	97 771	49 48
	13 14	47 127 47 168	49 118 49 163	50 882 50 837	98 009 98 005	49 500	51 734	48 266	97 767	47
	15	1.47 209		0.50 793		49 539 1.49 577	51 776 1.51 819	48 224 0.48 181	97 763	46
	16	47 249	49 252			49 615	51 861	48 139	1.97 759 97 754	45
	17	47 290	49 296		97 993	49 654	51 903	48 097	97 750	43
	19	47 330 47 37 I	49 341 49 385	50 659 50 615		49 692	51 946	48 054	97 746	42
	20	T.47 411	-			49 730	51 988	48 012	97 742	41
	2I	47 452	49 474	0.50 570 50 526		49 806	ī.52 031 52 073	0.47 969 47 927	ī.97 738	40
	22	47 492	49 519		97 974	49 844	52 115	47 885	97 734 97 729	39 38
	23	47 533	49 563			49 882	52 157	47 843	97 725	37
	24	47 573 1.47 613	49 607	50 393 0.50 348		49 920	_ 52 200	47 800	_ 97 721	36
	25 26	47 654	49 696			49 958	1.52 242 52 284	0.47 758 47 716		35
	27 28	47 694	49 740		97 954	50 034	52 326	47 674	97 713 97 708	34
		47 734	49 784	•	97 950	50 072	52 368	47 632	97 704	32
	29	47 774	49 828			50 110	52 410	47 590	9 7 700	31
	30 31	7.47 814 47 854	ī.49 872 49 916			1.50 148		0.47 548	ī.97 696	30
	32	47 894	49 960			50 185 50 223	52 494 52 536	47 506 47 464	97 691 97 687	29 28
	33	47 934	50 004			50 261	52 578	47 422	97 683	27
	34	_ 47 974	_ 50 048			_ 50 298	52 620	47 380	97 679	26
	35 36	1.48 014 48 054		0.49 908 49 864				0.47 339	1.97 674	25
	37	48 094	50 136 50 180			50 374 50 411	52 703 52 745	47 297 47 255	97 670 97 666	24 23
	38	48 133	50 223	49 777	97 910	50 449	52 787	47 213	97 662	22
	39	48 173	50 267	49 733	97 906	50 486	52 829	47 171	97 657	21
ı	40	1.48 213	ī.50 311	0.49 689		ī.50 523		0.47 130	1.97 653	20
ı	41	48 252 48 292	50 355	49 645 49 602	97 898 97 894	50 561 50 598	52912	47 088	97 649	19 18
1	42 43	48 332	50 398 50 442	49 558	97 890	50 635	52 953 52 995	47 047 47 005	97 645 97 640	17
ı	44	48 371	50 485	49 515	97 886	50 673	53 037	46 963	97 636	16
ı	45	1.48 411	ī.50 529	0.49 471	1.97 882	1.50 710		0.46 922	7.97 632	15
1	46	48 450 48 490	50 572 50 616	49 428	97 878 97 874	50 747 50 784	53 120 53 161	46 880 46 839	97 628 97 623	14
ı	47 48	48 529	50 659	49 384 49 34 I	97 874 97 870	50 821	53 202	46 798	97 619	13 12
ľ	49	48 568	50 703	49 297	97 866	50 858	53 244	46 756	97 61 <u>5</u>	, II
1	50	ī.48 607	ī.50 746	0.49 254	ī.97 861	ī.50 896	ĩ.53 285	0.46 715	ī.97 610	10
	51	48 647	50 789	49 211	97 857 97 853	50 933	53 327	46 673	97 606	9 8
	52 53	48 686 48 725	50 833 50 876	49 167 49 124	97 853 97 849	50 970 51 007	53 368 • 53 409	46 632 46 591	97 602 97 597	7
ı	54	48 764	50 919	49 081	97 845	51 043	53 450	46 550	97 593	7 6
I	55	1.48 803	ī.50 962	0.49 038	1.97 841	ī.51 0 80	ī.53 492	0.46 508	ī.97 589	
ı	56	48 842	51 005 51 048	48 995	97 837	51 117	53 533	46 467	97 584	4
ı	57	48 881 48 920	51 048	48 952 48 908	97 833 97 829	51 154 51 191	53 574 53 615	46 426 46 385	97 580 97 5 7 6	5 4 3 2
1	54 55 56 57 58 59 60 '	48 959	_ 51 135	48 865	97 825	_ 51 227	_ 53 656	46 344	_ 97 57 I	I
	<u>60′</u>	ī.48 998	1.51 178	0.48 822	1.97 821	1.51 264	1.53 697	0.46 303	1.97 567	0'_
L		log cos	log oot	log tan	log sin	log oos	log oot	log tan	log sin	,

LOG SIN, etc. 69°-72°

72°

 20° LOG SIN, etc.

	1 1	19					<u>20°</u>	LOG	<u> 3IN,</u> e
0'	log sin	log tan	log cot	log cos		g tan	log cot	log oos	
I	1.51 264 51 301	1.53 697 53 738	0.46 303 46 262	1.97 567 97 563		6 107 6 146			60′
2 2	51 338	53 779	46 221	97 558.	53 475 5	6 185	43815	9 7 2 94 9 7 2 89	59 58
3 4	51 374 51 411	53 820 53 861	46 180 46 139	97 554 97 550	53 509 5	6 224 6 264	43 776	97 285	57
5	1.51 447	ī.53 902	0.46 098	1.97 545		6 303		97 280 1.97 276	56
	51 484	53 943	46 057	97 541	53 613 50	6 342	43 658	97 271	54
7 8	51 520	53 984 54 025	46 01 6 45 975	97 536 97 532		6 381 6 420	43 619 43 580	97 266 97 262	53
9	51 593	54 065	45 935	97 528		6 459	43 541	97 202 97 257	52 51
10	1.51 629	1.54 106	0.45 894	1.97 523		6 498	0.43 502	1.97 252	50
11 12	51 666	54 147 54 187	45 853 45 813	97 519 97 515		6 537 6 576	43 463 43 424	97 248 97 243	49 48
13	51 738	54 228	45 772	97 510	53 854 56	6 615	43 385	97 243 97 238	47
14	51 774 1.51 811	54 269 1.54 309	45 731 0.45 691	97 506		6 654	43 346	97 234	46
15 16	51 847	54 350	45 650	ī.97 501 97 497		6 693 6 732	0.43 307 43 268	1.97 229 97 224	45 44
17	51 883	54 390	45 610	97 492	53 991 56	5 771	43 229	97 220	43
18 19	51 919	54 431 54 471	45 569 45 529	97 488 97 484		5 8 i o 5 8 4 9	43 190 43 151	97 215 97 210	42 41
20	ī.51 991	ī.54 512	0.45 488	7,404 1.97,479		5 887	0.43 113	7, 210 7.97 206	40
21	52 027	54 552	45 448	97 475	54 127 56	926	43 074	97 201	39
22 23	52 063 52 099	54 593 54 633	45 407 45 367	97 470 97 466		5 965 7 004	43 035 42 996	97 196 97 192	38
24	52 135	54 673	45 327	97 461	_ 54 229 _ 57	7 004	42 996 42 958	97 192 97 187	37 36
25 26	1.52 171	ī.54 714	0.45 286	ī.97 457	1.54 263 1.57	7 081	0.42 919	ī.97 182	35
26 27	52 207 52 242	54 754 54 794	45 246 45 206	97 453 97 448		7 120 7 158	42 880 42 842	97 178 97 173	34
28	52 278	54 835	45 165	97 444	54 3 ⁶ 5 57	7 197	42 803	97 168	33 32
29 20	52 314	54 875	45 125	97 439	54 399 57	235	42 765	97 163	31
30 31	1.52 350 52 385	1.54 915 54 955	0.45 085 45 045	1.97 435 97 430					30
32	52 421	54 995	45 005	97 430 97 426	54 500 57	7 312 7 351	42 688 42 649	97 154 97 149	29 28
33	52 456	55 035	44 965	97 421	54 534 57	389	42 611	97 145	27
34 35	52 492 1.52 527	55 075 1.55 115	44 925 0.44 885	97 417 1.97 412		428 466	42 572 0.42 534	97 140 1.07 135	26 25
36	52 563	55 155	44 845	97 408	54 635 57	504	0.42 534 42 496	97 135 97 130	25 24
37 38	52 598 52 634	55 195	44 805	97 403	54 668 57	543	42 457	97 126	23
39	52 669	55 235 55 275	44 765 44 725	97 399 97 394	54 702 57 54 735 57	581 619	42 419 42 381	97 121 97 116	22 2I
40	1.52 705	1.55 315	0.44 685	ī.97 390			0.42 342		20
4I	52 740	55 355	44 645	97 385	54 802 57	696	42 304	97 107	19
42 43	52 775 52 811	55 395 55 434	44 605 44 566	97 381 97 376	. 07	734	42 266	97 102 97 097	18
44	52 846	55 474	44 526	97 372	54 903 57	810	42 220	97 097 97 092	17 16
45 46	1.52 881 52 016			ī.97 367	T.54 936 T.57	849	0.42 151	ī.97 087	15
47	52 916 52 951	55 554 55 593	44 446 44 407	97 363 97 358		887 925	42 113 42 075	97 083 97 078	14 13
48	52 986	55 633	44 367	97 353	55 036 57	963	42 037	97 073	12
49 50	53 021	55 673	44 327	97 349	55 069 58	001	41 999	97 068	11
50 51	1.53 056 53 092	1.55 712 55 752	0.44 288 44 248	ī.97 344 97 340		039 077	0.41 961 41 923	7.97 063	10
52	53 126	55 79 I	44 209	97 335	55 169 58	3 1 1 5	41 885	97 059 97 054	9 8
53 54	53 161 53 106	55 831	44 169	97 331	55 202 58	153	41 847	97 049	7 6
54 55	53 196 1.53 231	55 870 1.55 910	44 I 30 0.44 090	97 326 1.97 322	1.55 268 1.58	191 229	41 809 0.41 771	_ 97 044 1.97 039	5
55 56	53 266	55 949	44 05 I	97 317	55 301 58	267	41 733	97 035	4
57 58	53 301 53 336	55 989 56 028	44 01 I 43 972	97 312 97 308	55 334 5 ⁸	304 342	41 696 41 658	97 030 97 025	3 2
59 60	_ 53 370	_ 56 067	43 933	_ 97 303	55 400 58	380	41 620	_97 020	r
60	1.53 405	7.56 107	0.43 893	1.97 299	1.55 433 1.58	3 418	0.41 582	1.97 015	0'
	log cos	log oot	log tan	log sin	log cos log	cot	log tan	log sin	' '

70°

69°

LOG SIN, etc. 69°-72°

LC	OG SIN, etc. 21° 22°									
		log sin	log tan	log oot	log oos	log sin	log tan	log oot	log cos	
	0′ 1	1.55 433	1.58 418	0.41 582	1.97 015	ī.57 358	1.60 641	0.39 359	1.96 717	60′
	2	55 466 55 499	58 455 58 493	41 545 41 507	97 010 97 005	57 389 57 420	60 677 60 714	39 323 39 286	96 711 96 706	59 58
	3	55 532	58 531	41 469	97001	57 451	60 750	39 250	96 701	57 56
	4 5	55 564 1.55 597	58 569 7.58 606	41 431 0.41 394	96 996 7.96 991	57 482 1.57 514	60 786 1 60 823	39 214 0.39 177	96 696 1 .96 691	55
	5 6	55 630	58 644	41 356	96 986	57 545	60 859	39 141	96 686	54
	7 8	55 663 55 695	58 681 58 719	41 319	96 981	57 576 57 607	60 895	39 105 39 069	96 681 96 676	53
	9	55 728	58 757	41 281 41 243	96 976 96 971	57 638	60 931 60 967	39 033	96 670	52 51
	10	1.55 761	ī.58 794	0.41 206	ī.96 966		7.61 004	0.38 996		50
	11 12	55 793 55 826	58 832 58 869	41 168	96 962	57 700	61 040 61 076	38 960 38 924	96 660 96 655	49 48
	13	55 858	58 907	41 131 41 093	96 957 96 952	57 731 57 762	61 112	38 888	96 650	47
	14	55 891	58 944	41 056	96 947	57 793	61 148	38 852	96 645	46
	15 16	1.55 923 55 956	59 019	0.41 019 40 981	1.96 942 96 937	1.57 824 57 855	61 220	0.38 816 38 780	96 634	45 44
	17	55 988	59 056	40 944	96 932	57 885	61 256	38 744	96 629	43
	18 19	56 021 56 053	59 094 59 131	40 906 40 869	96 927 96 922	57 916 57 947	61 292 61 328	38 708 38 672	96 624 96 619	42 41
	20	7.56 o85		0.40 832		1.57 978		0.38 636		40
	21	56 118	59 205	40 795	96 912	58 008	61 400	38 600	96 608	39 38
	22 23	56 150 56 182	59 243 59 280	40 757 40 720	96 907 96 903	58 039 58 070	61 436 61 472	38 564 38 528	96 603 96 598	38
	24	56 215	59 317	40 683	96 898	58 101	61 508	38 492	96 593	36
	25 26	1.56 247			ī.96 893	1.58 131 58 162		0.38 456 38 421		35
	27	56 279 56 311	59 39 1 59 429	40 609 40 571	96 888 96 883	58 102	61 579 61 615	38 385	96 582 96 577	34
	28	56 343	59 466	40 534	96 878	58 223	61 651	38 349	96 572	32
	30	56 375	59 503	40 497 0.40 460	96 873 ī. 96 868	58 253	61 687	38 313 0.38 278	96 567 7 66 760	3 ¹
	31	56 440	59 577	40 423	96 863	58 314	61 758	38 242	96 556	29
	32	56 472	59 614	40 386	96 858	58 345	61 794	38 206	96 551	28
	33	56 504 56 536	59 651 59 688	40 349 40 312	96 853 96 848	58 375 58 406	61 830 61 865	38 170 38 135	96 546 96 541	27 26
	35	ī.56 568	1.59 725	0.40 275	1.96 843	ī.58 436	ī.61 901	0.38 099	ī.96 535	25
	36	56 599 56 631	59 762 59 799	40 238 40 201	96 838 96 833	58 467 58 497	61 936 61 972	38 064 38 028	96 530 96 525	24 23
	37 38	56 663	59 835	40 165	96 828	58 527	62 008	37 992	96 520	22
	39	56 695	59 872	40 128	96 823	58 557	62 043	37 957	96 514	21
	40 41	ī.56 727 56 759	1.59 909 59 946	0.40 091 40 054	7.96 818 96 813	7.58 588 58 618	62 114	0.37 921 37 886	7.96 509 96 504	20 19
	42	56 790	59 983	40 017	96 808	58 648	62 150	37 850	96 498	18
	43 44	56 822 56 854	60 019 60 056	39 981	96 803 96 798	58 678 58 709	62 185 62 221	37 8±5 37 779	96 493 96 488	17 16
	45	7.56 886		39 944 0.39 907	ī.96 793	T.58 739	ī.62 256	0.37 744	ī.96 483	15
	46	56 917	60 130	39 870	96 788	58 769	62 292	37 708	96 477	14
	47 48	56 949 56 980	60 166 60 203	39 834 39 797	96 783 96 778	58 799 58 829	62 327 62 362	37 673 37 638	96 472 96 467	13 12
•	49	57 012	60 240	39 760	96 772	58 859	62 398	37 602	96 461	11
	50		ī.60 276	0.39 724	1.96 767	ī.58 889	1.62 433	0.37 567	ī.96 456	10
	51 52	57 °75 57 107	60 313 60 349	39 687 39 651	96 762 96 757	58 919 58 949	62 468 62 504	37 53 ² 37 496	96 451 96 445	9 8
	53	57 138	60 386	39 614	96 752	58 979	62 539	37 461	96 440	7 6
	54	57 169 1.57 201	60 422 1.60 459	39 578 0.39 541	96 747 7.96 742	59 009 1.59 039	62 574 1.62 609	37 426 0.37 391	96 435 1.96 429	
	55 56	57 232	60 495	39 505	96 737	59 069	62 645	37 355	96 424	5 4
	57 58	57 264 57 295	60 532 60 568	39 468 39 432	96 732 96 727	59 098 59 128	62 680 62 715	37 320 37 285	96 419 96 413	3 2
	59 60 ′	_ 57 326	60 605	39 395	96 722	_ 59 158	62 750	37 265 37 250	96 408	1
	60′	1.57 358	1.60 641		1.96 717	1.59 188	1.62 785	0.37 215	1.96 403	_0′_
	0.01	log oos	log oot	log tan	log sin	log oos	log oot	log tan	log sin	,
LU)G SI 55°-6	N, etc.	6	8°	(5	8)	-	67°		
•		-								

		20				24	LOG SI	IN, et
′	log sin log t	tan log cot	log oos	log sin	log tan	log oot	log oos	
0'		785 0.37 215	7.96 403	ī.60 931	ī.64 858	0.35 142	ī.96 073	60′
1	59 218 62	820 37 180 855 37 145	96 397	60 960	64 892	35 108	96 067	59 58
3	59 247 62 59 277 62	855 37 145 890 37 110	96 392 96 387	60 988 61 016	64 926 64 960	35 074 35 040	96 062 96 056	57
4		926 37 074	96 381	61 045 •		35 006	96 050	56
5 6	7.59 336 7.62		ī.96 376	7.61 073		0.34 972		55
		996 37 004 031 36 969	96 370 96 365	61 101 61 129	65 062 65 096	34 938	96 039 96 034	54
7 8		066 36 934	96 360	61 158	65 130	34 904 34 870	96 028	53 52
9		101 36 899	96 354	61 186	65 164	34 836	96 022	51
10	1.59 484 1.63	135 0.36 865	ī.96 349	1.61 214		0.34 803		50
11	59 514 63	170 36 830	96 343	61 242	65 231 65 265	34 769	96 001	49 48
12	3, 3.0	205 36 795 240 36 760	96 338 96 333	61 270 61 298	65 299	34 735 34 701	96 005 96 000	47
13 14		275 36 725	96 327	61 326	65 333	34 667	95 994	46
15	1.59 632 1.63	310 0.36 690	ī.96 322			0.34 634	7.95 988	45
16	59 661 63	345 36 655	96 316	61 382	65 400	34 600 34 566	95 982 95 977	44
17 18		379 36 621 414 36 586	96 311 96 305	61 411 61 438	65 434 65 467	34 533	95 971	43 42
19		449 36 551	96 300	61 466	65 501	34 499	95 965	41
20	7.59 778 7.63			ī.61 494	7.65 535 65 568	0.34 465	ī.95 960	40
2I	59 808 63	519 36481	96 289	61 522,	65 568	34 432	95 954	39 38
22	59 837 63	553 36 447	96 284	61 550 61 578	65 602 65 636	34 398 34 364	95 948 95 942	3° 37
23 24	59 866 63 59 895 63	588 36 412 623 36 377	96 278 96 273	61 606	65 669	34 33I	95 937	36
25	7.59 924 T.63		1.96 267	ī.61 634		0.34 297	T.95 931	35
26		692 36 308	96 262	61 662	65 736	34 264	95 925	34
27	59 983 63	726 36 274	96 256	61 689 61 717	65 770 65 803	34 230 34 197	95 920 95 914	33 32
28 29		761 36 239 796 36 204	96 251 96 245	61 745	65 837	34 163	95 908	31
30	1	830 0.36 170	ī.96 240			0.34 130		30
31	60 099 63	865 36 135	96 234	61 800	65 904	34 096	95 897	29
32	60 128 63	899 36 101	96 229	61 828	65 937	34 063	95 891	28
33		934 36 066 968 36 032	96 223 96 218	61 856 61 883	65 97 I 66 004	34 029 33 996	95 885 95 879	27 26
34 35	1.60 215 T.64		ī.96 212		T.66 038	0.33 962		25
36		037. 35 963	96 207	61 939	66 071	33 929	95 868	24
37 38		072 35 928	96 201	61 966	66 104 66 138	33 896 33 862	95 862 95 856	23
38 39		. 106 35 894 . 140 35 860	96 196 96 190	61 994 62 021	66 171	33 829	95 850	21
40	7.60 359 T.64	_	ī.96 185	1.62 049	ī.66 204	0.33 796	ī.95 844	20
41		209 35 791	96 179	62 076	66 238	33 762	95 839	19
42	60 417 64	243 35 757	96 174	62 104	66 271	33 729	95 ⁸ 33	18
43		. 278 35 722 . 312 35 688	96 168 96 162	62 131	66 304 66 337	33 696 33 663	95 827 95 821	17 16
44 45	60 474 64 1.60 503 1.64		7.96 157	7.62 186	1.66 371	0.33 629	1.95 815	15
46 46	60 532 64	. 381 35 619	96 151	62 214	66 404	33 596	95 810	14
47	60 561 64	415 35 585	96 146	62 241	66 437	33 563	95 804	13
48 49		449 35 551 483 35 517		62 268 62 296	66 470 66 503	33 530 33 497	• 95 798 95 792	12 11
50		, 483 35 517 , 517 0.35 483				0.33 463		10
51	60 675 64	1 552 35 448	96 123	62 350	66 570	33 430	95 780	9 8
52	60 704 64	₁ 586 35414	. 96 118	62 377	66 603	33 397	95 775	8
53		1620 35 380 1654 35 346	96 112 96 107	62 405 62 432	66 636 66 669	33 364 33 331	95 769 95 763	7 6
54 55		1 654 35 346 1 688 0.35 312		1.62 459		0.33 298	_	
55 56		722 35 278	96 095	62 486	66 735	33 265	95 75 I	4
57 5 8	60 846 64	4 756 35 244	, 96090	62 51 3	66 768 66 801	33 232 33 199		5 4 3 2
58	60 875 64	4 790	96 084 5 96 079	62 541 62 568	66 834			I
59 60 ′		4 858 0.35 14:	2 1.96 073	1.62 595	7.66 867	0.33 133	1.95 728	0'
		cot log tan	log sin	log cos	log cot	log tan	log sin	′_

 65° LOG SIN, etc. 65° - 68°

Q	G S	G SIN, etc. 20° 26°							
Ī	,	log sin	log tan log cot	log cos	log sin	log tan	log oot	log oos	
	0′	1.62 595	1.66 867 0.33 133	ī.95 728	ī.64 184	7.68 818	0.31 182	ī.95 366	60′
	I 2	62 622 62 649	66 900 33 100 66 933 33 067	95 722 95 716	64 210 64 236	. 68 850 68 882	31 150 31 118	95 360 95 354	- 59 -58
	3	62 676	66 966 33 034	95 710	64 262	68 914	31 086	95 348	57
	4	62 703	66 999 33 001	95 704	64 288	68 946	31 054	95 341	56
	5 6	1.62 730	1.67 032 0.32 968	T.95 698	1.64 313		0.31 022	1.95 335	55
		62 757 62 784	67 065 32 935 67 098 32 902	95 692 95 686	64 339 64 365	69 010 69 042	30 990 30 958	95 329 95 323	54
	7 8	62 811	67 131 32 869	95 68o	64 391	69 074	30 926	95 323	52
	. 9	62 838	67 163 32 837	95 674	64 417	69 106	30 894	95 310	51
	10	1.62 865	1.67 196 0.32 804	ī.95 668	T.64 442		0.30 862	1.95 304	50
	11 12	62 892 62 918	67 229 32 77 I 67 262 32 738	95 663	64 468 64 494	69 170 69 202	30 830	95 298	49 48
	13	62 945	67 262 32 738 67 295 32 705	95 657 95 651	64 519	69 234	30 798 30 766	95 292 95 286	47
	14	62 972	67 327 32 673	95 645	64 545	69 266	30 734	95 279	46
	15		T.67 360 0.32 640		ī.64 57 I		0.30 702	1.95 273	45
	16 17	63 026 63 052	67 393 32 607 67 426 32 574	95 633 95 627	64 596 64 622	69 329 69 361	30 67 I 30 639	95 267	44
	18	63 079	67 426 32 574 67 458 32 542	95 621	64 647	69 393	30 607	95 261 95 254	43 42
	19	63 106	67 491 32 509	95 615	64 673	69 425	3º 575	95 248	41
	20	1.63 133	1.67 524 0.32 476	ī.95 609	ī.64 698	1.69 457	0.30 543	ī.95 242	40
	2I 22	63 159 63 186	67 556 32 444 67 589 32 411	95 603	64 724	69 488	30 512	95 236	39 38
	23	63 213	67 589 32 411 67 622 32 378	95 597 95 59 1	64 749 64 775	69 520 69 552	30 480 30 448	95 229 95 223	37
	24	63 239	67 654 32 346	95 585	64 800	69 584	30 416	95 217	36
	25		1.67 687 0.32 313	ī 95 579	1.64 826	1.69 615		1.95 211	35
	26 27	63 292 63 319	67 719 32 281 67 752 32 248	95 573	64 851 64 877	69 647 69 679	30 353 30 321	95 204	34
	28	63 345	67 785 32 215	95 567 95 561	64 902	69 710	30 290	95 198 95 192	33 32
	29	63 372	67 817 32 183	95 555	64 927	69 742	30 258	95 185	31
	30	,00,	T.67 850 0.32 150	ī.95 549	ī.64 953	1.69 774	0.30 226	ī.95 179	30
	31	63 425	67 882 32 118	95 543	64 978	69 805	30 195	95 173	29
	32 33	63 451 63 478	67 915 32 085 67 947 32 053	95 537 95 531	65 003 65 029	69 837 69 868	30 163 30 132	95 167 95 160	28 27
	34	63 504	67 980 32 020	95 525	65 054	69 900	30 100	95 154	26
	35 36		T.68 012 0.31 988	ī.95 5 1 9		1.69 932		1.95 148	25
	36	63 557	68 044 31 956 68 077 31 923	95 513	65 104	69 963	30 037	95 141	24
	37 38	63 583 63 610	68 077 31 923 68 109 31 891	95 507 95 500	65 130 65 155	69 995 70 026	30 005 29 974	95 I 35 95 I 29	23
ı	39	63 636	68 142 31 858	95 494	65 180	70 058	29 942	95 122	21
1	40		1.68 174 0.31 826	ī.95 488	ī.65 205	ī.70 089	0.29 911	7.95 116	20
	41	63 689	68 206 31 794 68 239 31 761	95 482	65 230 65 255	70 I2I 70 I52	29 879 29 848	-95 110	19 18
1	42 43	63 715 63 741	68 239 31 761 68 271 31 729	95 476 95 470	65 281	70 184	29 816	95 103 95 097	17
ı	44	63 767	68 303 31 697	95 464	65 306	70 215	29 785	95 090	ΙĠ
1	45	7.63 794	7.68 336 0.31 664	ī.95 458	1.65 331		0.29 753	1.95 o84	15
ı	46	63 820 63 846	68 368 31 632 68 400 31 600	95 452 95 446	65 356 65 381	70 278 70 309	29 722 29 69 I	95 078 95 071	14 13
ı	47 48	63 872	68 432 31 568	95 440	65 406	70 341	29 659	95 065	12
ı	49	63 898	68 465 31 535	95 434	65 431	70 372	29 628	95 059	11
ı	50			1.95 427		ī.70 404		ī.95 052	10
ı	51 52	63 950 63 976	68 529 31 471 68 561 31 439	95 421 95 415	65 481 65 506	70 435 70 466	29 565 29 534	95 046 95 039	9 8
ı	53	64 002	68 593 31 407	95 409	65 531	70 498	29 502	95 033	7 6
ı	54	64 028	68 626 31 374	_ 95 403	65 556	_ 70 529	29 47 I	_95 O27	
	55 56	1.64 054 64 080	7.68 658 0.31 342 68 690 31 310	1.95 397 95 391	7.65 580 65 605	70 560 70 592	29 408	1.95 020 95 014	5 4 3
	57	64 106	68 722 31 278	95 384	65 630	70 623	29 377	95 007	3
	57 58	64 132	68 754 31 246	95 378	65 655	70 654	29 346	95 001	2
	59 60 ′	64 158 7.64 184	68 786 31 214 7.68 818 0.31 182	_95 372 1.95 366	65 680 7.65 705	70 685 1.70 717	29 315 0.29 283	_94 995 1.94 988	0'
ŀ		log cos	log oot log tan	log sin	log oos	log cot	log tan	log sin	-
ō	G SI	N, etc.	64°	(6	0)	C	3°		
•	51°-6	4 °	UT	("	,	•	, 0	_	

log sin, etc. 61°-64°

62°

25°-28° LOG SIN, etc.

_			<u> 37° </u>				28°	LOG S	ilN, e
	log sin	log tan	log oot	log oos	log sin	log tan	log cot	log oos	
0′ 1	1.65 705 65 729		0.29 283 29 252	1.94 988 94 982	1.67 161	1.72 567	0.27 433	ī.94 593	60′
2	65 754	70 779		94 902	67 185 67 208	72 598 72 628	27 402 27 372	94 587 94 580	59 58
3	65 779	70 810	29 190	94 969	67 232	72 659	27 341	94 573	57
4 5	65 804 7.65 828	70 841 1.70 873	29 159 0.29 127	94 962 1.94 956	67 256 1.67 280	72 689	27 311	94 567	56
5 6	65 853	70 904	29 096	94 949	67 303	72 720	0.27 280 27 250	1.94 560 94 553	55 54
7 8	65 878	70 935	29 065	94 943	67 327	72 780	27 220	94 546	53
8	65 902	70 966 70 997	29 034 29 003	94 936 94 930	67 350 67 374	72 811 72 841	27 189	94 540	52
10	T.65 952	ī.71 028	0.28 972	ī.94 923	1.67 398	ī.72 872	27 159 0.27 128	94 533	51
11	65 976	71 059	28 941	94 917	67 421	72 902	27 098	1.94 526 94 519	50
12	66 001	71 090	28 910	94 911	67 445	72 932	27 068	94 513	48
13 14	66 025	71 121 71 153	28 879 28 847	94 904 94 898	67 468 67 492	72 963 72 993	27 037 27 007	94 506 94 499	47 46
15	ī.66 075	1.71 184	0.28816	ī.94 891	1.67 515	ī.73 023		I.94 492	45
16	66 099	71 215	28 785	94 885	67 539	73 054	26 946	. 94 485	44
17 18	66 124 66 148	71 246 71 277	28 754 28 723	94 878 94 871	67 562 67 586	73 084 73 114	26 916 - 26 886	94 479	43
19	66 173	71 308	28 692	94 865	67 609	73 144	26 856	94 472 94 465	42 41
20	1.66 197	ī.71 339	0.28 661	1.94 858		ī.73 175	0.26 825	ĩ.94 458	40
21	66 221	71 370	28 630	94 852	67 656	73 205	26 795	94 451	39
22	66 246 66 270	71 401	28 599 28 569	94 845 94 839	67 680	73 235	26 765	94 445	38
23 24	66 295	71 431 71 462	28 538	94 839	67 703 67 726	73 265 73 295	26 735 26 705	94 438 94 431	37 36
25 26	7.66 319	ī.71 493	0.28 507	ī.94 826		1.73 326	0.26 674	T.94 424	35
	66 343	71 524	28 476	94819	67 773	73 356	26 644	94 417	34
27 28	66 368 66 392	71 555 71 586	28 445 28 414	94 813 94 806	67 796 67 820	73 386 73 416	26 614 26 584	94 410 94 404	33 32
2 9	66 416	71 617	28 383	94 799	67 843	73 446	26 554	94 397	31
30	ī.66 441	ī.71 648	0.28 352	ī.94 793	ī.67 866	ī.73 476		1.94 390	30.
31	66 465	71 679	28 321	94 786	67 890	73 507	26 493	94 383	29
32 33	66 489	71 709 71 740	28 29 I 28 260	94 780 94 773	67 913 67 936	73 537 73 567	26 463 26 433	94 376 94 369	28 27
34	66 537	71 771	28 229	94 767	67 959	73 597	26 403	94 362	26
35	T.66 562		0.28 198	1.94 760		1.73 627	0,26 373	ī.94 355	25
36 27	66 586 66 610	71 833 71 863	28 167 28 137	94 753	68 006 68 029	73 657 73 687	26 343 26 313	94 349	24
37 38	66 634	71 894	28 106	94 747 94 740	68 052	73 717	26 283	94 342 94 335	23 22
39	66 658	71 925	28 075	94 734	68 075	73 747	26 253	94 328	21
40	1.66 682			ī.94 727			0.26 223	ī.94 321	20
4I 42	66 706 66 731	71 986 72 017	28 014 27 983	94 720	68 121 68 144	73 ⁸⁰ 7 73 ⁸ 37	26 193 26 163	94 314	19 18
43	66 755	72 048	27 952	94 714 94 7 07	68 167	73 867	26 133	94 307 94 300	17
44	66 779	72 078	27 922	94 700	68 190	73 897	26 103	94 293	16
45 46	1.66 803 66 827		0.27 891 27 860	1.94 694	1.68 213		0.26 073	ī.94 286	15
47	66 85 i	72 140 72 170	27 800 27 830	94 687 94 680	68 237 68 260	73 957 73 987	26 043 26 01 3	94 279 94 273	14 13
48	66 875	72 201	27 799	94 674	68 283	74 017	25 983	94 266	12
49	66 899	72 231	27 769	94 667	68 305	74 047	25 953	94 259	ΙΙ
50	1.66 922	1.72 262	0.27 738	1.94 660	ī 68 328	1.74 077	0.25 923	1.94 252	10
51 52	66 946 66 970	72 293 72 323	27 707 27 677	94 654 94 647	68 351 68 374	74 107 74 137	25 893 25 863	94 245 94 238	9 8
53	66 994	72 354	27 646	94 640	68 397	7.4 1 66	25 834	94 231	7 6
54	67 018	72 384	27 616	94 634	68 420	74 196	25 804	94 224	
55 56	1.67 042 67 066	72 415	0.27 585 27 555	1.94 627 94 620	1.68 443 68 466	74 226	0.25 774 25 744	94 217	5 4
57	67 090	72 476	27 524	94 614	68 489	74 286	25 714	94 203	5 4 3 2
57 58	67 113	72 506	27 494	94 607	68 512	74 316	25 684	94 196	2 I
59 60 ′	67 137 7.67 161	72537 $\overline{1.72567}$	27 463 0.27 433	94 600 1.94 593	68 534 1.68 557	74 345 1.74 375	25 655 0.25 625	_94 189 1.94 182	0'
_ 	log cos	log cot	log tan	log sin	log cos	log cot	log tan	log sin	,

(61) 61° LOG SIN, etc. 61°-64°

<u> </u>	51	N, etc.	~	U				บบ		
1	<u>'</u>	log sin	log tan	log oot	log oos	log sin	log tan	log oot	log cos	
	\mathbf{D}'	ī.68 557	ī.74 375	0.25 625	1.94 182	ī.69 897	ī.76 144	0.23 856	ī.93 753	60'
I		68 580	74 405	25 595	94 175	69 919	76 173	23 827	93 746	59 58
2		68 603 68 625	74 435	25 565	94 168	69 941	76 202	23 798	93 738	
3		68 648	74 465 74 494	25 535 25 506	94 161	69 963 69 984	76 231 76 261	23 769 23 739	93 731	57
		7.68 671	74 494 1.74 524	0.25 476	94 I54 1.94 I47	T.70 006	T.76 290	0.23 710	93 724 1.93 717	36
5	5 1	68 694	74 554	25 446	94 140	70 028	76 319	23 681	93 709	55 54
7 8		68 716	74 583	25 417	94 133	70 050	76 348	23 652	93 702	53
		68 739	74 613	25 387	94 126	70 072	76 377	23 623	93 695	52
9		68 762	74 643	25 357	94 119	70 093	76 406	23 594	93 687	51
	0	ī.68 784	ī.74 673	0.25 327	ī.94 II2		ī.76 435	0,23 565	ī.93 680	50
	I	68 807	74 702	25 298	94 105	70 137	76 464	23 536	93 673	49
	3	68 829 68 852	74 732	25 268	94 098	70 159	76 493	23 507	93 665	48
	4	68 875	74 762 74 791	25 238 25 209	94 090 94 083	70 180 70 202	76 522 76 551	23 478 23 449	93 658 93 650	47 46
	5	ī.68 897	ī.74 821	0.25 179	ī.94 076	ī.70 224	T.76 580	0.23 420	T.93 643	45
	6	68 920	74 851	25 149	94 069	70 245	76 609	23 391	93 636	44
	7	68 942	74 880	25 120	94 062	70 267	76 639	23 361	93 628	43
	8	68 965	74 910	25 090	94 055	70 288	76 668	23 332	93 621	42
	9	68 987	74 939	25 061	94 048	70 310	76 697	23 303	93 614	41
	0	1.69 010	1.74 969	0.25 031	1.94 041		7.76 725	0.23 275	ī.93 606	40
	2	69 032 69 055	74 998 75 028	25 002 24 972	94 034 94 027	70 353	76 754 76 783	23 246 23 217	93 599	39 38
	3	69 077	75 058	24 9/2	94 027	7º 375 7º 396	76 812	23 188	93 591 93 584	37
	4	69 100	75 087	24 913	94 012	70 418	76 841	23 159	93 577	36
2	5	1.69 122	1.75 117	0.24 883	1.94 005	ī.70 439	ī.76 870	0.23 130		35
	6	69 144	75 146	24 854	93 998	70 461	76 899	23 101	93 562	34
	7	69 167	75 176	24 824	93 991	70 482	76 928	23072	93 554	33
	8	69 189 69 21 2	75 205 75 235	24 795	93 984 93 977	70 504 70 525	76 957 76 986	23 043	93 547	32
		_		24 765				23014	93 539	31
_	0	ī.69 234 69 256	75 264 75 294	0.24 736 24 706	1.93 970 93 963	7.70 547 70 568	1.77 015 77 044	0.22 985 22 956	1.93 532 93 525	30
	2	69 279	75 323	24 677	93 955	70 590	77 073	22 937	93 523	28
	3	69 301	75 353	24 647	93 948	70 611	77 101	22 899	93 510	27
3	4	69 323	75 382	24 618	93 941	70 633	77 130	22 870	93 502	26
3	5	1.69 345	1.75 411	0.24 589	1.93 934	1.70 654	1.77 159	0.22 841		25
	6	69 368	75 441	24 559	93 927	70 675	77 188	22 812	93 487	24
3	7	69 390 69 412	75 47º 75 500	24 530 24 500	93 920 93 912	70 697 70 718	77 217 77 246	22 783 22 754	93 480 93 472	23
3		69 434	75 529	24 471	93 905	70 739	77 274	22 726	93 472	21
4		ī.69 456	ī.75 558	0.24 442	ī.93 898	ī.70 761	1.77 303	0.22 697	ī.93 457	20
4	- 1	69 479	75 588	24 4 1 2	93 891	70 782	77 332	22 668	93 450	19
4		69 501	75 617	24 383	93 884	70 803	77 361	22 639	93 442	18
4		69 523	75 647	24 353	93 876	70 824	77 390	22 610	93 435	17
4		69 545	75 676	24 324	93 869	70 846	77 418	22 582	93 427	16
4.		7.69 567 69 589	1.75 705	0.24 295 24 265	T.93 862 93 855	ī.70 867 70 888	1.77 447 77 476	0.22 553 22 524	1.93 420 93 412	15 14
4		69 611	75 735 75 764	24 236	93 847	70 909	77 505	22 495	93 405	13
4		69 633	75 793	24 207	93 840	70 931	77 533	22 467	93 397	12
49	- 1	69 655	75 822	24 178	93 833	70 952	77 562	22 438	93 390	11
50	0	ī.69 677	7.75 852	0.24 148	7.93 826	ī.70 973	ī.77 <u>5</u> 91	0.22 409	7.93 382	10
5	Ιİ	69 699	75 88 1	24 119	93 819	70 994	77 619	22 381	93 375	9 8
5	2	69 721	75 910	24 090 24 061	93 811 93 804	71 015	77 648	22 352	93 367	0 7
5. 54	3	69 743 69 765	75 939 75 969	24 031	93 797	71 036 71 058	77 677 77 706	22 323 22 294	93 360 93 352	7 6
5.5		T.69 787	T.75 998	0.24 002	1.93 789	ĭ.71 070	ī.77 734		ī.93 344	5
50	6	69 809	76 027	23 973	93 782	71 100	77 763	22 237	93 337	5 4 3 2
50 50 50	7	69 831	76 056	23 944	93 775	71 121	77 791 77 820	22 209	93 329	3
58	8	69 853	76 086	23 914 23 885	93 768	71 142	77 820	22 180	93 322	
59 6 0	8, I	69 875 7.69 897	76 115 1.76 144	0.23 856	_ 93 760 1.03 753	71 163 1.71 184	77 849	22 I5I 0.22 I23	_ 93 314 1.93 307	0'
1 - O/	- -	log oos	log oot	log tan	log sin	log cos	log cot	log tan	log sin	
	- [TOE OOR	108 000	109 001	70 PM	108 000	100 000	700 Amm	705 pre	1 7

LOG SIN, etc. 57°-60° 60°

(62)

32° LOG SIN, etc.

	-	T	3.					32°	LOG S	SIN, e
Variable Variable	-0'	log sin				log sin	log tan	log oot		T
2 71 226 77 935 22 065 93 201 72 461 79 673 20 383 93 834 53 3 71 247 77 963 22 037 93 284 71 268 77 992 22 008 93 275 5 17.1 268 77 992 22 008 93 275 5 17.1 289 7.18 208 0.21 980 7.93 265 7 1310 78 049 21 951 93 261 7 7 1317 80 97 21 923 32 53 8 71 352 78 106 21 804 32 45 9 71 373 78 135 21 865 93 238 71 352 78 106 21 808 93 235 72 522 79 777 20 223 93 79 75 53 9 71 373 78 135 21 865 93 238 72 522 79 776 20 224 93 787 53 9 71 373 78 135 21 865 93 238 72 522 79 804 20 196 93 779 53 10 17.13 93 7.8 163 0.21 83 8 93 223 72 603 79 842 20 168 92 771 55 11 2 71 435 78 220 21 808 93 223 72 603 79 946 20 056 92 739 12 71 435 78 290 21 780 93 215 13 71 456 78 249 21 751 93 207 14 71 477 78 277 21 723 93 200 15 17.1 498 1.78 306 0.21 694 1.03 192 16 71 159 78 334 21 666 93 184 17 15 39 78 363 21 637 93 177 18 71 500 78 391 21 600 93 169 71 87 150 78 391 21 600 93 169 71 87 150 78 839 21 600 93 169 72 72 83 80 084 10 916 92 609 12 1 71 682 78 449 21 581 93 161 20 1.71 602 7.8 448 0.21 552 7.93 154 12 1 71 643 78 505 21 495 93 138 12 1 71 622 78 476 21 524 93 146 12 1 71 607 78 595 21 495 93 138 13 71 685 78 502 21 438 93 123 14 71 77 78 677 21 33 53 93 103 15 17 78 78 78 50 21 435 93 103 17 72 88 38 0223 19 777 92 659 38 17 79 70 79 92 90 92 61 33 18 71 505 7.8 590 0.21 410 7.93 115 17 72 88 38 0 223 19 777 92 659 38 17 70 70 78 87 50 21 438 93 123 20 71 78 78 78 79 21 21 23 53 93 000 21 71 72 72 78 78 78 79 20 0.21 40 78 31 22 71 77 77 78 67 71 21 353 93 000 23 71 78 78 78 78 21 21 33 93 000 24 71 78 78 78 79 21 21 23 93 300 25 71 77 70 77 78 67 75 20 21 20 28 8 20 30 31 27 71 77 77 78 67 77 21 33 53 93 100 28 71 79 70 78 87 50 21 24 50 8 28 71 79 79 79 83 20 21 268 79 30 30 28 71 79 79 78 79 20 20 28 92 93 10 29 71 78 78 79 20 20 20 28 92 93 10 20 71 71 88 79 00 20 21 20 88 70 30 10 20 71 71 80 71 80 70 80 80 80 80 80 90 90 90 90 90 90 90 90 90 90 90 90 90					, ,			0.20 421	1.92 842	60′
3 71 247 77 963 22 037 93 284 72 482 76 663 10 377 94 818 57 57 57 58 57 94 58 57 94 58 57 59 57 58 57 58 57 58 58 57 58 58 57 58 58 57 58 58 57 58 58 58 58 58 58 58 58 58 58 58 58 58		71 226					79 607	20 393		59
Triple T			77 963	22 037			79 663			
17, 13, 13, 13, 13, 13, 13, 13, 13, 13, 13		I _ '	11 22				_ 79 691	20 309	92 810	
7	6			_		1.72 522				
9			78 077	21 923						
10				21 894	93 246	72 582	79 804		7 1-1	
111		4 _				I _ '			92 771	
12			78 103	0.21 837			ī.79 860			50
13										49
14	13	71 456	78 249							
16	•		- ⁷⁸ 277				79 972	20 028		
17			1.78 306							
18 71 560 78 391 21 609 93 169 72 783 80 084 19 166 92 699 42 20 17 1602 78 448 0.21 552 19.3 161 72 803 80 112 19 888 92 691 41 21 71 622 78 476 21 524 93 146 72 803 80 102 19 868 92 653 39 22 71 643 78 505 21 495 93 138 72 863 80 195 19 805 92 659 37 24 71 685 78 502 21 438 93 123 72 902 80 221 19 749 92 651 36 25 7,17 770 78 678 21 323 93 108 72 902 80 231 19 749 92 633 36 27 71 747 78 647 21 353 93 108 72 962 80 335 19 655 92 637 33 27 71 787 78 792 21 268 73 307 73 602 80 331 19 639 92 635 34 27			78 363	21 637						
20	ìέ	71 560	78 391	21 609						
21		71 581		21 581	93 161	72 803	80 112	19 888		
222			ī.78 448		ī.93 154			0.19 860		40
23			78 476			72 843			92 675	39
24			78 533						92 007 92 650	38
25		71 685	78 562			, ,			92 651	37 36
71 720 78 618 21 382 93 108 72 942 80 307 19 693 92 635 34 71 767 78 675 21 325 93 092 72 982 80 363 19 637 92 619 32 29 71 788 78 704 21 296 93 084 73 002 80 391 19 609 92 611 31 31 31 31 32 78 760 21 240 93 069 32 73 002 80 391 19 609 92 611 31 31 32 71 850 78 789 21 211 93 061 73 061 80 447 19 553 92 587 29 33 71 850 78 789 21 211 93 061 73 061 80 447 19 553 92 587 29 33 71 850 78 789 21 211 93 061 73 061 80 447 19 526 92 587 28 335 71 891 78 845 21 155 93 046 73 061 80 530 19 470 92 571 26 336 71 932 78 902 21 098 93 030 73 08 80 502 19 498 92 579 27 73 101 80 530 19 470 92 571 26 336 71 932 78 930 21 070 93 022 73 160 80 644 19 386 92 546 23 38 71 973 78 959 21 041 93 044 71 93 58 92 538 22 338 71 994 78 987 21 013 93 047 73 200 80 642 19 358 92 538 22 338 71 994 78 987 21 013 93 047 73 200 80 642 19 358 92 538 22 338 71 994 78 987 21 013 93 047 73 200 80 642 19 358 92 538 22 338 71 994 78 987 21 013 93 047 73 200 80 642 19 358 92 538 22 338 72 79 100 20 900 92 976 73 239 80 753 19 247 92 500 18 447 72 057 79 02 02 02 02 02 02 02 0	25					ī.72 922	ī.80 279		ī.92 643	
28									92 635	34
30	28									
30 T.71 809 T.78 732 0.21 268 T.93 077 71 829 78 760 21 240 93 069 73 041 80 447 19 553 92 595 29 32 71 870 78 760 21 211 93 069 73 041 80 447 19 553 92 595 29 33 71 870 78 817 21 183 93 053 73 061 80 474 19 553 92 595 28 34 71 891 78 845 21 155 93 046 73 061 80 474 19 526 92 587 28 36 71 911 71.78 874 0.21 126 7.93 036 73 081 80 530 19 470 92 571 26 37 71 932 78 959 21 041 93 030 73 160 80 586 19 414 92 555 24 38 71 973 78 959 21 041 93 014 73 180 80 642 19 358 92 538 22 40 1.72 014 7.79 015 0.20 985 7.92 999 73 239 80 669 19 331 92 530 21 41 72 034 79 043					93 084					
31	30		ī.78 732	0.21 268	_				- 1	
33 71 850 76 769 21 211 93 061 73 061 80 474 19 526 92 587 28 34 71 891 78 845 21 155 93 046 73 081 80 502 19 498 92 579 26 35 17 1911 1.78 874 0.21 126 1.93 038 73 101 80 530 19 470 92 571 26 36 71 932 78 902 21 098 93 030 73 140 80 386 19 414 92 555 24 38 71 973 78 987 21 013 93 046 73 180 80 642 19 336 92 546 23 39 71 994 78 987 21 013 93 047 73 180 80 642 19 336 92 546 23 39 71 994 78 987 21 013 93 047 73 180 80 669 19 331 92 538 22 40 7.2 014 1.79 015 0.20 985 1.92 999 7.73 219 1.80 697 0.19 303 1.92 522 20 41 72 055 79 072 20 928 29 93 73 278 80 781		71 829	78 760		93 069	73 041	80 447			29
71 891 78 845 21 155 93 046 17.71 911 1.78 874 0.21 126 1.93 038 71 932 78 902 21 098 93 030 71 952 78 930 21 070 93 022 38 71 973 78 959 21 041 93 014 73 180 80 846 19 414 92 555 24 23 39 71 994 78 987 21 013 93 007 1.72 014 1.79 015 0.20 985 1.92 999 41 72 034 79 043 20 957 92 991 42 72 055 79 072 20 928 92 983 43 72 075 79 100 20 900 92 976 44 72 096 79 128 20 872 92 968 45 1.72 116 1.79 156 0.20 844 1.92 960 73 180 80 642 19 358 92 538 21 73 389 80 725 19 275 92 514 19 72 096 79 128 20 872 92 968 45 1.72 116 1.79 156 0.20 844 1.92 960 75 173 189 17 88 80 808 19 192 92 490 16 1.72 116 1.79 156 0.20 844 1.92 960 77 198 79 269 20 731 92 929 77 3208 80 808 19 192 92 490 16 1.72 118 1.79 297 0.20 703 1.92 921 17 72 238 79 326 20 674 92 913 77 2 279 79 382 20 618 92 897 77 3 405 18 80 97 0.19 025 1.92 441 72 299 79 410 20 590 92 887 73 495 81 030 18 970 92 445 74 72 299 79 440 20 590 92 887 75 353 81 141 18 859 92 392 75 381 79 523 20 447 92 858 77 2 381 79 523 20 447 92 858 77 2 381 79 523 20 447 92 858 77 2 381 79 523 20 447 92 858 77 3 591 81 224 18 776 92 367 77 3591 81 106 18 80 19 410 78 180 80 642 19 386 92 867 79 38				21 211		73 061	80 474			28
35 T.71 911 T.78 874 0.21 126 T.93 038 T.73 121 T.80 558 0.19 442 T.92 563 25 36 71 932 78 902 21 098 93 030 73 140 80 586 19 414 92 555 24 37 71 972 78 930 21 070 93 022 73 160 80 614 19 386 92 546 23 39 71 994 78 987 21 013 93 007 73 180 80 642 19 358 92 538 22 40 T.72 014 T.79 015 0.20 985 T.92 999 73 200 80 669 19 331 92 530 21 42 72 034 79 043 20 957 92 991 73 239 80 725 19 275 92 514 19 43 72 075 79 100 20 900 92 976 73 278 80 781 19 217 92 506 18 45 T.72 116 T.79 156 0.20 844 T.92 960 73 318 T.80 836 0.19 164 T.92 482 15 <td></td> <td></td> <td>78 845</td> <td></td> <td></td> <td>73 101</td> <td>80 502 80 520</td> <td></td> <td></td> <td></td>			78 845			73 101	80 502 80 520			
36 71 932 78 902 21 098 93 030 73 140 80 \$86 19 414 92 555 24 37 71 952 78 930 21 070 93 022 73 160 80 614 19 386 92 546 23 38 71 973 78 959 21 041 93 014 93 014 73 180 80 642 19 358 92 538 22 39 71 994 78 987 21 013 93 007 73 200 80 669 19 331 92 530 22 40 1.72 014 7.79 015 0.20 985 7.92 999 73 20 928 92 983 73 259 80 753 19 247 92 506 18 72 034 79 043 20 957 92 991 73 259 80 753 19 247 92 506 18 43 72 075 79 100 20 900 92 976 79 128 20 872 92 968 73 278 80 781 19 219 92 498 17 73 278 80 781 19 219 92 498 17 45 1.72 116 1.79 156 0.20 844 1.92 960 72 137 79 185 20 815 92 952 73 337 80 864 19 136 92 473 14 73 377 80 892 19 108 92 465 13 48 72 177 79 241 20 759 92 936 73 377 80 891 91 90 81 92 457 12 73 377 80 991 91 08 92 465 13 49 72 198 79 269 20 731 92 929 73 373 80 864 19 136 92 475 12 73 377 80 991 91 081 92 457 12 50 1.72 218 7.79 297 0.20 703 7.92 921 73 346 78 80 91 91 90 81 92 457 12 73 377 80 91 91 90 81 92 457 12 51 72 279 79 382 20 674 92 913 73 435 81 003 18 997 92 433 92 73 377 80 91 91 90 81 92 457 12 52 72 279 79 382 20 618 92 897 73 448 1086 18 914 92 408 6 73 474 81 68 81 8942 92 416 77 73 494 81 086 18 914 92 408 6 55 72 360 79 495 20 505 92 886 72 92			1.78874				1.80 558	-		
37 71 952 78 930 21 070 93 022 73 160 80 614 19 386 92 546 23 38 71 973 78 959 21 041 93 014 73 180 80 642 19 358 92 538 22 40 1.72 014 1.79 015 0.20 985 1.92 999 73 209 80 669 19 331 92 530 21 41 72 034 79 043 20 957 92 991 73 219 1.80 697 0.19 303 1.92 522 20 43 72 075 79 100 20 900 92 976 73 259 80 753 19 247 92 506 18 43 72 075 79 100 20 900 92 976 73 278 80 781 19 219 92 498 17 44 72 096 79 128 20 872 92 968 73 278 80 808 19 192 92 498 17 45 1.72 116 1.79 156 0.20 844 1.92 960 73 337 80 861 19 132 92 490 16 47 72 157 79 241 20 759 92 936 73 377 80 892	36		78 902	21 098	93 030	73 140	80 586			
39 71 994 78 987 21 013 93 007 73 200 80 669 19 331 92 530 21 40 1.72 014 1.79 015 0.20 985 1.92 999 73 200 80 669 19 331 92 530 21 41 72 034 79 043 20 957 92 991 73 239 80 725 19 275 92 514 19 42 72 055 79 072 20 928 92 983 73 259 80 753 19 247 92 506 18 43 72 075 79 100 20 900 92 976 73 278 80 781 19 219 92 498 17 44 72 096 79 128 20 872 92 968 73 278 80 781 19 219 92 490 16 45 1.72 116 1.79 156 0.20 844 1.92 960 73 378 80 80 19 192 92 490 16 47 72 157 79 213 20 815 92 952 73 337 80 892 19 108 92 473 14	37		78 930			73 160				
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41				-			_			
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$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				20 928	92 983	73 259	80 753	19 247		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$				20 900 20 872						
46				0,20 844						
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	46	72 137		20 815						
49	47			20 787	92 944		80 892	19 108	,	
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52 72 259 79 354 20 646 92 905 73 455 81 030 18 970 92 425 8 53 72 279 79 382 20 618 92 897 73 474 81 058 18 942 92 416 7 54 72 299 79 410 20 590 92 889 73 494 81 086 18 914 92 408 6 55 1.72 320 1.79 438 0.20 562 1.92 881 1.73 513 1.81 113 0.18 887 1.92 400 5 56 72 340 79 496 20 534 92 874 73 533 81 141 18 859 92 392 4 57 72 360 79 495 20 505 92 866 73 552 81 169 18 831 92 384 3 58 72 381 79 523 20 477 92 858 73 572 81 196 18 804 92 376 2 59 72 401 79 551 20 449 92 850 73 591 81 224 18 776 92 367 1 60' 1.72 421 1.79 579 0.20 421 1.92 842 1.73 611 1.81 252	51		79 326	20 674	92 921		81 003			70
53 72 279 79 382 20 618 92 897 73 474 81 058 18 942 92 416 7 54 72 299 79 410 20 590 92 889 73 494 81 086 18 914 92 408 6 55 1.72 320 1.79 438 0.20 562 1.92 881 1.73 513 1.81 113 0.18 887 1.92 400 5 56 72 340 79 466 20 534 92 874 73 533 81 141 18 859 92 392 4 57 72 360 79 495 20 505 92 866 73 552 81 169 18 831 92 384 3 58 72 381 79 523 20 477 92 858 73 572 81 196 18 804 92 376 2 59 72 401 79 551 20 449 92 850 73 591 81 224 18 776 92 367 1 60' 1.72 421 1.79 579 0.20 421 1.92 842 1.73 611 1.81 252 0.18 748 1.92 359 0'	52	72 259	79 354	20 646	92 905		81 030	18 970		
55 \$\overline{1.72}\$ 320 \$\overline{1.79}\$ 438 \$0.20\$ 562 \$\overline{1.92}\$ 281 \$\overline{1.73}\$ 513 \$\overline{1.81}\$ 113 \$0.18\$ 887 \$\overline{1.92}\$ 400 \$5 56 72 340 79 466 20 534 92 874 73 533 81 141 18 859 92 392 4 57 72 360 79 495 20 505 92 866 73 552 81 169 18 831 92 384 3 58 72 381 79 523 20 477 92 858 73 572 81 196 18 804 92 376 2 59 72 401 79 551 20 449 92 850 73 591 81 224 18 776 92 367 1 60' 1.72 421 1.79 579 0.20 421 1.92 842 1.73 611 1.81 252 0.18 748 1.92 359 0'						73 474		18 942	92416	
57 72 360 79 495 20 505 92 866 73 552 81 169 18 831 92 384 3 58 72 381 79 523 20 477 92 858 73 572 81 196 18 804 92 376 2 59 72 401 79 551 20 449 92 850 73 591 81 224 18 776 92 367 1 60' 1.72 421 1.79 579 0.20 421 1.92 842 1.73 611 1.81 252 0.18 748 1.92 359 0'	55					73 494				
57 72 360 79 495 20 505 92 866 73 552 81 169 18 831 92 384 3 58 72 381 79 523 20 477 92 858 73 572 81 196 18 804 92 376 2 59 72 401 79 551 20 449 92 850 73 591 81 224 18 776 92 367 1 60' 1.72 421 1.79 579 0.20 421 1.92 842 1.73 611 1.81 252 0.18 748 1.92 359 0'	56							18859		3 4
59 72 401 79 551 20 449 92 850 73 591 81 224 18 776 92 367 1 60' 1.72 421 1.79 579 0.20 421 1.92 842 1.73 611 1.81 252 0.18 748 1.92 359 0'	57	72 360	79 495	20 505	92 866	73 552	81 169	18 831	92 384	3
	58		79 523							
	60'		_ /9 551 1.79 579			1.73 611				
log cos log cot log tan log sin log cos log cot log tan log sin l		log cos	log cot	log tan	log sin	log oos	log oot	log tan	log sin	 -

58°

57°

(63)

LOG SIN, etc. 57°-60°

<u>og s</u>	IN, etc.				34°				
,	log sin	log tan	log oot	log cos	log sin	log tan	log cot	log oos	
0'	1.73 611		0.18 748	1.92 359	1.74 756	ī.82 899	0.17 101	1.91 857	60′
1 2	73 630 73 650	81 279 81 307	18 721 18 693	92 351	74 775	82 926 82 953	17 074 17 047	91 849 91 840	59 58
3	73 669	81 335	18 665	92 343 92 335	74 794 74 812	82 980	17 020	91 832 •	57
4	73 689	81 362	18 638	92 326	74 831	83 008	16 992	91 823	56
5 6	1.73 708		0.18610	ī.92 318	7.74 850	ī.83 o35	0.16 965	1.91 815	55
7	73 727 73 747	81 418 81 445	18 582 18 555	92 310 92 302	74 868 74 887	83 062 83 089	16938 16911	91 806 91 798	54 53
7 8	73 766	81 473	18 527	92 302	74 906	83 117	16 883	91 789	52
9	73 785	81 500	18 500	92 285	74 924	83 144	16 856	91 781	51
10	1.73 805	ī.81 528	0.18 472	ī.92 277	ī.74 943	7.83 171	0.16 829	ĩ.91 772	50
II I2	73 824	81 556	18 444	92 269	74 961	83 198	16 802	91 763	49
13	73 843 73 863	81 583 81 611	18 417 18 389	92 260 92 252	74 980 74 999	83 225 83 252	16 775 16 748	91 755 91 746	48 47
14	73 882	81 638	18 362	92 244	75 017	83 280	16 720	91 738	46
15	ī.73 901	ī.81 666	0.18 334	1.92 235	ī.75 036	7.83 307		ī.91 72 9	45
16 17	73 921	81 693 81 721	18 307 18 279	92 227	75 054	83 334	16 666	91 720	44
18	73 940 73 959	81 748	18 252	92 219 92 21 I	75 073 75 09 I	83 361 83 388	16 639 16 612	91 712 91 703	43 42
19	73 978	81 776	18 224	92 202	75 110	83 415	16 585	91 695	41
20	1.73 997	ī.81 803	0.18 197	ī.92 194	1.75 128	ī.83 442	0.16 558	ī.91 686	40
21	74 017	81 831	18 169	92 186	75 147	83 470	16 530	91 677	39
22 23	74 036	81 858 81 886	18 142 18 114	92 177 92 169	75 165 75 184	83 497 83 524	16 503 16 476	91 669 91 660	38 37
24	74 074	81 913	18 087	92 161	75 202	83 551	16 449	91 651	36
25	T.74 093		0.18 059	1.92 152	1.75 221	T.83 578		ī.91 643	35
26	74 113	81 968	18032	92 144	75 239	83 605	16 395	91 634	34
27 28	74 132 74 151	81 996 82 023	18 004 17 977	92 136 92 127	75 258 75 276	83 632 83 659	16 368 16 341	91 625 91 617	33 32
29	74 170	82 051	17 949	92 119	75 294	83 686	16 314	91 608	3 ²
30	1.74 189	7.82078	0.17 922	1.92 111	1.75 313	1.83 713	0.16 287	7.91 599	30
31	74 208	82 106	17 894	92 102	75 331	83 740	16 260	91 591	29
32 33	74 227 74 246	82 133 82 161	17 867 17 839	92 094 92 086	75 350 75 368	83 768 83 795	16 232 16 205	91 582 91 573	28 27
34	74 265	82 188	17812	92 000	75 386 75 386	83 822	16 178	91 565	26
35		1.82 215	0.17 785	1.92 069	T.75 405		0.16 151		25
36	74 303	82 243	17 757	92 060	75 423	83 876	16 124	91 547	24
37 38	74 322 74 34 I	82 270 82 298	17 730 17 702	92 052 92 044	75 44 I 75 459	83 903 83 930	16 097 16 070	91 538 91 530	23 22
39	74 360	82 325	17 675	92 035	75 478	83 957	16 043	91 521	21
40	1.74 379	ī.82 352	0.17 648	1.92 027	ī.75 496		0.16 016	•	20
41	74 398	82 380	17 620	92 018	75 5 14	84 01 1	15 989	91 504	19
42 43	74 417	82 407 82 435	17 593 17 565	92 010 92 002	75 533 75 551	84 038 84 065	15 962 15 935	91 495 91 486	18 17
43	74 455	82 462	17 538	91 993	75 569	84 092	15 935	91 477	16
45	1.74 474	ī.82 489	0.17 511	ī.91 985	ī.75 587	ī.84 119	0.15 881	ī.91 469	15
46	74 493	82 517	17 483	91 976	75 605	84 146	15 854	91 460	14
47 48	74 512	82 544 82 571	17 456 17 429	91 968 91 959	75 624 75 642	84 173 84 200	15 827 15 800	91 451 91 442	13
49	74 549	82 599	17 401	91 951	75 660	84 227	15 773	91 433	II
50	ī.74 568	7.82 626	0.17 374		ī.75 678		0.15 746		10
51	74 587	82 653	17 347	91 934	75 696	84 280	15 720	91 416	
52	74 606	82 681 82 708	17 319	91 925	75 714	84 307	15 693	91 407 91 398	98 76 54 32 1
53 54	74 625 74 644	82 735	17 292 17 265	91 917 91 908	75 733 75 751	84 334 84 361	15 666 15 639	91 398	6
	1.74 662	ī.82 762	0.17 238	1.91 900	ī.75 769	T.84 388	0.15 612	ī.91 381	5
56	74 681	82 790	17 210	91 891	75 787	84 415	15 585	91 372	4
55 56 57 58	74 7 ⁰⁰ 74 7 ¹ 9	82 817 82 844	17 183 17 156	91 883 91 874	75 805 75 823	84 442 84 469	15 558 15 531	91 363 91 354	3
59	74 719	82 871	17 129	91 866	75 841	84 496	15 504	91 354	ī
59 60 ′	1.74 756	1.82 899	0.17 101	1.91 857	1.75 859	1.84 523	0.15 477	ī.91 <u>33</u> 6	0′
	log cos	log cot	log tan	log sin	log oos	log oot	log tan	log sin	'

LOG SIN, etc. 53°-56°

56°

(64)

 $33^{\circ}-36^{\circ}$ LOG SIN, etc.

	30°		36°_	LOG SI	11, 61
	log sin log tan log cot log cos	log sin log tan	log oot	log cos	\neg
0′	1.75 859 1.84 523 0.15 477 1.91 336	1.76 922 1.86 126		ī.90 796	60'
I	75 877 84 550 15 450 91 328	76 939 86 153	13847	90 787	59 58
3	75 895 84 576 15 424 91 319 75 913 84 603 15 397 91 310	76 957 86 179 76 974 86 206	13 821 13 794	90 777 90 768	5° 57
4	75 931 84 630 15 370 91 301	76 991 86 232	13 768	90 759	56
	1.75 949 1.84 657 0.15 343 1.91 292	1.77 009 1.86 259		T.90 750	55
5 6	75 967 84 684 15 316 91 283	77 026 86 285	13 715	90 741	54
7 8	75 985 84 711 15 289 91 274	77 043 86 312	13 688 13 662	90 731	53
	76 003 84 738 15 262 91 266 76 021 84 764 15 236 91 257	77 061 86 338 77 078 86 365	13 635	90 722 90 713	52 51
9	1 '	ī.77 095 ī.86 392		1.90 704	50
10	76 039 T.84 791 0.15 209 1.91 248 76 057 84 818 15 182 91 239	77 112 86 418	13 582	90 694	49
12	76 075 84 845 15 155 91 230	77 130 86 445	13 555	90 685	48
13	76 093 84 872 15 128 91 221	77 147 86 471	13 529	90 676	47
14	76 111 84 899 15 101 91 212	77 164 86 498	13 502	90 667	46
15	1.76 129 1.84 925 0.15 075 1.91 203	77 181 T.86 524 77 199 86 551	0.13 476 13 449	90 648	45 44
16	76 146 84 952 15 048 91 194 76 164 84 979 15 021 91 185	77 216 86 577	13 423	90 639	43
17 18	76 164 84 979 15 021 91 185 76 182 85 006 14 994 91 176	77 233 86 603	13 397	90 630	42
19	76 200 85 033 14 967 91 167	77 250 86 630	13 370	90 620	4 I
20	1.76 218 1.85 059 0.14 941 1.91 158	ī.77 268 ī.86 656	0.13 344	1.90 611	40
21	76 236 85 086 14 914 91 149	77 285 86 683	13 317	90 602	39
22	76 253 85 113 14 887 91 141	77 302 86 709	13 291	90 592	38
23	76 271 85 140 14 860 91 132	77 319 86 736 77 336 86 762	13 264 13 238	90 583 90 574	37 36
24	76 289 85 166 14 834 91 123 1.76 307 1.85 193 0.14 807 1.91 114	77 353 T.86 789		ī.90 565	35
2 5 26	76 324 85 220 14 780 91 105	77 370 86 815	13 185	90 555	34
27	76 342 85 247 14 753 91 096	77 387 86 842	13 158	90 546	33
28	76 360 85 273 14 727 91 087	77405 86868	13 132	90 537	32
29	76 378 85 300 14 700 91 078	77 422 86 894	13 106	90 527	31
30	7.76 395 T.85 327 0.14 673 T.91 069	1.77 439 1.86 921	0.13 079		30
31	76 413 85 354 14 646 91 060	77 456 86 947	13 053 13 026	90 509 90 499	29 28
32	76 431 85 380 14 620 91 051 76 448 85 407 14 593 91 042	77 473 86 974 77 490 87 000	13 000	90 499	27
33 34	76 448 85 407 14 593 91 042 76 466 85 434 14 566 91 033	77 507 87 027	12973	90 480	26
35	1.76 484 1.85 460 0.14 540 1.91 023		0.12 947	1.90 471	25
36	76 501 85 487 14 513 91 014	77 541 87 079	12 921	90 462	24
37 38	76 519 85 514 14 486 91 005	77 558 87 106	12 894	90 452	23
	76 537 85 540 14 460 90 996	77 575 87 132 77 592 87 158	12 868 12 842	90 443 90 434	22 2I
39	76 554 85 567 14 433 90 987		0.12 815		20
40	76 572 T.85 594 0.14 406 T.90 978 76 590 85 620 14 380 90 969	77 609 T.87 185	12 789	1.90 424 90 415	19
4I 42	76 590 85 620 14 380 90 969 76 607 85 647 14 353 90 960	77 643 87 238	12 762	90 405	ı8
43	76 625 85 674 14 326 90 951	77 660 87 264	12 736	90 396	17
44	76 642 85 700 14 300 90 942	77 677 87 290	12 710	90 386	16
45	1.76 660 1.85 727 0.14 273 1.90 933		0.12 683	1.90 377	15
46	76 677 85 754 14 246 90 924	77 711 87 343 77 728 87 369	12 657 12 631	90 368 90 358	14 13
47 48	76 695 85 780 14 220 90 915 76 712 85 807 14 193 90 906	77 728 87 369 77 744 87 396	12 604	90 349	12
49	76 730 85 834 14 166 90 896	77 761 87 422	12 578	90 339	11
50	1.76 747 1.85 860 0.14 140 1.90 887	1.77 778 T.87 448	0.12 552	ī.90 330	10
51	76 765 85 887 14 113 90 878	■ 77 795 87 475	12 525	90 320	9 8
52	76 782 85 913 14 087 90 869	77 812 87 501	12 499	90 311	8
53	76 800 85 940 14 060 90 860	77 829 87 527 77 846 87 554	12 473 12 446	90 3 01 90 292	7 6
54	76 817 85 967 14 033 90 851 1.76 835 1.85 993 0.14 007 1.90 842	77 846 87 554 7.77 862 7.87 580		_ ~	
55	76 835 T.85 993 0.14 007 T.90 842	1 77 879 87 606		90 273	4
57	76 870 86 046 13 954 90 823	77 896 87 633	12 367	90 263	3
55 56 57 58	76 887 86 073 13 927 90 814	77 913 87 659		90 254	5 4 3 2
59 60 /	76 904 86 100 13 900 90 805			90 244 1.90 235	0'
60		1.77 946 1.87 711 log cos log cot			\ \
	log oos log cot log tan log sir	Tog ous Tog cot	-25 000		

54°

 53° Loc

LOG SIN, etc. 53°-56°

UG 3	in, etc.		01			บ	0		
,	log sin	log tan	log oot	log cos	log sin	log tan	log oot	log oos	
0′	ī.77 946	1.87 711	0.12 289	ī.90 235	1.78 934	1.89 281	0.10 719	ī.89 653	60
I	77 963	87 738	12 262	90 225	78 950	89 307	10 693	89 643	59
2	77 980	87 764	12 236	90 216	78 967	89 333	10 667	89 633	58
3	77 997 78 013	87 790 87 817	12 210 12 183	90 206 90 197	78 983 78 999	89 359	10 641 10 615	89 624 89 614	57 56
4			0.12 157	1.90 187	70 999	89 385 7.89 411	0.10 589		50
5 6	78 047	87 869	12 131	90 178	79 031	89 437	10 563	89 594	55 54
7 8	.78 063	87 895	12 105	90 168	79 047	89 463	10 537	89 584	53
	78 080	87 922	12 078	90 159	79 063	89 489	10 511	89 574	52
9	78 097	87 948	12052	90 149	79 079	89 515	10 485	89 564	51
10	1.78 113	ī.87 974	0.12 026	ī.90 139	ī.79 095	1.89 541	0.10 459	ī.89 554	50
II	•78 130	88 000	12 000	90 130	79 111	89 567	10 433	89 544	49
12	78 147 78 163	88 027	11 973	90 120	79 128	89 593	10 407	89 534	48
13 14	78 180	88 053 88 079	11 947 11 921	90 111	79 144 79 160	89 619 89 645	10 381	89 524 89 514	47 46
15		ī.88 105		1.90 091		7.89 671	0.10 329		45
16	78 213	88 131	11 869	90 082	79 192	89 697	10 303	89 495	44
17	78 230	88 158	11 842	90 072	79 208	89.723	10 277	89 485	43
18	78 246	88 184	11 816	90 063	79 224	89 749	10 251	89 475	42
19	78 263	88 210	11 790	90 053	79 240	89 775	10 225	89 465	41
20	7.78 280	ī.88 236	0.11 764	ī.90 043			0.10 199	ī.89 455	40
2I 22	78 296 78 313	88 262 88 289	11 738	90 034 90 024	79 272 79 288	89 827	10 173	89 445	39
23	78 329	88 315	11 711 11 685	90 024 90 014	79 200 79 304	89 853 89 879	10 147 10 121	89 435 89 425	38
24	78 346	88 341	11 659	90 005	79 319	89 905	10 095	89 415	37 36
25	ī.78 362	ī.88 367		ī.89 995	ī.79 335	7.89 931	0.10 069		35
26	78 379	88 393	11 607	89 985	79 351	89 957	10 043	89 395	34
27	78 395	88 420	11 580	89 976	79 367	89 983	10 017	89 385	33
28	78412	88 446	11 554	89 966	79 383	90 009	09 991	89 375	32
29	78 428	88 472	11 528	89 956	_ 79 399	90 035	09 965	89 364	31
30	78 445	1.88 498 88 524	0.11 502	1.89 947	1.79 415	1.90 061		ī.89 354	30
31 32	78 478	88 550	11 476 11 450	89 937 89 927	79 431 79 447	90 086 90 112	09 914 09 888	89 344 89 334	29 28
33	78 494	88 577	11 423	89 918	79 463	90 138	09 862	·89 324	27
34	78 510	88 603	11 397	89 908	79 478	90 164	09 836	89 314	26
35 36	1.78 527	7.88 629	0.11 371	ī.89 898	ī.79 494	ī.90 190	0.09 810	ī.89 304	25
36	78 543	88 655	11 345	89 888	79 510	90 216	09 784	89 294	24
37 38	78 560	88 681	11 319	89 879	79 526	90 242	09 758	89 284	23
39	78 576 78 592	88 707 88 733	11 293 11 267	89 869 89 859	79 542 79 558	90 268 90 294	09 732 09 706	89 274 89 264	22 2I
40	T.78 609		0.11 241	ī.89 849			0.09 680		20
4I	78 625	88 786	11 214	89 840	1.79 573 79 589	90 346	0.09 080	89 244	19
42	78 642	88 812	11 188	89 830	79 605	90 371	09 629	89 233	18
43	78 658	88 838	11 162	89 820	79 621	90 397	09 603	89 223	17
44	78 674	88 864	11 136	89 810	79 636	90 423	09 577	89 213	16
45	7.78 691		0.11 110	1.89 801	7.79 652	1.90 449	0.09 551	1.89 203	15
46	78 707	88 916 88 942	11 084	89 791	79 668 70 684	90 475	09 525	89 193	14
47 48.	78 723 78 739	88 968	11 058 11 032	89 781 89 771	79 684 79 699	90 501 90 527	09 499 09 473	89 183 89 173	13 12
49	78 756	88 994	11 006	89 761	79 715	90 553	09 447	89 162	II
50	1.78 772		0.10 980		1.79 731	_		7.89 152	10
51	78 788	89 046	10 954	89 742	79 746	90 604	0.09 422	89 142	
52	78 805	89 073	10 927	89 732	79 762	90 630	09 370	89 132	8
53	78 821	89 099	10 901	89 722	79 778	90 656	09 344	89 122	7
54	78 837	89 125	10 875	89 712	79 793	90 682	09 318	89 112	98 76 5432 I
55 56	78 853 78 869	89 177	10 849	1.89 702 89 693	7.79 809	1.90 708	0.09 292	1.89 101	5
50	78 886	89 203	10 797	89 683	79 825 79 840	90 734 90 759	09 266 09 241	89 09 I 89 08 I	4 2
57 58	78 902	89 229	10 771	89 673	79 856	90 785	09 215	89 071	2
59 60 ′	78918	89 255	10 745	89 663	79 872	90 811	09 189	_ 89 060	I
60'	1.78 934		0.10 719	7.89 653		ī.90 837	0.09 163	ī.89 050	0'
	log oos	log cot	log tan	log sin	log oos	log oot	log tan	log sin	1

LOG SIN, etc. 49°-52°

52°

(66)

40°

37°-40° LOG SIN, etc.

7	T :						40	LOG	SIN, e
	log sin	log tan		log oos	log sin	log tan	log oot	log oos	
0'	70 002				ī.80 807		0.07 619	1.88 425	60′
2	79 903 79 918				80 822 80 837	92 407	, 525	88 415	
3	79 934			89 0 30 89 0 20	80 837 80 852	92 433 92 458		88 404	59 58
4	_ 79 950	90 940	09 060	89 009	80 867				57 56
5 6	1.79 965	1.90 966			1.80 882	1.92 510	0.07 490	1.88 372	55
	79 981	90 992 91 018		88 989	80 897	92 535	07 465	88 362	54
7 8	79 996 80 012	91 043	08 982 08 957	88 978 88 968	80 912 80 927		07 439	88 351	53
9	80 027	91 069		88 958	80 942			88 340 88 330	52
10			0.08 905	ĩ.88 948	T.80 957		0.07 362	T.88 319	51
īĭ	80 058	91 121	08 879	88 937	80 972	92 663	o.o7 302 o7 337	88 308	50
12	80 074	91 147	08 853	88 927	80 987	92 689	07 311	88 298	49 48
13	80 089	91 172	08 828 08 802	88 917	81 002	92 715	07 285	88 287	47
14	80 105 1.80 120	91 198		88 906 T.88 896	81 017	92 740	07 260	88 276	46
15 16	80 136	1.91 224 91 250	0.08 770	88 886	81 047	92 792	0.07 234 07 208	88 255	45
17	80 151	91 276	08 724	88 875	81 061	92 817	07 183	88 244	44 43
18	80 166	91 301	08 699	88 865	81 076	92 843	07 157	88 234	42
19	80 182	91 327	08 673	88 855	81 091	92 868	07 132	88 223	41
20	ī.80 197	ī.91 353	0.08 647	ī.88 844		ī.92 894	0.07 106	ī.88 212	40
21	80 213	91 379	08 621	88 834	81 121	92 920	07 080	88 201	39
22 23	80 228 80 244	91 404 91 430	08 596 08 570	88 824 88 813	81 136 81 151	92 945	07 055	88 191 88 180	38
24	80 259	91 456	08 544	88 803	81 166	92 971 92 996	07 029 07 004	88 169 -	37 36
25	T.80 274	ī.91 482	0.08 518	ī.88 793			0.06 978		35
2 6	80 290	91 507		88 782	81 195	93 048	06 952	88 148	34
27	80 305	91 533	08 467	88 772	81 210	93 073	06 927	88 137	33
28	80 320	91 559	08 441	88 761	81 225	93 099	06 901	88 126	32
29	80 336	91 585	08 415	88 751	81 240	_ 93 124	06 876	88 115	. 31
30	7.80 351 80 366		0.08 390 08 364	1.88 741		1.93 150		7.88 105	30
31 32	80 382	91 636 91 662	08 338	88 730 88 720	81 269 81 284	93 175 93 201	06 825 06 799	88 094 88 083	29 28
33	80 397	91 688	08 312	88 709	81 299	93 227	06 773	88 072	27
34	80 412	91 713	08 287	88 699	81 314	93 252	06 748	88 oбı	26
35			0.08 261		ī.81 328	1.93 278	0.06 722		25
36	80 443	91 765	08 235	88 678	81 343	93 303	06 697	88 040	24
37 38	80 458 80 473	91 791 91 816	08 209 08 184	88 668 88 657	81 358 81 372	93 329	06 671 06 646	88 029 88 018	23
39	80 489	91 842	08 158	88 647	81 387	93 354 93 380	06 620	88 007	22 21
40	ī.80 504			ī.88 636		ī.93 406		ī.87 996	
41	80 519	91 893	08 107	88 626	81 417	93 431	06 569	87 985	20
42	80 534	91 919	08 081	88 615	81 431	93 457	06 543	87 975	18
43	80 550	91 945	08 055	88 605	81 446	93 482	06 518	87 964	17
44 45	80 565 1.80 580	91 971	08 029 0.08 004	88 594	81 461	93 508	06 492	87 953	16
45 46	80 595	92 022	0.08 004	88 573	ī.81 475 81 490	7.93 533 93 559	0.06 467 06 44 I	7.87 942 87 931	15
47	80 610	92 048	07 952	88 563	81 505	93 584	06 416	87 931 87 920	14 13
47 48	80 625	92 073	07 927	88 552	81 519	93 610	06 390	87 909	12
49	80 641	92 099	07 901	88 542	81 534	93 636	06 364	87 898	11
50	ī.80 656	1.92 125	0.07 875	T.88 531	T.81 549	ī.93 661	0.06 339	1.87 887	10
51	80 071	92 150	07 850	88 521	81 503	93 687	06 313	87 877	9 8
. 52 53	80 686 80 701	92 176 92 202	07 824	88 510 88 499	81 578 81 502	93 712	06 288 06 262	87 866 87 855	8
54	80 716	92 202	07 798 07 773	88 489	81 592 81 607	93 738 93 763	06 237	87 844	7 6
		I.92 253		1.88 478	1.81 622	1.93 789	0.06 211	7.87 833	5
56	80 746	92 279	07 721	88 468	81 636	93 814	o6 186	87822	4
57	80 762	92 304	07 696	88 457	81 651	93 840	06 160	87 811	3
55 56 57 58 59	80 777 80 792	92 330	07 670	88 447 88 426	81 665 81 680	93 865	06 135 06 109	87 800 87 789	3 2 I
60 ′		_ 92 356 1.92 381	07 644	88 436 1.88 425	7.81 694	93 891 7.93 916	0.06 084	1.87 778	ο'
	log oos	log oot	log tan	log sin	log oos	log oot	log tan	log sin	
		0				.0. *	· · ·	0	·

	41°-4		Л	1 0		42 °				
.Ç	GS	IN, etc.	4	1 °				12°		
1		log sin	log tan	log eet	log oos	log sin	log tan	log cot	log cos	
	0′	1.81 694	1.93916	0.06 084	1.87 778	1.82 551	ī.95 444		1.87 107	60′
	1 2	81 709 81 723	93 942 93 967	06 058 06 033	87 767 87 756	82 565 82 579	95 469 95 495	04 531 04 505	87 096 87 085	59 58
	3	81 738	93 993	06 007	87 745	82 593	95 520	04 480	87 073	57
	4	81 752	94 018	05 982	87 734	82 607	95 545	04 455	87 062	56
	5 6		ī.94 044	0.05 956	1.87 723	7.82 621	1.95 571	0.04 429	7.87 050	55
	6	81 781	94 069	05 931	87 712	82 635	95 596	04 404	87 039	54
	7 8	81 796 81 810	94 095 94 120	05 905 05 880	87 701 87 690	82 649 82 663	95 622 95 647	04 378 04 353	87 028 87 016	53
1	9	81 825	94 146	05 854	87 679	82 677	95 672	04 333	87 005	52 51
	10	1.81 839	ī.94 171	0.05 829	ī.87 668	1.82 691	ī.95 698	_	ī.86 993	50
	11	81 854	94 197	05 803	87 657	82 705	95 723	04 277	86 982	49
	12	81 868	94 222	05 778	87 646	82 719	95 748	04 252	86 970	48
	13 14	81 882 81 897	94 248	05 752	87 635 87 624	82 733 82 747	95 774	04 226 04 201	86 959 86 947	47
	15		94 273 1.94 2 99	05 727 0.05 70I	ī.87 613	1.82 761	95 799 1.95 825		1.86 936	46
	16	81 926	94 324	05 676	87 601	82 775	95 850	04 150	86 924	45 44
	17	81 940	94 350	05 650	87 590	82 788	95 875	04 125	86 913	43
	18	81 955	94 375	05 625	87 579	82 802	95 901	04 099	86 902	42
	19	81 969	94 401	05 599	87 568	82 816	95 926	04 074	86 890	41
	20	1.81 983 81 998	1.94 426 94 452	0.05 574 05 548	ī.87 557 87 546	ī.82 830 82 844	7.95 952 95 977	0.04 048	ī.86 879 86 867	40
	22	82 012	94 452	05 523	87 535	82 858	95 977	03 998	86 855	39 38
	23	82 026	94 503	05 497	87 524	82 872	96 028	03 972	86 844	37
- 1	24	82 041	94 528	05 472	87 513	82 885	96 053	03 947	86 832	36
1	25	1.82 055 82 069	I-94 554	0.05 446		1.82 899 82 91 3	7.96 078 96 104		7.86 821	35
	26 27	82 084	94 579 94 604	05 421 05 396	87 490 87 479	82 927	96 129	03 896 03 871	86 809 86 798	34 33
	28	82 098	94 630	05 370	87 468	82 941	96 155	03 845	86 786	33 32
	29	82 112	94 655	05 345	87 457	82 955	96 180	03 820	86 775	31
	30		ī.94 681	0.05 319	7.87 446		ī.96 205	0.03 795	7.86 763	30
- 1	31	82 141	94 706	05 294	87 434	82 982	96 231	03 769	86 752	29
	32	82 155 82 169	94 732 94 757	05 268 05 243	87 423 87 412	82 996 83 010	96 256 96 281	03 744 03 719	86 740 86 728	28 27
	33 34	82 184	94 783	05 217	87 401	83 023	96 307	03 693	86 717	2 6
		1.82 198	ī.94 808	0.05 192		•ī.83 o37	ī.96 332	0.03 668	ī.86 705	25
	35 36	82 212	94 834	05 166	87 378	83 051	96 357	03 643	86 694	24
	37 38	82 226 82 240	94 859 94 884	05 141 05 116	87 367 87 356	83 065 83 078	96 383 96 408	03 617 03 592	86 682 86 670	23 22
	39	82 255	94 910	05 090	87 345	83 092	96 433	03 567	86 659	21
ı	40		ī.94 935	0.05 065	ī.87 334	ī.83 106	ī.96 459		ī.86 647	20
	41	82 283	94 961	05 039	87 322	83 120	96 484	03 516	86 635	19
	42	82 297	94 986	05 014	87 311	83 133	96 510	03 490	86 624	18
	43	82 311 82 326	95 012 95 037	04 988 04 963	87 300 87 288	83 147 83 161	96 535 96 560	03 465 03 440	86 612 86 600	17 16
	44		7.95 062		ī.87 277			0.03 414		15
	45 46	82 354	95 088	04 912	87 266	83 188	96 611	03 389	86 577	14
	47 48	82 368	95 113	04 887	87 255	83 202	96 636	03 364	86 565	13
1		82 382	95 139	04 861	87 243 87 232	83 215 83 229	96 662 96 687	03 338	86 554 86 542	12 11
	49	82 396	95 164	04 836	_			03 313	ī.86 530	10
	50 51	1.82 410 82 424	7.95 190 95 215	0.04 810	1.87 221 87 209	1.83 242 83 256	7.96 712 96 738	0.03 262	86 518	
	52	82 439	95 240	04 760	87 198	83 270	96 763	03 237	86 507	9 8
	53	82 453	95 266	04 734	87 187	83 283	96 788	03 212	86 495	7 6
J	54	82 467	95 291	04 709	87 175	83 297	96 814	03 186	86 483 7 86 422	0
J	55 56	1.82 481 82 495	95 34 ²	0.04 683 04 658	7.87 164 87 153	7.83 310 83 324	7.96 839 96 864	0.03 161	ī.86 472 86 460	5 4
ı	57	82 509	95 342	04 632	87 141	83 338	96 890	03 110	86 448	3
	57 58	82 523	95 393	04 607	87 130	83 351	96 915	03 085	86 436	
	59 60 ′	82 537	95 418	04 582	87 119	83 365	96 940	03 060	86 425 1.86 413	0 ′
	60′	1.82 551	1.95 444 log cot	0.04 556 log tan	1.87 107 log sin	1.83 378 log oos	1.96 966 log oot	0.03 034 log tan	log sin	-
Ĺ	0.0	log cos		OO		8)		1 170	0	'

LOG SIN, etc. 45°-48°

48°

(68)

41°-44°
44° LOG SIN, etc.

			<u> </u>				44	LOG	,,,,
	log sin	log tan	log oot	log cos	log sin	log tan	log oot	log cos	
0 ′	1.83 378 83 392		0.03 034		ī.84 177			1.85 693	60′
2	83 405	96 991 97 016	03 009 02 984	86 401 86 389	84 190 84 203		01 491	85 681	59
3	83419	97 042	02 958	86 377	84 216		01 466 01 44 0	85 669 85 657	58
4	83 432	_ 97 067	02 933	86 366	84 229	98 585	01 415	85 645	56
5 6	T.83 446		0.02 908		1.84 242	7.98 610		7.85 632	55
	83 459 83 473	97 I I 8 97 I 43	02 882 02 857	86 342 86 330	84 255 84 269	98 635 98 661	01 365	85 620	54
7 8	83 486	97 168	02 832	86 318	84 282		01 339 01 314	85 608 85 596	53 52
9	83 500	97 193	02 807	86 306	84 295	98 711	01 289	85 583	51
10	7.83 513	1.97 219	0.02 781	7.86 295	ī.84 308	ī.98 737	0.01 263	ī.85 571	50
11 12	83 527 83 540	97_244	02 756	86 283	84 321	98 762	01 238	85 559	49
13	83 554	97 269 97 295	02 731 02 705	86 271 86 259	84 334 84 347	98 787 98 812	01 213 01 188	85 547 85 534	48
14	83 567	97 320	02 680	86 247	84 360	98 838	01 162	85 534 85 522	47 46
15	7.83 581	1.97 345	0.02 655	ī.86 235	ī.84 373	ī.98 863		ī.85 510	45
16	83 594	97 371	02 629	86 223	84 385	98 888	01 112	85 497	44
17	83 608	97 396 97 421	02 604 02 579	86 211 86 200	84 398 84 411	98 91 3 98 939	01 087 01 061	85 485	43
19	83 634	97 447	02 553	86 188	84 424	98 939	01 036	85 473 85 460	42 41
20	T.83 648		0.02 528	7.86 176	ī.84 437		-	1.85 448	40
21	83 661	97 497	02 503	86 164	84 450	99 015	00 985	85 436	39
22	83 674 83 688	97 523	02 477	86 152 86 140	84 463		00 960	85 423	38
23 24	83 701	97 548 97 573	02 452 02 427	86 140 86 128	84 476 84 489		00 935 00 910	85 411 85 399	37 36
25	1.83 715	1.97 598	0.02 402		ī.84 502	1.99 116	0.00 884	ī.85 386	35
26	83 728	97 624	02 376	86 104	84 515	99 141	00 859	85 374	34
27 28	83 741	97 649	02 351	86 092 86 080	84 528	99 166	00 834	85 361	33
20 29	83 755 83 768	97 674 97 700	02 326	86 068	84 540 84 553	99 191 99 217	00 809 00 783	85 349 85 337	32 31
30	7.83 781	I.97 725	0.02 275	ī.86 o56	1.84 566	ī.99 242		1.85 324	30
31	83 795	97 750	02 250	86 044	84 579	99 267	00 733	85 312	29
32	83 808	97 776	02 224	86 032	84 592	99 293	00 707	85 299	28
33 34	83 821	97 801 97 826	02 199 02 174	86 020 86 008	84 605 84 618	99 318 99 343	00 682 00 657	85 287 85 274	27 26
35		7.97 851	0.02 149	ī.85 996		1.99 368	0.00 632	T.85 262	25
36	83 861	97 877	02 123	85 984	84 643	99 394	00 606	85 250	24
37	83 874	97 902	02 098	85 972	84 656	99 419	00 581	85 237	23
3 8 39	83 887 83 901	97 927 97 953	02 073 02 047	85 960 85 948	84 669 84 682	99 444 99 469	00 556 00 531	85 225 85 212	22 21
40	ī.83 914	ī.97 978	0.02 022	ī.85 936	7.84 694	7.99 495		7.85 200	20
41	83 927	98 003	0.02 022	85 924	84 707	99 520	0.00 505	85 187	19
42	83 940	98 029	01 971	85 912	84 720	99 545	00 455	85 175	18
43	83 954	98 054	01 946	85 900	84 733	99 570	00 430	85 162	17
44 45	83 967 7.83 980	98 079 1.98 104	01 921	85 888 T.8r 876	84 745 7.84 758	99 596 1.99 621	00 404	85 150 7.85 137	16
45 46	83 993	98 130	01 870	85 864	84 771	99 646	0.00 379	85 125	15 14
47	84 006	98 155	oi 845	85 851	84 784	99 672	00 328	85 112	13
48	84 020	98 180	01 820	85 839	84 796	99 697	00 303	85 100	12
49	84 033	98 206	01 794	85 827	84 809	99 722	00 278	85 087	II
50	84 059	7.98 231 98 256		ī.85 815 85 803	84 835	I.99 747	0.00 253	1.85 074 85 062	10
51 52	84 072	98 281	01 744 01 719	85 791	84 847	99 773 99 7 98	00 202	85 002 85 049	9 8
53	84 085	98 307	01 693	85 779	84 860	99 798 99 823	00 177	85 037	7 6
54	84 098	98 332	or 668	85 766	84 873	99 848	00 152	85 024	
55 56	7.84 112 84 125	7.98 357 98 383	0.01 643	1.85 754 85 742	7.84 885 84 898	ī.99 874 99 899	0.00 126	1.85 012 84 999	5
57	84 138	98 408	01 592	85 742 85 730	84 911	99 924	00 076	84 986	5 4 3 2
57 58	84 151	98 433	01 567	85 718	84 923	_99 949	00 051	84 974	2
59 60 ′	84 164	98 458	01 542	85 706	84 936	1.99 975	00 025	84 961	I O/
60′	1.84 177	1.98 484	0.01 516	1.85 693	1.84 949	0.00 000	log tan	1.84 949	0′
	log cos	log oot	log tan	log sin	log cos	log cot_	Tog ran	log sin	,

46°

45°

LOG SIN, etc. 45°-48°

CONSTANTS.

	MAT	HEMATICAL CONSTANTS.	
QUANTITY.	Numerical Value.		Common Logarithm.
	2.71 828 18	Base of Napierian, natural, or hyperbolic logarithms.	0.43 429 45
ı/log _{10€}	2.30 258 5	Factor to multiply into common logs to convert into Napierian logs.	0.36 221 57
log ₁₀ €	0.43 429 45	Factor to multiply into Napierian logs to convert into common logs.	ī.63 778 43
π	3.14 159 265	Ratio of circumference to diameter.	0.49 714 99
π^2	9.86 960 44	Square of π .	0.99 429 97
1 radian	57° 17′ 45″	57.° 29 58 = 206 265." = arc equal to radius.	
	UNITED STAT	TES, BRITISH, AND METRIC UNITS.	
	e following ratios are	given on the authority of the U.S. Coast and Geo Washington, D.C., 1890."	detic Survey,
r metre	39.37 inches.	This is the legalized ratio for the U. S. The U. S. and the British inch are equal. By comparisons to date (July, 1895), it appears probable that this value is smaller than the real ratio of the "Metre des Archives" to the thirty-sixth part of the "Imperial Standard Yard" by one or two parts in one million.	1.59 516 54
ı metre	1.09 361 1 yard.	The U.S. and the British yard are equal.	0.03 886 29
r metre	3.28 o8 33 feet.	_	0.51 598 42
ı kilometer	0.62 1 3 70 mile	of 5280 feet.	T.79 335 03
ı mile	1.60 934 7 kilom.	_	0.20 664 97
ı yard	0.91 440 2 metre.		1.96 113 71
ı foot	0.30 480 1 metre.		ī.48 401 58
r inch	25.40 005 mm.	Deduced from above legalized ratio of yard and metre in U. S.	1.40 483 46
r inch	25.40 000 mm.	is more convenient besides being proba- bly more exact. It is probably about one part in one million too small, as the reciprocal of 0.0254 is 39.37 008.	1.40 483 37

CONSTANTS.

CONSTANTS.

QUANTITY,	Numerical		Common
	VALUE.		LOGARITHM.
1 pound Av.	7000 grains.	The pound avoirdupois is the	3.84 509 80
	, ,	same in Great Britain and the	3.04 309 80
		U. S.	
1 pound Av.	453.59 242 77 grammes.	C. S.	26-666-9
I ounce Av.	28.34 953 grammes.		2.65 666 58
I ounce Troy	31.10 348 grammes.		1.45 254 59
ı grain			1.49 280 91
1 grain	0.06 479 892 gramme.	Avoirdupois and Troy grains are the same.	2.81 156 78
1 kilogramme	2.20 462 2 pounds Av.		0.34 333 42
ı gramme	15.43 235 639 grains.		1.18 843 22
ı litre	1.05 668 U. S. quarts.	By original definition one litre	0.02 394 4
	J 1	was the volume of one cubic	0.02 394 4
		decimetre, but at present the	
	[accepted definition is that pro-	
		1 - + !	
İ		visionally adopted by the Inter-	
		national Bureau of Weights and	
		Measures in 1880, viz.: the	
		volume of one kilogramme of	
		water at its maximum density.	
		The experimental determina-	
•		tion with high accuracy of the	
	`	relation between this volume	
İ		and the cubic decimetre is still	
		unfinished. The following val-	
		ues assume this ratio to be	1
		unity.	
ı litre	0.26 417 U.S. gallon.	-	ī.42 188 4
: litre	33.814 U. S. fluid oz.	27	1.52 910
ı quart, U. S.	o.94 636 litre.	27	ī.97 605 6
ı gallon, U.S.	3.78 544 litres.	1	0.578116
ı fluid ounce	0.02 957 3 litre.		2.47 090
r bushel, V.S.	231 cu. inches.		2.36 361 20
r British gallon	4.54 346 litres.		0.65 738 67
ı British bushel	36.34 77 litres.		1.56 047 69
	331//		50 047 09
	· · · · - · · · · · · · · · · · · ·		

MECHANICAL OR DYNAMICAL EQUIVALENT OF HEAT.

The best values of this quantity (usually denoted by J) at present attainable (November, 1895) are the following. The values are uncertain by only about \pm one twentieth of one per cent.

427.3 kilogrammetres of work or energy are required at latitude 45°, sea-level $(g=980.6~{\rm c.g.s.})$, to raise 1 kilogramme of water through 1° C. at 15° C.

778.8 ft. lbs. of work or energy are required at latitude 45° , sea-level (g = 980.6 c.g.s.), to raise 1 lb. of water through 1° Fahr. at 59° Fahr. $(= 15^{\circ}$ C.). For most engineering purposes 779 ft. lbs. would be near enough.

1402 ft. lbs. of work or energy are required at latitude 45°, sea-level (g=980.6), to raise 1 lb. of water through 1° Cent. at 15° C. For most engineering purposes 1400 ft. lbs. would be near enough.

4.190°107 ergs of work or energy are required to raise 1 gramme of water through 1° C. at 15° C.

To reduce these values to any given locality, multiply by the ratio g_{45} : g, where g_{45} is the value (980.6) of the acceleration of gravity at latitude 45° , sea-level, and g is the value at the given place. The latter may be obtained from the latitude and altitude of the place by the formula given upon the next page, unless otherwise better known. The altitude correction is but six one-thousandths of one per cent (0.00 006) for each 1000 ft. of elevation, and therefore quite negligible. Within the limits of uncertainty of the quantities involved the latitude correction for places between 30° and 60° may be applied thus:—

	427-3	778.8	1402
For each degree of latitude north of 45° subtract	0.04 kgm.	0.07 ft. lbs.	0.13 ft. lbs.
For each degree of latitude south of 45° add	0.04 kgm.	0.07 ft. lbs.	0.13 ft. lbs.

Note. —The persistence with which the time-honored values, 772 ft. lbs. and 424 kgm., of this most important constant are adhered to in practice, although known to be nearly one per cent too small, is due largely to the flagrant negligence of the authors of text-hooks of both physics and engineering. No attention is paid to the fact that Joule's original data have been amended acceptably to him, and that his work has been smpplemented by the elaborate researches of at least three other independent observers with radically diverse methods. How remarkably these new results check each other and confirm Joule's amended results may be seen from the following table, which is given to indicate the source of the foregoing values.

	OBIGINAL DATA.			REDUCED TO LAT.	Diffs.		
AUTHORITY.	J. kgm.	g.	t°.C.	45° SEA- LEVEL,	FROM DA	DATE.	Reference.
Joule (as corrected and reduced to Baltimore by Rowland.) [Assigning eq.							See quotations in the Rowland and Griffiths references.
wts. to all methods.] [Assigning Rowland's arbi-	427.99	980.05	15.°	'			
trary wts.]	426.66	980.05	15.°				
Mesn of both.	427-33	980,05	15.°	427.08	16	1847-78	
ROWLAND [at Baltimore].	427.4	980.05	15.°	427.16	08	1879	Proc. Am. Acad. A. and S. xv. 75 (1880).
GEIFFITHS [at Greenwich]. (In ergs.)	4.194.107	981.17	15.°	427.70	+.46	1892	Phil. Transac. clxxxiv. 496 (1893).
Miculescu [st Paris].	426.84	98r.00	15.°	427.01	 23	1892	Ann. de Ch. et de Ph. xxvii, 237 (1892).
Mean of all.				427.24	±.23		
Mesn omitting Joule.				427.29			

The specific heat of water, and therefore the value of J, diminishes slightly with rise of temperature. The rate of this diminution is not yet satisfactorily determined, but about as nearly as it is now known the true specific heat s_i at any temperature t° not far from 15° C., may be expressed in terms of true specific heat s_{15} at 15° C. by

$$s_t = s_{15} [1. - 0.00 \, 030 \, (t - 15)].$$

Hence J_t , the number of kgm. or ergs necessary to raise 1 kgr. of water from t° to $t^{\circ} + 1^{\circ}$, will be

$$J_t = J_{15} [1. -0.00030 (t - 15)]$$
 [Range 13° - 20°],

or for 1 lb. of water 1° Fahr.

$$J_t = J_{59} [1 - 0.00030(t - 59)]$$
 [Range 56° - 68°].

The values of J_{15} and J_{59} are given on pages 71 and 72. For further discussion of this subject consult Griffiths, Phil. Mag. xi. 431 (1895).

The scale of temperature in which these results are expressed is the hydrogen scale of the International Bureau of Weights and Measures, which represents, as nearly as it is known, the Thomson absolute scale.

VALUE OF g AT DIFFERENT LATITUDES AND ELEVATIONS.

$$g = g_{45 \ 0} (I - 0.00 \ 259 \cos 2 \lambda - 0.00 \ 000 \ 020 \ H).$$

 $g_{45,0} = 980.6 \frac{\text{cm}}{\text{sec}^2}$ approx. This is the approximate average value of g at latitude 45° , sea-level. The experimental values vary widely in the next place of figures.

 $\lambda =$ latitude of place.

H = altitude of place above sea-level in metres.

Note. — Very recent observations render it probable that near the earth's surface the coefficient of H is more nearly 0.00 000 030.

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The diameter corresponding to any gauge number above zero (i.e. of any size less than that of a No. o wire) may be found to within one hundred-thousandth of an inch (five decimal places) by the expression

Diam. in inches of gauge number
$$n$$
 $= 0.32486 \times 0.890525^n$,

or, Log of diam. in inches =
$$\overline{1}.51 \ 170 + \overline{1}.94 \ 964 \ 5 \ n$$
, or, """""""" = $9.51 \ 170 - 10. + (9.94 \ 964 \ 5 - 10.) n$.

The diameter corresponding to any gauge numbers o, oo, oo, and so on, may similarly be computed by the following expressions in which N is the number of zeros.

Diam. in inches =
$$0.28 930 \times 1.12 293^N$$
,
or, Log of diam. in inches = $\overline{1.46} 1348 + 0.05 035 3 N$.

The two primary sizes on which the gauge is based are No. 0000, diameter 0.46 inch exactly, and No. 36, diameter 0.005 inch exactly.

PHYSICAL AND CHEMICAL CONSTANTS.

For very reliable and extended tables consult Landolt und Börnstein, Physikalisch — Chemische Tabellen.

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